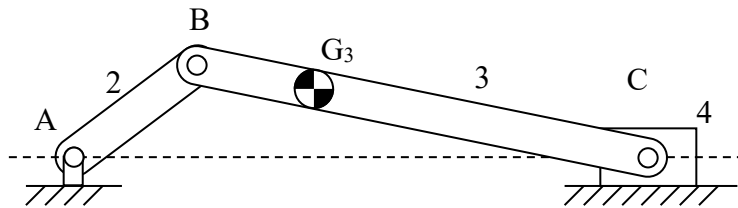
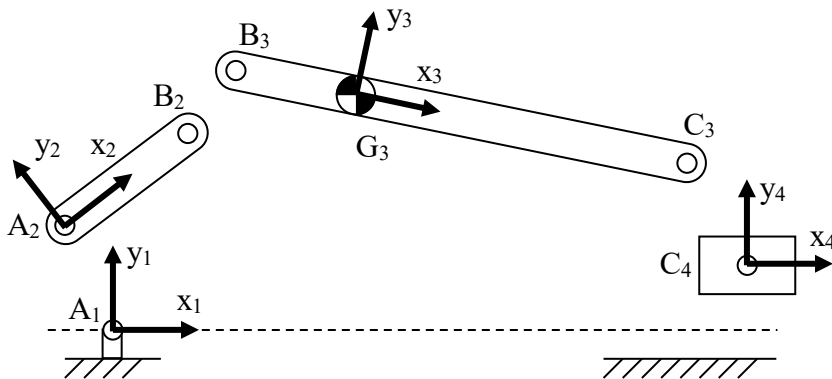


Use generalized coordinates $\{q\}$ and joint constraints $\{\Phi\}$ for the slider crank shown below.

$$\{q\} = \begin{Bmatrix} x_2 \\ y_2 \\ \phi_2 \\ x_3 \\ y_3 \\ \phi_3 \\ x_4 \\ y_4 \\ \phi_4 \end{Bmatrix} = \begin{Bmatrix} \{r_2\}^G \\ \phi_2 \\ \{r_3\}^G \\ \phi_3 \\ \{r_4\}^G \\ \phi_4 \end{Bmatrix} \quad \{\Phi\} = \begin{Bmatrix} \{r_2\}^A - \{r_1\}^A \\ \{r_3\}^B - \{r_2\}^B \\ \{r_4\}^C - \{r_3\}^C \\ \phi_4 \\ y_4 \\ \phi_2 - \omega_2 t \end{Bmatrix}$$



- AB = R = 0.985 inch
- BC = L = 4.33 inch
- BG₃ = 1.1 inch
- G₂ is at A₂ (balanced crank)
- G₃ is on centerline of link 3
- G₄ is at C₄ (simple piston model)
- x₂ axis along centerline of link 2
- x₃ axis along centerline of link 3
- ω₂ = 1000 rpm CCW constant



BLUEPRINT INFORMATION

$$\begin{aligned} \{s_2\}^A &= \begin{Bmatrix} 0 \\ 0 \end{Bmatrix} & \{s_2\}^B &= \begin{Bmatrix} R \\ 0 \end{Bmatrix} & \{s_3\}^B &= \begin{Bmatrix} -BG_3 \\ 0 \end{Bmatrix} & \{s_3\}^C &= \begin{Bmatrix} L - BG_3 \\ 0 \end{Bmatrix} \\ \{s_4\}^C &= \begin{Bmatrix} 0 \\ 0 \end{Bmatrix} & \{r_1\}^A &= \begin{Bmatrix} 0 \\ 0 \end{Bmatrix} \end{aligned}$$

example for B3 $\{r_3\}^B = \{r_3\} + [A_3]\{s_3\}^B \quad [A_3] = \begin{bmatrix} \cos \phi_3 & -\sin \phi_3 \\ \sin \phi_3 & \cos \phi_3 \end{bmatrix}$

1) Evaluate residuals $\{\Phi\}$ for rough estimates of generalized coordinates $\{q\}$ at $t = 0.005$ sec shown below. Comment on the relative precision of $\{\Phi\}$ versus $\{q\}$. Attach hardcopy of code.

