ductile materials (steel, stainless steel, aluminum, titanium, bronze)

distortion energy failure theory using maximum octahedral shear

σ_X σ_Y τ_{XY}

von Mises equivalent stress σ'

$$\sigma' = \sqrt{\sigma_X^{\ 2} + \sigma_Y^{\ 2} - \sigma_X \sigma_Y + 3\,\tau_{XY}^{\ 2}}$$ Eq 5.7d Norton

compare σ' to S_Y

σ' to S_{UT}

normal stress and shear stress $\sigma_Y = 0$

shaft torsion bar

$$\sigma' = \sqrt{\sigma_{NORMAL}^{\ 2} + 3\,\tau_{SHEAR}^{\ 2}}$$

cannot compare τ to S_Y or S_{UT}

normal stress and shear stress (round shaft with bending moment M and torsional moment T)

$$\sigma' = \sqrt{\sigma_{BENDING}^{\ 2} + 3\,\tau_{TORSION}^{\ 2}} \qquad \sigma = \frac{M\,c}{I} \qquad \tau = \frac{T\,c}{J} \qquad c = \frac{d}{2} \qquad I = \frac{\pi d^4}{64} \qquad J = \frac{\pi d^4}{32}$$

$$\sigma' = \sqrt{\left(\frac{M\,c}{I}\right)^2 + 3\left(\frac{T\,c}{J}\right)^2} = \sqrt{\left(\frac{64M\,(d/2)}{\pi d^4}\right)^2 + 3\left(\frac{32T\,(d/2)}{\pi d^4}\right)^2} = \frac{32}{\pi d^3}\sqrt{M^2 + \frac{3}{4}T^2}$$

$$\sigma' = \frac{32}{\pi d^3}\sqrt{M^2 + \frac{3}{4}T^2}$$

biaxial normal stress (thin wall pressure vessel) $\tau_{XY} = 0$

$$\sigma' = \sqrt{\sigma_{TANGENTIAL}^{\ 2} + \sigma_{AXIAL}^{\ 2} - \sigma_{TANGENTIAL}\,\sigma_{AXIAL}}$$

pure shear (direct shear, key shear, shaft with no bending) $\sigma_X = \sigma_Y = 0$

$$\sigma' = \sqrt{3}\,\tau_{SHEAR}$$

cannot compare τ to S_Y or S_{UT}

brittle materials (cast iron, ceramics)

maximum tensile failure theory

$\sigma' \neq \tilde{\sigma}$

Dowling equivalent stress $\tilde{\sigma}$

1) find principal normal stresses using Mohr's circle $\sigma_1 \quad \sigma_2 \quad \sigma_3$

2) calculate Dowling constants $C_1 \quad C_2 \quad C_3$ using Eq. 5.12c Norton $S_{UT} > 0 \qquad S_{UC} < 0$

pos neg

$$C_1 = \frac{1}{2}\left[|\sigma_1 - \sigma_2| + \boxed{\frac{2\,S_{UT} - |S_{UC}|}{-|S_{UC}|}}(\sigma_1 + \sigma_2) \right]$$

$$C_2 = \frac{1}{2}\left[|\sigma_2 - \sigma_3| + \frac{2\,S_{UT} - |S_{UC}|}{-|S_{UC}|}(\sigma_2 + \sigma_3) \right]$$

$$C_3 = \frac{1}{2}\left[|\sigma_3 - \sigma_1| + \frac{2\,S_{UT} - |S_{UC}|}{-|S_{UC}|}(\sigma_3 + \sigma_1) \right]$$

$|S_{UC}| \approx 3\,|S_{UT}|$

3) find maximum

$\tilde{\sigma} = \mathrm{MAX}(\, C_1 \; C_2 \; C_3 \; \sigma_1 \; \sigma_2 \; \sigma_3 \,) \qquad \tilde{\sigma} = 0 \quad \text{if} \quad \mathrm{MAX} < 0$

4) compare Dowling equivalent stress to ultimate tensile strength

$N = S_{UT} / \tilde{\sigma}$

overhang

$P = T\,\omega$ ω must be rad/time NOT rev/time

$$T = P / \omega = 1\ \text{HP}\left(\frac{33000\ \text{ft.lbf}}{\text{HP.min}}\right)\left(\frac{\text{min}}{400\ \text{rev}}\right)\left(\frac{\text{rev}}{2\pi\ \text{rad}}\right)\left(\frac{12\ \text{in}}{\text{ft}}\right) = 157.6\ \text{in.lbf}$$

#41 ANSI chain, pitch p = 0.5 inch, maximum working load = 314 lbf, McMaster-Carr

pitch circumference = $2\,\pi\, r_{SPR} \approx (9T)\,p$
$r_{SPR} \approx (9T)\,p / 2\,\pi = 0.7162$ in

