

# CONSERVATION OF MASS

In this lesson, we will:

- Use the Reynolds Transport Theorem to generate the **equation of conservation of mass for a control volume** and show some simplifications of this equation
- Discuss **mass flow rate** and **volume flow rate**
- Do some example problems

## Derivation of Conservation of Mass from the RTT

For a system  $\frac{dm_{sys}}{dt} = 0$  \*

Apply RTT: consider a fixed CV for simplicity

$$\frac{dB_{sys}}{dt} = \frac{d}{dt} \int_{CV} \rho b dV + \int_{CS} \rho b (\vec{V} \cdot \vec{n}) dA$$

Let  $B = m = \text{mass} \rightarrow b = \frac{B}{m} = \frac{m}{m} = 1$

$$\frac{dm_{sys}}{dt} = 0 = \frac{d}{dt} \int_{CV} \rho dV + \int_{CS} \rho (\vec{V} \cdot \vec{n}) dA \quad (1)$$

CONV. OF MASS FOR A SYSTEM

CONV. OF MASS EQ FOR A FIXED CV \*

rate of change of mass within the CV  
 $= \frac{d}{dt} m_{CV}$

net rate of mass flow out of the system through the CS

For steady flow, there is no net mass flow out of the CV \*

- If +
- If -
- If 0

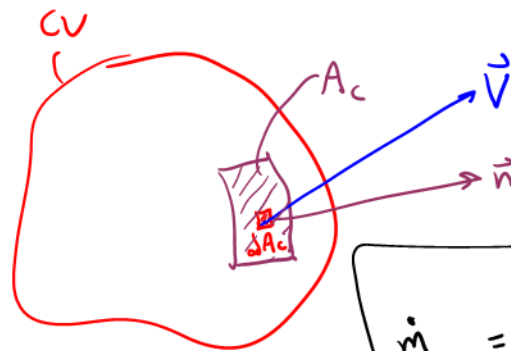
- +
- 
- 0

STEADY FLOW

- must be -
- must be +
- must be 0

## Mass Flow Rate

$$\{\dot{m}\} = \left\{ \frac{\text{mass}}{\text{time}} \right\}$$



$$\dot{m}_{A_c} = \int_{A_c} \rho (\vec{V} \cdot \vec{n}) dA_c$$

$\dot{m}_{A_c}$  = mass flow rate out of area  $A_c$



If mass flow rate is out,  $\vec{V} \cdot \vec{n} > 0$ ,  $\therefore \dot{m}_{A_c} > 0$

★ THIS IS AN OUTLET



If mass flow rate is in,  $\vec{V} \cdot \vec{n} < 0$ ,  $\therefore \dot{m}_{A_c} < 0$

★ THIS IS AN INLET

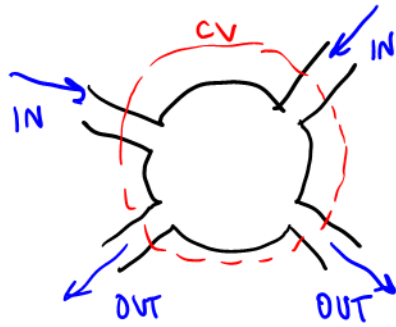
If  $A_c =$  entire CS, then

$$\dot{m}_{CS} = \int_{CS} \rho (\vec{V} \cdot \vec{n}) dA \quad (2)$$

2<sup>nd</sup> term in our cons of mass eq. for a CV (1)

THIS IS THE NET RATE OF MASS FLOW OUT OF THE CS ★

- Simplification : We usually have well defined inlets & outlets.  
So, we can split this integral of Eq. (2) into several parts, one for each inlet & outlet



$$\text{let } \dot{m}_{cs} = \sum_{\text{out}} \dot{m} - \sum_{\text{in}} \dot{m}$$