$$\{q\} = \begin{Bmatrix} 0 \text{ inch} \\ 0 \text{ inch} \\ 0.4363 \text{ rad } (25^\circ) \\ 2.0 \text{ inch} \\ 0.5 \text{ inch} \\ -0.1745 \text{ rad } (-10^\circ) \\ 5.0 \text{ inch} \\ 0 \text{ inch} \\ 0 \text{ rad } (0^\circ) \end{Bmatrix} \quad \{\Phi\} = \begin{Bmatrix} 0 \text{ in} \\ 0 \text{ in} \\ 0.0240 \text{ in} \\ 0.2747 \text{ in} \\ -0.1809 \text{ in} \\ 0.0609 \text{ in} \\ 0 \text{ rad} \\ 0 \text{ in} \\ -0.0873 \text{ rad} \end{Bmatrix}$$

2) Use geometric equations to determine better estimates for $\{q\}$ at time $t = 0.005$ sec. Then evaluate new residuals. Comment on precision of $\{q\}$ and $\{\Phi\}$ between parts 1) and 2). Attach hardcopy of code.

$$\{q\} = \begin{Bmatrix} 0 \text{ inch} \\ 0 \text{ inch} \\ \omega_2 t = 0.5236 \text{ rad} \\ 1.946 \text{ in} \\ 0.367 \text{ in} \\ -0.114 \text{ rad } (-6.53^\circ) \\ 5.155 \text{ in} \\ 0 \text{ inch} \\ 0 \text{ rad } (0^\circ) \end{Bmatrix} \quad \{\Phi\} = \begin{Bmatrix} 0 \text{ in} \\ 0 \text{ in} \\ 0.0001013 \text{ in} \\ -0.0004042 \text{ in} \\ -0.0000452 \text{ in} \\ 0.0003267 \text{ in} \\ 0 \text{ rad} \\ 0 \text{ in} \\ 0 \text{ rad} \end{Bmatrix}$$

$\omega_2 = 1000 \text{ rpm} = 104.72 \text{ rad/s}$
 $\phi_2 = \omega_2 t = 0.5236 \text{ rad} = 30^\circ$

 $\theta = \phi_2$
 $R \sin\theta = L \sin\phi \quad \phi = 6.53^\circ$
 $s = R \cos\theta + L \cos\phi = 5.115 \text{ in}$
 $\phi_3 = -\phi \quad x_4 = s$

 $x_3^G = R \cos\theta + (BG_3) \cos\phi = 1.946 \text{ in}$
 $y_3^G = R \sin\theta - (BG_3) \sin\phi = 0.367 \text{ in}$

3) Evaluate the Jacobian $[\Phi_q]$ for your better estimate of $\{q\}$ at $t = 0.005$ sec. Attach hardcopy of code.

$$[\Phi_q] = \begin{bmatrix} +1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & +1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ -1 & 0 & +0.4925 & +1 & 0 & -0.1251 & 0 & 0 & 0 \\ 0 & -1 & -0.8530 & 0 & +1 & -1.0929 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 & 0 & -0.3674 & +1 & 0 & 0 \\ 0 & 0 & 0 & 0 & -1 & -3.2090 & 0 & +1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & 0 & +1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 & +1 & 0 \\ 0 & 0 & +1 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$\det \text{ JAC} = -4.3019$

4) Use your code to perform a Newton-Raphson position solution at $t = 0.010$ sec. Calculate piston position x_4 and determinant of the Jacobian. Validate with geometric equations. Attach hardcopy of code.

$$x_4 \text{ (Newton-Raphson)} \quad \underline{4.7376 \text{ inch}} \quad \det[\Phi_q] \quad \underline{-4.2451}$$

$$x_4 \text{ (geometric)} \quad \underline{4.7376 \text{ inch}}$$

5) Compute piston velocity \dot{x}_4 and acceleration \ddot{x}_4 at $t = 0.010$ sec using a matrix solution with right-hand-side (RHS) vectors $\{v\}$ and $\{y\}$. Validate with geometric equations. Attach hardcopy of code.