$\alpha = 360° / \text{number of teeth} = 40°$
$p = 0.5$ in
$\sin \alpha/2 = (p/2) / r_{SPR}$
EXACT $r_{SPR} = (p/2) / (\sin \alpha/2) = 0.731$ in

$T = F\, r_{SPR}$ $F = T / r_{SPR} = 220$ lbf

bending moment $M = F\,L = 165$ in.lbf

torsion moment $T = 157.6$ in.lbf

$I = \pi\, d^4 / 64 = 3.068 \times 10^{-3}\ \text{in}^4$ $J = \pi\, d^4 / 32 = 6.136 \times 10^{-3}\ \text{in}^4$

$c = d / 2 = 0.25$ in

1 ksi = 1000 psi

$$\sigma_{NOM} = M\,c / I = \frac{(165\ \text{in.lbf})(0.25\ \text{in})}{(3.068\text{x}10^{-3}\ \text{in}^4)} = 13.45\ \text{ksi}$$

1 ksi = 1 kpsi

$$\tau_{NOM} = T\,c / J = \frac{(157.6\ \text{in.lbf})(0.25\ \text{in})}{(6.136\text{x}10^{-3}\ \text{in}^4)} = 6.421\ \text{ksi}$$

maximum shear failure criterion (OLD)

$\sigma_x = 13.45$ ksi $\quad \sigma_y = 0 \quad \tau_{xy} = 6.421$ ksi

$$\tau_{MAX} = \sqrt{(\sigma_x / 2)^2 + \tau_{xy}^2} = 9.30 \text{ ksi}$$

1045 cold-rolled steel $\quad S_y = 77$ ksi $\quad$ Table A-9 Norton

$$N = \frac{0.5\, S_y}{\tau_{MAX}} = 4.14$$ Eq 5.10 and 5.11 Norton

von Mises failure criterion

$\sigma_x = 13.45$ ksi $\quad \sigma_y = 0 \quad \tau_{xy} = 6.421$ ksi

$$\sigma' = \sqrt{\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3\tau_{xy}^2} = 17.45 \text{ ksi}$$ Eq 5.7d Norton

1045 cold-rolled steel $\quad S_y = 77$ ksi $\quad$ Table A-9 Norton

$$N = \frac{S_y}{\sigma'} = 4.41$$ Eq 5.8a Norton

iterative solution for new diameter

$$\sigma_{NOM} = M\, c / I = \frac{M \frac{d}{2} 64}{\pi d^4} = \frac{32\, M}{\pi d^3} \qquad \tau_{NOM} = T\, c / J = \frac{T \frac{d}{2} 32}{\pi d^4} = \frac{16\, T}{\pi d^3}$$

try NEW d = 0.625 in

$$\text{NEW } \sigma' = \text{OLD } \sigma' \left(\frac{0.5}{0.625}\right)^3 = 0.512 \text{ OLD } \sigma'$$

static stress concentration factors

shaft bending $\quad \boxed{D/d = 1.5} \quad A = 0.93836 \quad b = -0.25759 \quad$ Figure C-2 Norton

$r/d = 0.1 \quad K_t = A(r/d)^b = 1.698$

$\sigma = K_t\, \sigma_{NOM} = 22.84$ ksi

shaft torsion D/d = 1.5 interpolated A = 0.8526 b = -0.2334 Figure C-3 Norton

r/d = 0.1 $K_t = A(r/d)^b = 1.459$

$\tau = K_t\, \tau_{NOM} = 9.368$ ksi

on-line calculator
https://www.amesweb.info/StressConcentrationFactor/SteppedShaftWithShoulderFillet.aspx

bending $K_t = 1.74$ torsion $K_t = 1.41$ different

maximum shear failure criterion (OLD)

$\sigma_x = 22.84$ ksi $\sigma_y = 0$ $\tau_{xy} = 9.368$ ksi

$$\tau_{MAX} = \sqrt{(\sigma_x/2)^2 + \tau_{xy}^2} = 14.77 \text{ ksi}$$

1045 cold-rolled steel $S_y = 77$ ksi Table A-9 Norton

$$N = \frac{0.5\, S_y}{\tau_{MAX}} = 2.61$$ Eq 5.10 and 5.11 Norton

von Mises failure criterion

$\sigma_x = 22.84$ ksi $\sigma_y = 0$ $\tau_{xy} = 9.368$ ksi

$$\sigma' = \sqrt{\sigma_x^2 + \sigma_y^2 - \sigma_x \sigma_y + 3\tau_{xy}^2} = 28.02 \text{ ksi}$$ Eq 5.7d Norton