Where  $\dot{m}$  is  $\oplus$  for both inlets & outlets

Eg (1) becomes,

$$\frac{d}{dt} \int_{cv} \rho dV = \sum_{\text{in}} \dot{m} - \sum_{\text{out}} \dot{m}$$

or

$$\frac{d}{dt} M_{cv} = \sum_{\text{in}} \dot{m} - \sum_{\text{out}} \dot{m}$$

rate of change of mass within the CV

net rate of mass flow into the CV

Special simple case for Steady Flow

$$\frac{d}{dt} M_{cv} = 0$$

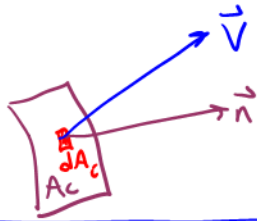
$\therefore$

$$\sum_{\text{in}} \dot{m} = \sum_{\text{out}} \dot{m} \quad \star$$

STEADY FLOW CONS. OF MASS FOR A FIXED CV

$\star$

## Volume Flow Rate



Define  $\dot{V}_{A_c} = \int_{A_c} (\vec{V} \cdot \vec{n}) dA_c = \text{volume flow rate out of area } A_c$

Notation:  $V$  = volume,  $\dot{V}$  = volume flow rate  
[ $m$  = mass,  $\dot{m}$  = mass flow rate]  
Some other authors use  $Q$  for volume flow rate

Average velocity (actually speed) through  $A_c$

$$V_{\text{avg}, A_c} = \frac{1}{A_c} \int_{A_c} (\vec{V} \cdot \vec{n}) dA_c = \dot{V}_{A_c}$$

$$V_{\text{avg}, A_c} = \frac{\dot{V}_{A_c}}{A_c} \star$$

Approximation for a given inlet or outlet

$$\dot{m}_{A_c} \approx \rho_{\text{avg}} \cdot V_{\text{avg}} A_c$$

or  $\dot{m}_{A_c} \approx \rho V A_c \star = \rho \dot{V}_{A_c}$

$$\dot{m}_{A_c} = \rho \dot{V}_{A_c} \star$$

• For incompressible flow ( $\rho \approx \text{const}$ )  
and steady, with well defined inlets & outlets

$$\sum_{\text{in}} \dot{m} = \sum_{\text{out}} \dot{m}$$

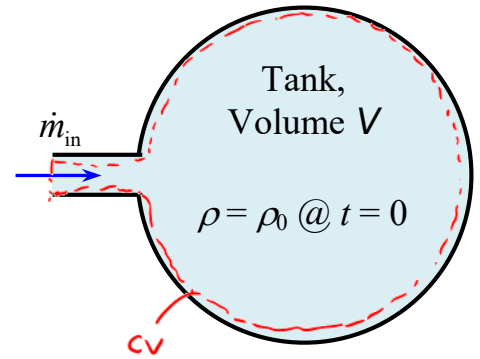
$$\sum_{\text{in}} [\cancel{\rho} \dot{V}] = \sum_{\text{out}} [\cancel{\rho} \dot{V}]$$

Incomp

$$\sum_{\text{in}} \dot{V} = \sum_{\text{out}} \dot{V}$$

### Example: Unsteady conservation of mass (flow into a tank)

**Given:** Air is pumped into a rigid tank of volume  $V$ . The mass flow rate of the air entering the tank is constant,  $\dot{m}_{in}$ . We assume that the process is slow enough that the air in the tank remains at the same temperature (isothermal conditions).



**To do:** Generate an equation for density  $\rho$  in the tank as a function of time.

**Solution:**

• Draw an appropriate C.V. ✘  
✘ ✘ ✘ ✘ ✘

• Cons. of mass eq.