$$\dot{x}_4 \text{ (matrix)} \quad \underline{-99.69 \text{ ips}} \quad \ddot{x}_4 \text{ (matrix)} \quad \underline{-4173 \text{ ips}^2}$$

$$\dot{x}_4 \text{ (geometric)} \quad \underline{-99.69 \text{ ips}} \quad \ddot{x}_4 \text{ (geometric)} \quad \underline{-4173 \text{ ips}^2}$$

EXTRA CREDIT

Place a loop around your solution for part 5) using $0 \leq t \leq 0.06$ sec and provide MATLAB graphs for piston position x_4 , velocity \dot{x}_4 and acceleration \ddot{x}_4 as functions of crank angle ϕ_2 .

Validate using results from geometric equations on the same MATLAB graphs.

EXTRA EXTRA CREDIT

Modify your slider crank code for part 5) to analyze the four bar in Notes_04_05. This should only require modifying the last three rows in your constraint vector, your Jacobian matrix and your acceleration RHS vector.

use	$\phi_2 = 65^\circ$	$\dot{\phi}_2 = 10 \text{ rad/sec CW}$	$\ddot{\phi}_2 = 2 \text{ rad/sec}^2 \text{ CCW}$
validation	$\phi_3 = 13.151^\circ$	$\dot{\phi}_3 = \underline{+3.9013 \text{ rad/sec}}$	$\ddot{\phi}_3 = +7.0627 \text{ rad/sec}^2$
	$\phi_4 = -65.173^\circ$	$\dot{\phi}_4 = -5.3533 \text{ rad/sec}$	$\ddot{\phi}_4 = \underline{+69.7682 \text{ rad/sec}^2}$

$$\text{use } \text{PHI}(9) = \text{phi2} - \text{phi2_start} - \text{w2}*t - \text{alpha2}*t*t/2$$

$$\text{qd_transpose} = \begin{matrix} 0 & 0 & -10.0000 & 251.4765 & -39.4096 & 3.9013 & 116.6046 & 53.9475 & -5.3533 \end{matrix}$$

$$\text{qdd_transpose} = \begin{matrix} 1.0\text{e}+003 * \\ 0 & 0 & 0.0020 & -1.7001 & -2.6150 & 0.0071 & -1.2309 & -1.3273 & 0.0698 \end{matrix}$$

$$\text{qdd}(6) = 7.0627$$

$$\text{qdd}(9) = 69.7682$$

```

q_new_transpose =
    0         0    1.0472    1.5709    0.6363   -0.1983    4.7376         0         0

det_JAC = -4.2451

sGEO = 4.7376

vGEO = -99.6932

aGEO = -4.1730e+003

qd_transpose =
    0         0   104.7198   -91.9624    38.4724   -12.1491   -99.6932         0         0

qdd_transpose =
    1.0e+003 *
    0         0         0   -5.0889   -6.9781    2.1739   -4.1730         0         0

+++++

% h06.m - ME 481 H06 - joint constraint matrices
% HJSIII, 20.03.04

% constants
d2r = pi / 180;
Rmat = [ 0 -1 ;
         1 0 ];

% blueprint information - units [inch]
R = 0.985;
L = 4.33;
BG3 = 1.1;
r1A = [ 0     0 ]';
s2pA = [ 0     0 ]';
s2pB = [ R     0 ]';
s3pB = [ -BG3  0 ]';
s3pC = [ L-BG3 0 ]';
s4pC = [ 0     0 ]';

% crank speed = 1000 rpm CCW
w2 = +1000 * 2 * pi /60; % [rad/sec]

% initial estimates for generalized coordinates
q = [ 0 0 25*d2r 2.0 0.5 -10*d2r 5.0 0 0 ]'; % rough, t=0.005
q = [ 0 0 30*d2r 1.946 0.367 -6.53*d2r 5.155 0 0 ]'; % manual, t=0.005
%t = 0.005; % part 1, 2, 3
t = 0.010; % part 4

% Newton-Raphson iteration loop
for iter = 1 : 10,

% generalized coordinates
r2 = q(1:2);
phi2 = q(3);
r3 = q(4:5);
phi3 = q(6);
r4 = q(7:8);
phi4 = q(9);

% transformation matrices
A2 = [ cos(phi2)  -sin(phi2) ;
       sin(phi2)   cos(phi2) ];

A3 = [ cos(phi3)  -sin(phi3) ;
       sin(phi3)   cos(phi3) ];

A4 = [ cos(phi4)  -sin(phi4) ;
       sin(phi4)   cos(phi4) ];

% revolute points
r2A = r2 + A2 * s2pA;
r2B = r2 + A2 * s2pB;
r3B = r3 + A3 * s3pB;
r3C = r3 + A3 * s3pC;
r4C = r4 + A4 * s4pC;