1045 cold-rolled steel $S_y = 77$ ksi Table A-9 Norton

$$N = \frac{S_y}{\sigma'} = 2.75$$ Eq 5.8a Norton

key length

assume 1020 hot-rolled $S_y = 30$ ksi Table A-9 Norton

d = 0.5 inch DIA shaft w = 0.125 inch square key Table 10-2 Norton

assume L_{KEY} = 0.625 inch < L overhang

T = 157.6 in.lbf r_{SHAFT} = 0.25 inch $F_{KEY} = T / r_{SHAFT}$ = 630.4 lbf

$A_{SHEAR} = w\ L = 0.078125\ in^2$ $\tau = F_{KEY} / A_{SHEAR}$ = 8069.1 psi

$\sigma' = \sqrt{3}\ \tau$ = 13.98 ksi

$N_{YIELD} = S_Y / \sigma'$ = 2.15

<u>fatigue stress concentration (notch sensitivity) factors</u>

full reversed bending σ_{NOM} = 13.45 ksi K_t = 1.698

1045 cold-rolled steel S_{ut} = 91 ksi Table A-9 Norton

Neuber $\sqrt{a}$ = 0.0692 $\sqrt{in}$ interpolated Table 6-6 Norton

$$q = \frac{1}{1+\frac{\sqrt{a}}{\sqrt{r}}} = \frac{1}{1+\frac{0.0692\sqrt{in}}{\sqrt{0.05\ in}}} = 0.7637$$ Eq 6.13 Norton

$K_f = 1 + q\ (Kt - 1)$ = 1.533 Eq 6.11b Norton

$\sigma = K_f\ \sigma_{NOM}$ = 20.62 ksi

$\sigma_{alt}' = \sigma$ = 20.62 ksi

constant torsion τ_{NOM} = 6.421 ksi K_t = 1.459

no fatigue stress concentration (notch sensitivity) factor $\tau = K_t\ \tau_{NOM}$ = 9.368 ksi

$\sigma_{mean}' = \sqrt{3}\ \tau$ = 16.23 ksi Eq 5.7d Norton

<u>modified endurance limit</u>

1045 cold-rolled steel S_{ut} = 91 ksi Table A-9 Norton

$S_e' = 0.5\ S_{ut}$ = 45.5 ksi Eq 6.5a Norton

C_{LOAD} = 1.0 bending Eq 6.7a Norton

$C_{SIZE} = 0.869\ d^{-0.097} = 0.9294$ circular section Eq 6.7b Norton

$C_{SURF} = 0.76$ machined Figure 6-26 Norton

$C_{SURF} = A(S_{ut})^b = 0.817$ $A = 2.7$ $b = -0.265$ machined Eq 6.7e and Table 6-3 Norton

use $C_{SURF} = 0.76$

$C_{TEMP} = 1.0$ normal environmental temperature range Eq 6.7f Norton

$C_{RELI} = 0.814$ $R = 99\%$ Table 6-4 Norton

$S_e = C_{LOAD}\ C_{SIZE}\ C_{SURF}\ C_{TEMP}\ C_{RELI}\ S_e' = (1)\ (0.9294)\ (0.76)\ (1)\ (0.814)\ 45.5\ \text{ksi} = 26.16\ \text{ksi}$

<u>fatigue factor of safety</u>

$$\left(\frac{400\ \text{rev}}{\text{min}}\right)\left(\frac{60\ \text{min}}{\text{hr}}\right)\left(\frac{24\ \text{hr}}{\text{day}}\right) = 576{,}000\ \text{rev/day}$$

use infinite life $N>10^6$ $S_N = S_e = 26.16$ ksi $S_{ut} = 91$ ksi

$\sigma_{alt}' = 20.62$ ksi $\sigma_{mean}' = 16.23$ ksi

$N_{alt} = S_N / \sigma_{alt}' = 1.269$ $N_{mean} = S_{ut} / \sigma_{mean}' = 5.607$

$N_{GOODMAN} = N_{alt}\ N_{mean} / (N_{alt} + N_{mean}) = 1.03$

1045 cold-rolled steel $S_y = 77$ ksi Table A-9 Norton

$N_{FIRST} = S_y / (\sigma_{alt}' + \sigma_{mean}') = 2.09$

A ball mount bracket for gas springs is made from AISI 1010 hot rolled steel as shown below. Determine vertical load F on the ball that would cause static yielding.

