

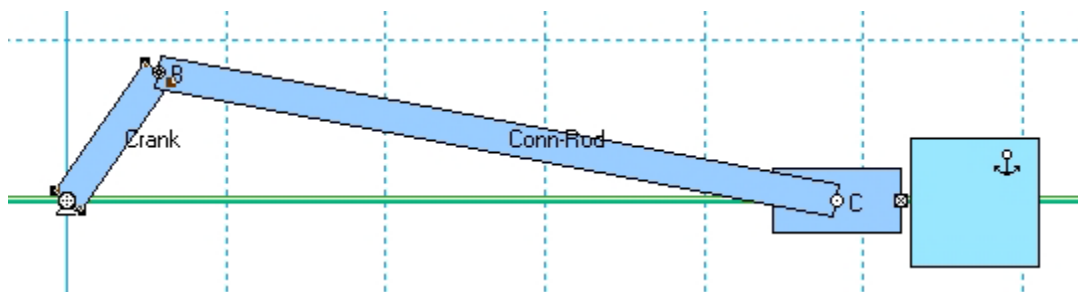
- 1) Modify your Working Model (WM) slider crank simulation as detailed below.
  - a) Change the motor that drives the crank to apply constant torque of 20 ft-lbf.
  - b) Place a large block so that the piston cannot move all the way to TDC.
  - c) Select World then Accuracy and set Animation Step to 0.0001 sec. You may also need to select World then Accuracy then More Choices and set Overlap Error smaller.
  - d) Left-click on the piston to highlight it. Hold down the Shift Key and left-click on the block to highlight it also. Select Object then Collide to enable collision between the two objects. Select Measure then Contact Force to measure piston force.
  - e) Move the block to three different positions and record piston force in the table below.
  - f) Validate your simulation with the closed-form force-torque equation derived in class.
  - g) Attach a screen shot of your WM mechanism.

Crank angle [deg]	Conn-rod angle [deg]	Crank torque [in.lbf]	WM piston force [lbf]	Equation piston force [lbf]
31.373	6.812	240	391.410	391.3519
85.882	13.118	240	240.255	240.2545
130.766	9.921	240	378.828	378.8317

$$T_{12} = \frac{P R \sin(\theta + \phi)}{\cos \phi} \quad P = \frac{T_{12} \cos \phi}{R \sin(\theta + \phi)}$$

### EXTRA CREDIT

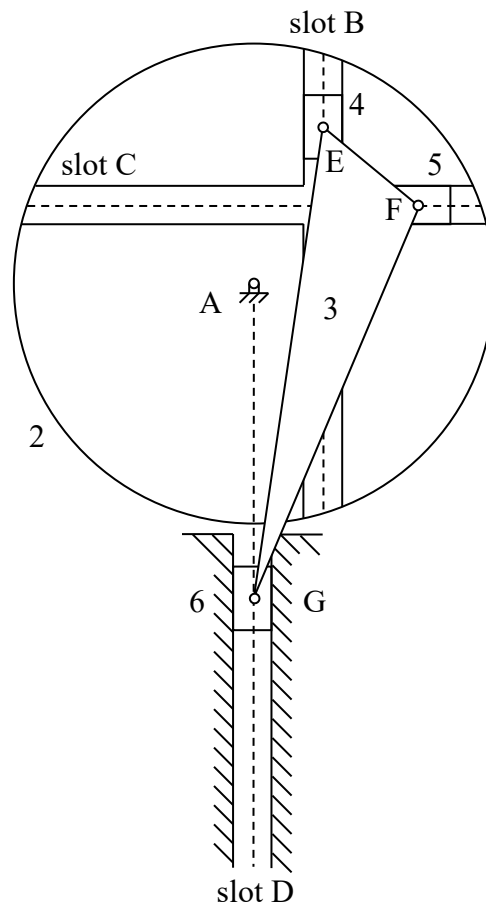
Develop a WM simulation to slowly move the block back and forth. Export WM data and read into MATLAB. Provide validation plots of WM piston force and closed-form equation piston force on the same MATLAB graph as a function of crank angle. Attach a screen shot of your WM mechanism.



2) Determine motor torque  $T_{12}$  required to push needle link 6 down with 0.5 N at the position shown below. The mechanism is drawn to scale full size. Neglect friction and dynamic effects.

Show your work.