```

```

% evaluate constraints
y4 = r4(2);

% fill constraint vector
PHI = [ r2A-r1A ;
        r3B-r2B ;
        r4C-r3C ;
        phi4 ;
        y4 ;
        phi2-w2*t ];
PHI_transpose = PHI'

% Jacobian
B2 = Rmat * A2;
B3 = Rmat * A3;
B4 = Rmat * A4;
JAC = zeros(9,9);
JAC(1:2,1:3) = [ +eye(2) +B2*s2pA ];
JAC(3:4,1:6) = [ -eye(2) -B2*s2pB +eye(2) +B3*s3pB ];
JAC(5:6,4:9) = [ -eye(2) -B3*s3pC +eye(2) +B4*s4pC ];
JAC(7,9) = 1;
JAC(8,8) = 1;
JAC(9,3) = 1;
JAC

% one step of Newton-Raphson
q = q - inv(JAC)*PHI;
q_new_transpose = q'

pause

% bottom - for iter
end

det_JAC = det( JAC )

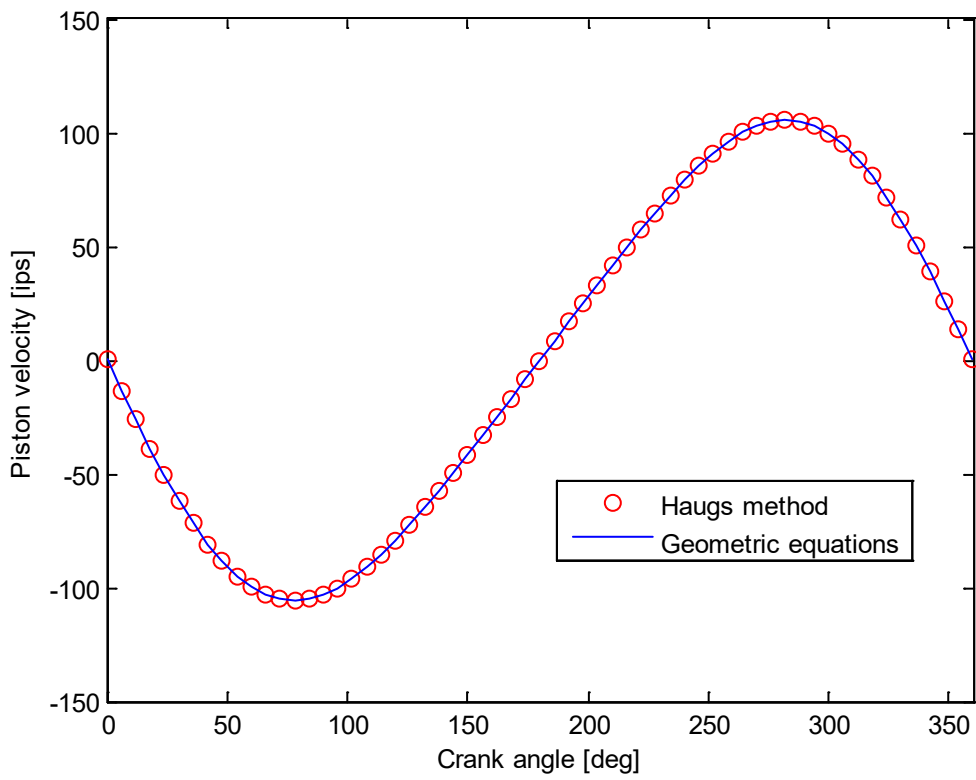
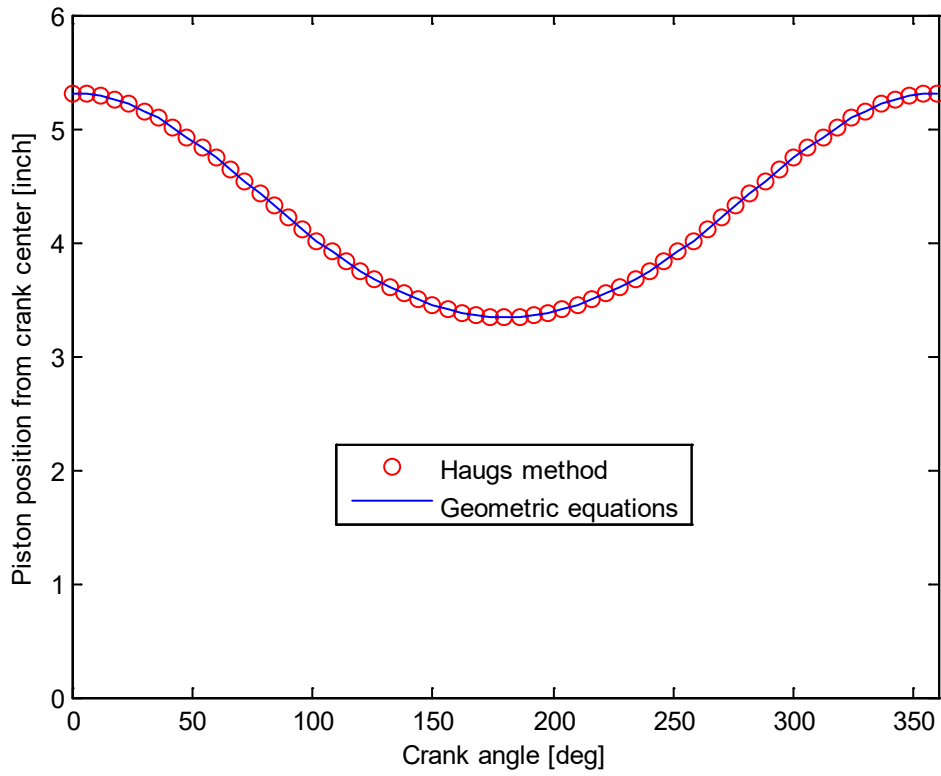
% geometric equations
th = phi2;
thdot = w2;
thddot = 0;
phi = asin( R*sin(th) / L );