$$\frac{d}{dt} \int_{CV} \rho dV = \sum_{in} \dot{m} - \sum_{out} \dot{m}$$

*no outlet*

• Assume  $\rho = \rho(t)$  only

$$\frac{d\rho}{dt} \int_{CV} dV = \dot{m}_{in}$$

$V$  ( $V$  is constant since the tank is rigid)

$$\frac{d\rho}{dt} = \frac{\dot{m}_{in}}{V} = \text{constant}$$

• Integrate from  $t=0$  where  $\rho = \rho_0$  to some later time  $t$

$$\int_{\rho_0}^{\rho} d\rho = \frac{\dot{m}_{in}}{V} \int_{t=0}^t dt$$

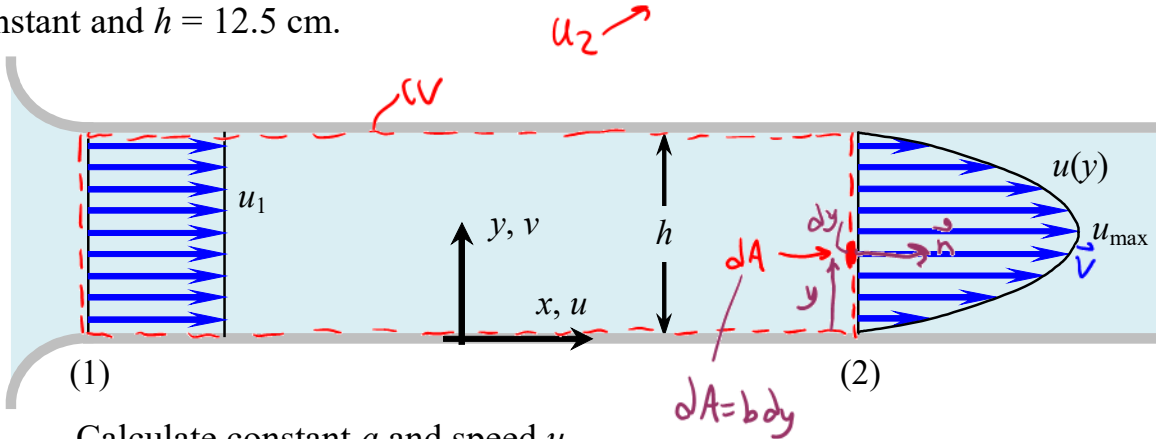
$$\rho - \rho_0 = \frac{\dot{m}_{in}}{V} (t - 0)$$

$$\rho = \rho_0 + \frac{\dot{m}_{in}}{V} t$$

### Example: Velocity profiles in 2-D channel flow

**Given:** Consider steady, incompressible, two-dimensional flow of a liquid between two very long parallel plates as sketched. At the inlet (1) there is a nice bell mouth, and the velocity is nearly uniform (except for a very thin, negligible boundary layer, not shown).

- At (1),  $u = u_1 = \text{constant} = 3.00 \text{ m/s}$ ,  $v = 0$ , and  $w = 0$ .
- At (2), the flow is fully developed, and  $u = ay(h - y)$ ,  $v = 0$ , and  $w = 0$ , where  $a$  is a constant and  $h = 12.5 \text{ cm}$ .



**To do:** Calculate constant  $a$  and speed  $u_{\max}$ .

**Solution:**

• Pick a wise control volume  $\star$

• Cons. of mass

Here - steady  
• incompressible

$[b = \text{width into the page}]$

$$\sum \dot{V}_{\text{in}} = \sum \dot{V}_{\text{out}}$$

only one (1)      only one (2)

$$u_1 b h = \int_{A_2} \vec{V} \cdot \vec{n} dA$$

$$u_1 b h = \int_{y=0}^h u_2 b dy$$

$(u_2, 0, 0) \cdot (1, 0, 0) = u_2$

$$a = 1150 \frac{1}{\text{ms}}$$

$$u_{\max} = 4.50 \text{ m/s}$$

$$u_1 b h = \int_{y=0}^h ay(h-y) dy$$

$$\text{or } u_{\max} = \frac{3u_1}{2}$$

$$u_1 b h = \frac{ah^3}{6} \rightarrow a = \frac{6u_1}{h^2} = \frac{6(3.00 \text{ m/s})}{(0.125 \text{ m})^2} = 1152 \frac{1}{\text{ms}} = a$$

$u_{\max}$  occurs @  $y = h/2$   $\rightarrow u_{\max} = a \frac{h}{2} (h - \frac{h}{2}) = a \frac{h^2}{4}$