$T_{12}$  7.36 N.mm CW instant centers  
7.69 N.mm CW WM  
7.603 N.mm CW Newtonian



from H05

$$\omega_2 = 4 \text{ rev/sec} = 8 \pi \text{ rad/sec}$$

actual power

$$T_{12} \circ \omega_2 + F_{\text{NEEDLE}} \circ V_{G6} = 0$$

graphical instant centers

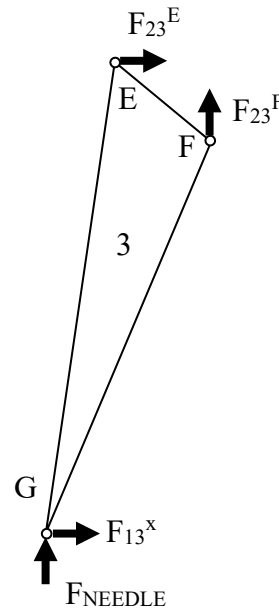
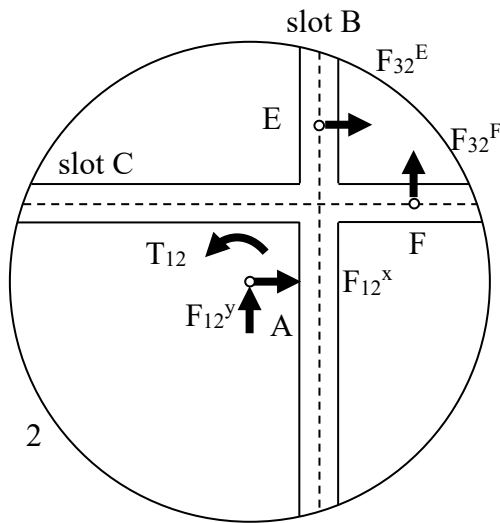
$$V_{G6} = 370 \text{ mmps down}$$

$$T_{12} = 7.36 \text{ N.mm CW}$$



remove each slider and replace with pin-in-slot

assume no friction



$$\begin{aligned} \Sigma F \text{ on 2 right} + & + F_{12}^x + F_{32}^E = 0 \\ \Sigma F \text{ on 2 up} + & + F_{12}^y + F_{32}^F = 0 \\ \Sigma M \text{ on 2 about A CCW} + & - F_{32}^E AE^y + F_{32}^F AF^x + T_{12} = 0 \end{aligned}$$

$$\begin{aligned} \Sigma F \text{ on 3 right} + & + F_{23}^E + F_{13}^x = 0 \\ \Sigma F \text{ on 3 up} + & + F_{23}^F + F_{NEEDLE} = 0 \\ \Sigma M \text{ on 3 about G CCW} + & - F_{23}^E GE^y + F_{23}^F GF^x = 0 \end{aligned}$$

using graphical measurements from drawing

$$AE^y = 20.6 \text{ mm} \quad AF^x = GF^x = 21.1 \text{ mm} \quad GE^y = 62.3 \text{ mm}$$

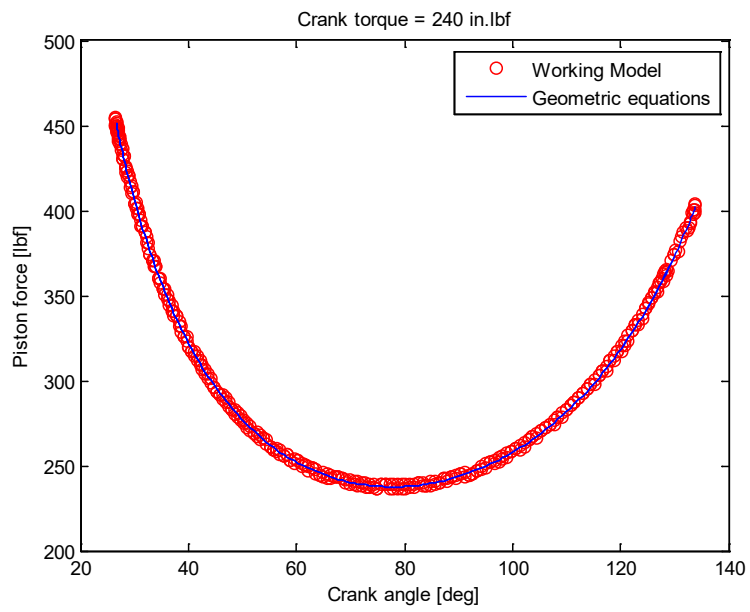
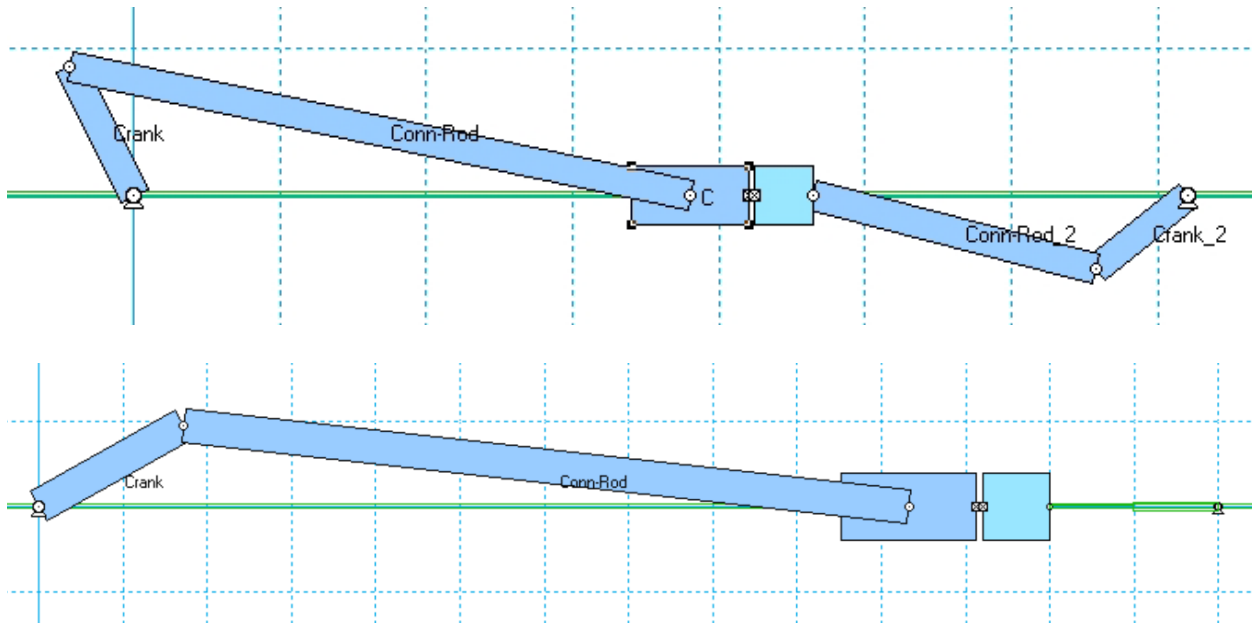
$$F_{NEEDLE} = 0.5 \text{ N}$$