sGEO = R*cos(th) + L*cos(phi)
phidot = R*thdot*cos(th) /L ./cos(phi);
vGEO = -R*thdot*sin(th) - L*phidot*sin(phi)
phiddot = ( R*thddot*cos(th) -R*thdot*thdot*sin(th) +L*phidot*phidot*sin(phi) ) ...
           /L ./cos(phi);
aGEO = -R*thddot*sin(th) -R*thdot*thdot*cos(th) -L*phiddot*sin(phi) ...
        -L*phidot*phidot*cos(phi)

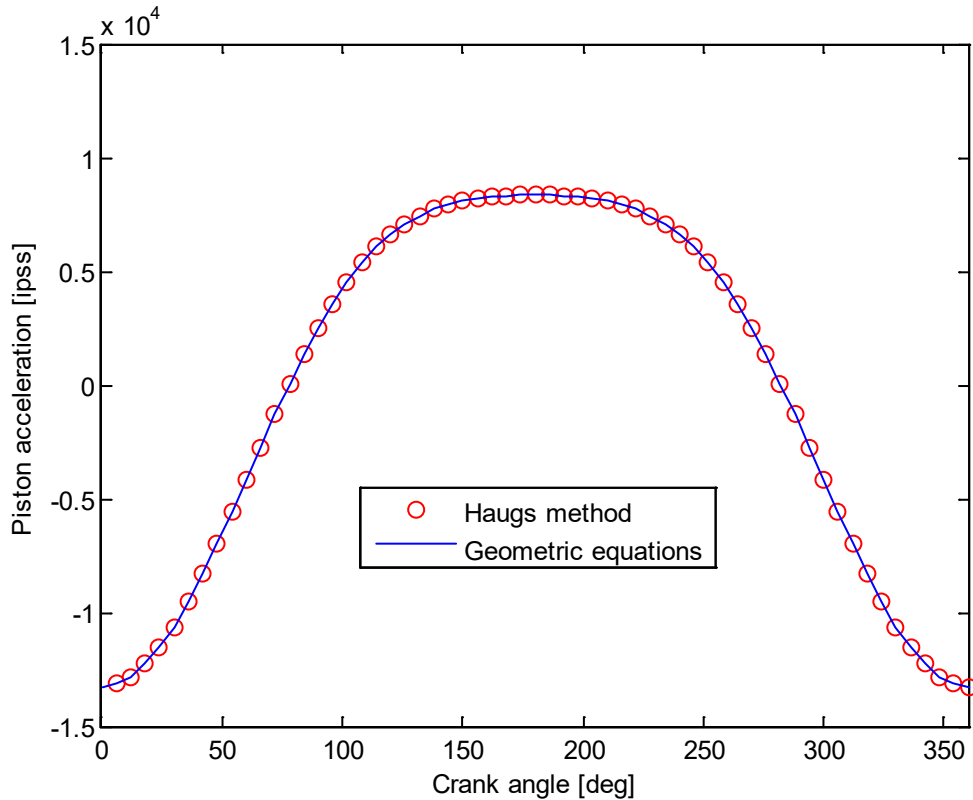
% matrix velocity
vel_rhs = zeros(9,1);
vel_rhs(9) = w2;
qd = inv(JAC) * vel_rhs;
qd_transpose = qd'

% matrix acceleration
phi2d = qd(3);
phi3d = qd(6);
acc_rhs = zeros(9,1);
acc_rhs(1:2) = phi2d*phi2d*A2*s2pA;
acc_rhs(3:4) = phi3d*phi3d*A3*s3pB - phi2d*phi2d*A2*s2pB;
acc_rhs(5:6) = -phi3d*phi3d*A3*s3pC;
qdd = inv(JAC) * acc_rhs;
qdd_transpose = qdd'

% bottom - h06