$Pa = \frac{N}{m^2}$

$MPa = \frac{N}{mm^2}$

w = 50.8 mm t = 2 mm a = 12.7 mm

AISI 1010 hot-rolled steel S_y = 179 MPa Table A-9 Norton

$$\sigma = \frac{Mc}{I} + \frac{F}{A}$$ at front face

c = t /2 = 1 mm I = w t^3 / 12 = 33.87 mm^4 A = w t = 101.6 mm^2 (a + t/2) = 13.7 mm

use $\sigma = S_y$ for yield

$$S_y = F\left(\frac{(a + t/2)c}{I} + \frac{1}{A}\right)$$

$$179\frac{N}{mm^2} = F\left(\frac{(13.7\text{ mm})(1\text{ mm})}{33.87\text{ mm}^4} + \frac{1}{101.6\text{ mm}^2}\right) = F(0.4045 + 0.009843)\frac{1}{mm^2}$$

F = 432.0 N = 97.12 lbf

Rockwell C 52

Class 50 cast iron bar mounted with two 0.25 inch DIA dowel pins (A8 steel hardness HRC52)

values shown in red are for 0.5 inch DIA dowel pins

bar S_{UT} = 52 ksi Table A-7 Norton
S_{UC} = -164 ksi

pins S_Y = 225 ksi Table A-10 Norton

free body diagram

direct shear on right pin

for 0.25 in DIA pins

for 0.5 in DIA pins

$A = \pi d^2 / 4 = 0.0491$ in^2 — 0.1963 in^2

$\tau = F_R / A = 30.55$ ksi — 7.639 ksi

$\sigma' = \sqrt{3}\ \tau = 52.91$ ksi — 13.23 ksi

$N = S_Y / \sigma' = 4.25$ — 17.00

bending of bar at top A

maximum M at right pin M = (500 lbf) (4 in) = 2000 in.lbf

$I = t\,(h^3 - d^3) / 12 = 0.0205\ \text{in}^4$ $\quad$ 0.01823 in^4

$c = h / 2 = 0.5$ in

$\sigma = M\,c / I = 48.78$ ksi $\quad$ 54.85 ksi

$\tilde{\sigma} = \sigma$

$\tilde{\sigma} = \sigma$

$N = S_{UT} / \tilde{\sigma} = 1.07$ $\quad$ 0.95

direct crushing of bar above right pin B

assume tight fit $\quad A_{PROJ} = d\,t = 0.0625\ \text{in}^2$ $\quad$ Section 4.8 Norton $\quad$ 0.125 in^2

normal

$\sigma_{CRUSH} = F_R / A_{PROJ} = -24.00$ ksi $\quad$ compressive $\quad$ -12.00 ksi

bending of bar above right pin B

$c = d / 2 = 0.125$ in $\quad$ same M $\quad$ same I $\quad$ 0.25

$\sigma_{BEND} = M\,c / I = +12.20$ ksi $\quad$ tension $\quad$ +27.43 ksi

Dowling equivalent stress $\quad$ Eq. 5.12c Norton

$\sigma_1 = +12.20$ ksi $\quad \sigma_2 = 0 \quad \sigma_3 = -24.00$ ksi $\quad$ 27.43 ksi $\quad$ 0 $\quad$ -12.00 ksi

$S_{UT} = 52$ ksi $\quad S_{UC} = -164$ ksi

$$\frac{2\,S_{UT} - |S_{UC}|}{-|S_{UC}|} = 0.3659$$

$$C_1 = \frac{1}{2}\left[\,|\sigma_1 - \sigma_2| + \frac{2\,S_{UT} - |S_{UC}|}{-|S_{UC}|}(\sigma_1 + \sigma_2)\,\right] = +8.33\ \text{ksi}$$ $\quad$ 18.73 ksi

$$C_2 = \frac{1}{2}\left[\,|\sigma_2 - \sigma_3| + \frac{2\,S_{UT} - |S_{UC}|}{-|S_{UC}|}(\sigma_2 + \sigma_3)\,\right] = +7.61\ \text{ksi}$$ $\quad$ 3.80 ksi

$\sigma_3 - \sigma_1 = -24 - 12.2$

$-24 + 12.2$

$$C_3 = \frac{1}{2}\left[\overset{+36.3}{|\sigma_3 - \sigma_1|} + \underbrace{\boxed{\frac{2\,S_{UT} - |S_{UC}|}{-|S_{UC}|}}}_{-11.8}(\sigma_3 + \sigma_1) \right] = +15.94 \text{ ksi}$$

22.54 ksi

$\tilde{\sigma}$

$\tilde{\sigma} = \text{MAX}(\, C_1\ C_2\ C_3\ \sigma_1\ \sigma_2\ \sigma_3\,) = +15.94$ ksi Note: not MAX(abs( )) 27.43 ksi

$N = S_{UT} / \tilde{\sigma} = 3.26$ 1.90