$$\begin{aligned} \text{from } \Sigma F \text{ on 3 y} \quad F_{23}^F &= -0.5 \text{ N} & F_{32}^F &= +0.5 \text{ N} \\ \text{from } \Sigma M \text{ on 3} \quad F_{23}^E &= -0.169 \text{ N} & F_{32}^E &= +0.169 \text{ N} \\ \text{from } \Sigma M \text{ on 2} \quad T_{12} &= -7.068 \text{ N.mm} \end{aligned}$$

using exact measurements computed in H05

$$\begin{aligned} \{r\}^E &= \begin{Bmatrix} 10 \\ 19.9279 \end{Bmatrix} & \{r\}^F &= \begin{Bmatrix} 22.5473 \\ 10 \end{Bmatrix} & \{r\}^G &= \begin{Bmatrix} 0 \\ -41.2603 \end{Bmatrix} \\ AE^y &= 19.9279 \text{ mm} & AF^x = GF^x &= 22.5473 \text{ mm} & GE^y &= 61.1882 \text{ mm} \end{aligned}$$

$$\begin{aligned} \text{from } \Sigma M \text{ on 3} \quad F_{23}^E &= -0.1842 \text{ N} & F_{32}^E &= +0.1842 \text{ N} \\ \text{from } \Sigma M \text{ on 2} \quad T_{12} &= -7.6029 \text{ N.mm} \end{aligned}$$



```
% hw09_ec.m - ME 481 H09 - read WM data for slider crank and validate
% HJSIII, 11.03.14

% general constants
d2r = pi / 180;

% mechanism constants
R = 1.97 / 2;          % crank length [inch]
L = 4.33;             % conn-rod length [inch]
T12 = 240;           % crank torque [in.lbf]

% load WM data - note angles in degrees
load hw09_ec_cut.txt;

t = hw09_ec_cut(:,1);
th_deg = hw09_ec_cut(:,2);
phi_deg = -hw09_ec_cut(:,4);
P_WM = -hw09_ec_cut(:,6);

% crank information
th = th_deg * d2r;

% geometric equations
phi = asin( R*sin(th) / L );
P_geo = T12 * cos(phi) / R ./sin(th+phi);

% plot results
figure( 1 )
plot( th_deg,P_WM,'ro', th_deg,P_geo,'b' )
% axis( [ 0 360 0 6 ] )
xlabel( 'Crank angle [deg]' )
ylabel( 'Piston force [lbf]' )
legend( 'Working Model', 'Geometric equations' )
title( 'Crank torque = 240 in.lbf' )

% manual check
th_deg_manual = [ 31.373  85.882  130.766 ];
phi_deg_manual = [  6.812  13.118   9.921 ];
th = th_deg_manual * d2r;
phi = phi_deg_manual * d2r;
P_manual = T12 * cos(phi) / R ./sin(th+phi)

% bottom of hw09_ec.m
```