```





```

% h06_ec.m - ME 481 H06 - joint constraint matrices - extra credit
% HJSIII, 13.02.07

% constants
d2r = pi / 180;
Rmat = [ 0 -1 ;
        1 0 ];

% blueprint information - units [inch]
R = 0.985;
L = 4.33;
BG3 = 1.1;
r1A = [ 0 0 ]';
s2pA = [ 0 0 ]';
s2pB = [ R 0 ]';
s3pB = [ -BG3 0 ]';
s3pC = [ L-BG3 0 ]';
s4pC = [ 0 0 ]';

% crank speed = 1000 rpm CCW
w2 = +1000 * 2 * pi / 60; % [rad/sec]

% initial estimates for generalized coordinates
q = [ 0 0 25*d2r 2.0 0.5 -10*d2r 5.0 0 0 ]'; % rough, t=0.005
q = [ 0 0 30*d2r 1.946 0.367 -6.53*d2r 5.155 0 0 ]'; % manual, t=0.005

% t = 0.005; % part 1, 2, 3
% t = 0.010; % part 4

% time loop
keep = [];
for t = 0 : 0.001 : 0.060,

% Newton-Raphson iteration loop
for iter = 1 : 10,

% generalized coordinates
r2 = q(1:2);

```

```

phi2 = q(3);
r3 = q(4:5);
phi3 = q(6);
r4 = q(7:8);
phi4 = q(9);

% transformation matrices
A2 = [ cos(phi2)  -sin(phi2) ;
      sin(phi2)   cos(phi2) ];

A3 = [ cos(phi3)  -sin(phi3) ;
      sin(phi3)   cos(phi3) ];

A4 = [ cos(phi4)  -sin(phi4) ;
      sin(phi4)   cos(phi4) ];

% revolute points
r2A = r2 + A2 * s2pA;
r2B = r2 + A2 * s2pB;
r3B = r3 + A3 * s3pB;
r3C = r3 + A3 * s3pC;
r4C = r4 + A4 * s4pC;

% evaluate constraints
y4 = r4(2);

% fill constraint vector
PHI = [ r2A-r1A ;
        r3B-r2B ;
        r4C-r3C ;
        phi4 ;
        y4 ;
        phi2-w2*t ];

% Jacobian
B2 = Rmat * A2;
B3 = Rmat * A3;
B4 = Rmat * A4;
JAC = zeros(9,9);
JAC(1:2,1:3) = [ +eye(2)  +B2*s2pA ];
JAC(3:4,1:6) = [ -eye(2)  -B2*s2pB  +eye(2)  +B3*s3pB ];
JAC(5:6,4:9) = [           -eye(2)  -B3*s3pC  +eye(2)  +B4*s4pC ];
JAC(7,9) = 1;
JAC(8,8) = 1;
JAC(9,3) = 1;

% one step of Newton-Raphson
q = q - inv(JAC)*PHI;

% bottom - for iter
end

% geometric equations
th = phi2;
thdot = w2;
thddot = 0;
phi = asin( R*sin(th) / L );
sGEO = R*cos(th) + L*cos(phi);

phidot = R*thdot*cos(th) /L /cos(phi);
vGEO = -R*thdot*sin(th) - L*phidot.*sin(phi);

phiddot = ( R*thddot*cos(th) -R*thdot*thdot*sin(th) +L*phidot*phidot*sin(phi) ) ...
           /L /cos(phi);
aGEO = -R*thddot*sin(th) -R*thdot*thdot*cos(th) -L*phiddot*sin(phi) ...
        -L*phidot*phidot*cos(phi);

% matrix velocity
vel_rhs = zeros(9,1);
vel_rhs(9) = w2;
qd = inv(JAC) * vel_rhs;

% matrix acceleration
phi2d = qd(3);
phi3d = qd(6);

```



```
acc_rhs = zeros(9,1);
acc_rhs(1:2) = phi2d*phi2d*A2*s2pA;
acc_rhs(3:4) = phi3d*phi3d*A3*s3pB - phi2d*phi2d*A2*s2pB;
acc_rhs(5:6) = -phi3d*phi3d*A3*s3pC;
qdd = inv(JAC) * acc_rhs;

% bottom - for t
keep = [ keep ; q(3) q(7) qd(7) qdd(7) sGEO vGEO aGEO ];
end

% plot results
th_deg = keep(:,1) / d2r;
sMAT = keep(:,2);
vMAT = keep(:,3);
aMAT = keep(:,4);
sGEO = keep(:,5);
vGEO = keep(:,6);
aGEO = keep(:,7);

figure( 1 )
plot( th_deg,sMAT,'ro', th_deg,sGEO,'b' )
axis( [ 0 360 0 6 ] )
xlabel( 'Crank angle [deg]' )
ylabel( 'Piston position from crank center [inch]' )
legend( 'Haug's method', 'Geometric equations' )

figure( 2 )
plot( th_deg,vMAT,'ro', th_deg,vGEO,'b' )
axis( [ 0 360 -150 150 ] )
xlabel( 'Crank angle [deg]' )
ylabel( 'Piston velocity [ips]' )
legend( 'Haug's method', 'Geometric equations' )

figure( 3 )
plot( th_deg,aMAT,'ro', th_deg,aGEO,'b' )
axis( [ 0 360 -15000 15000 ] )
xlabel( 'Crank angle [deg]' )
ylabel( 'Piston acceleration [ipss]' )
legend( 'Haug's method', 'Geometric equations' )

% bottom of h06_ec
```

```

% h06_ec_ec.m - ME 481 H06 - joint constraint matrices - extra extra credit
% HJSIII, 13.02.08

% constants
d2r = pi / 180;
Rmat = [ 0 -1 ;
         1 0 ];

% Notes_04_05 four bar
% blueprint information - units [cm]
AB = 30;
BC = 60;
CD = 45;
AD = 90;
BG3 = 23;
CG3 = BC - BG3;
DG4 = 24;
CG4 = CD - DG4;
r1A = [ 0 0 ]';
r1D = [ AD 0 ]';
s2pA = [ 0 0 ]';
s2pB = [ AB 0 ]';
s3pB = [ -BG3 0 ]';
s3pC = [ CG3 0 ]';
s4pC = [ -CG4 0 ]';
s4pD = [ DG4 0 ]';

% initial estimates for generalized coordinates
phi2 = 65 * d2r;
phi3 = 13.151 * d2r;
phi4 = -65.173 * d2r;

t = 0;
phi2_start = phi2; % 65 deg
w2 = -10; % 10 rad/sec CW
alpha2 = 2; % 2 rad/sec/sec CCW

xG3 = AB*cos(phi2) + BG3*cos(phi3);
yG3 = AB*sin(phi2) + BG3*sin(phi3);

xG4 = AB*cos(phi2) + BC*cos(phi3) + CG4*cos(phi4);
yG4 = AB*sin(phi2) + BC*sin(phi3) + CG4*sin(phi4);

q = [ 0 0 phi2 xG3 yG3 phi3 xG4 yG4 phi4 ]';

% Newton-Raphson iteration loop
for iter = 1 : 10,

% generalized coordinates
r2 = q(1:2);
phi2 = q(3);
r3 = q(4:5);
phi3 = q(6);
r4 = q(7:8);
phi4 = q(9);

% transformation matrices
A2 = [ cos(phi2) -sin(phi2) ;
       sin(phi2)  cos(phi2) ];

A3 = [ cos(phi3) -sin(phi3) ;
       sin(phi3)  cos(phi3) ];

A4 = [ cos(phi4) -sin(phi4) ;
       sin(phi4)  cos(phi4) ];

% revolute points
r2A = r2 + A2 * s2pA;
r2B = r2 + A2 * s2pB;
r3B = r3 + A3 * s3pB;
r3C = r3 + A3 * s3pC;
r4C = r4 + A4 * s4pC;
r4D = r4 + A4 * s4pD;

```

```

% fill constraint vector
PHI = [ r2A-r1A          ;
        r3B-r2B          ;
        r4C-r3C          ;
        r4D-r1D          ;
        phi2-phi2_start-w2*t-alpha2*t*t/2 ];

% Jacobian
B2 = Rmat * A2;
B3 = Rmat * A3;
B4 = Rmat * A4;
JAC = zeros(9,9);
JAC(1:2,1:3) = [ +eye(2) +B2*s2pA          ];
JAC(3:4,1:6) = [ -eye(2) -B2*s2pB +eye(2) +B3*s3pB ];
JAC(5:6,4:9) = [          -eye(2) -B3*s3pC +eye(2) +B4*s4pC ];
JAC(7:8,7:9) = [          +eye(2) +B4*s4pD ];
JAC(9,3) = 1;

% one step of Newton-Raphson
q = q - inv(JAC)*PHI;

phi_transpose = PHI'
qnew_transpose = q'
pause

% bottom - for iter
end

% matrix velocity
vel_rhs = zeros(9,1);
vel_rhs(9) = w2 + alpha2*t;
qd = inv(JAC) * vel_rhs;
qd_transpose = qd'

% matrix acceleration
phi2d = qd(3);
phi3d = qd(6);
phi4d = qd(9);
acc_rhs = zeros(9,1);
acc_rhs(1:2) = phi2d*phi2d*A2*s2pA;
acc_rhs(3:4) = phi3d*phi3d*A3*s3pB - phi2d*phi2d*A2*s2pB;
acc_rhs(5:6) = phi4d*phi4d*A4*s4pC - phi3d*phi3d*A3*s3pC;
acc_rhs(7:8) = phi4d*phi4d*A4*s4pD;
acc_rhs(9) = alpha2;
qdd = inv(JAC) * acc_rhs;
qdd_transpose = qdd'

% bottom of h06_ec_ec

```