

**Today, we will:**

- Continue our discussion about dimensional analysis with pumps
- Do an example problem – dimensional analysis with pumps; the affinity laws
- Discuss turbines

From previous lecture...dimensional analysis of pump parameters:

$$C_H = \text{function}(C_Q, \text{Re}, \varepsilon/D) \quad \text{and} \quad C_P = \text{function}(C_Q, \text{Re}, \varepsilon/D)$$

where

$$C_Q = \frac{\dot{V}}{\omega D^3} \quad C_H = \frac{gH}{\omega^2 D^2} \quad C_P = \frac{bhp}{\rho \omega^3 D^5}$$

Capacity coefficient      Head coefficient      Power coefficient

But for many pumps, effects of Re and roughness are small at high Re, and thus,

$$C_H \approx \text{function}(C_Q) \quad \text{and} \quad C_P \approx \text{function}(C_Q)$$

$$\eta_{\text{pump}} \rightarrow \eta_{\text{pump}} = \frac{\rho \dot{V} g H}{bhp}$$

$\dot{V} = \omega D^3 C_Q$

$gH = \omega^2 D^2 C_H$

$bhp = \rho \omega^3 D^5 C_P$

$$\therefore \eta_{\text{pump}} = \frac{\rho \omega D^3 C_Q \omega^2 D^2 C_H}{\rho \omega^3 D^5 C_P} = \frac{C_Q C_H}{C_P} = \eta_{\text{pump}}$$

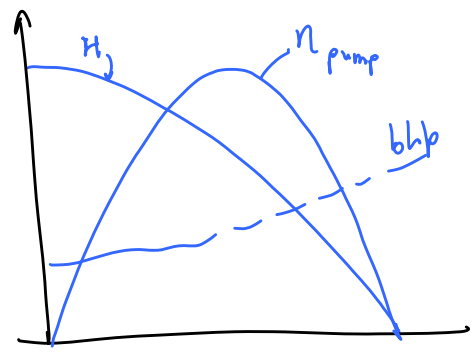
$$\therefore \eta_{\text{pump}} = \text{func}(C_Q) \quad \text{also}$$

## 2. THE AFFINITY LAWS

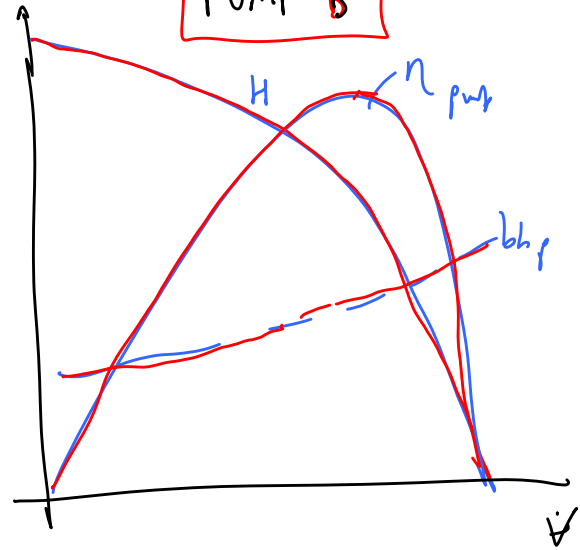
If 2 pumps are geometrically similar  $\hat{=}$  dynamically similar,  
then their pump performance curves fall on top of each other when plotted non dimensionally

e.g. Pump A  $\hat{=}$  Pump B  
 $\downarrow$   
 geometrically similar, but Pump B is bigger

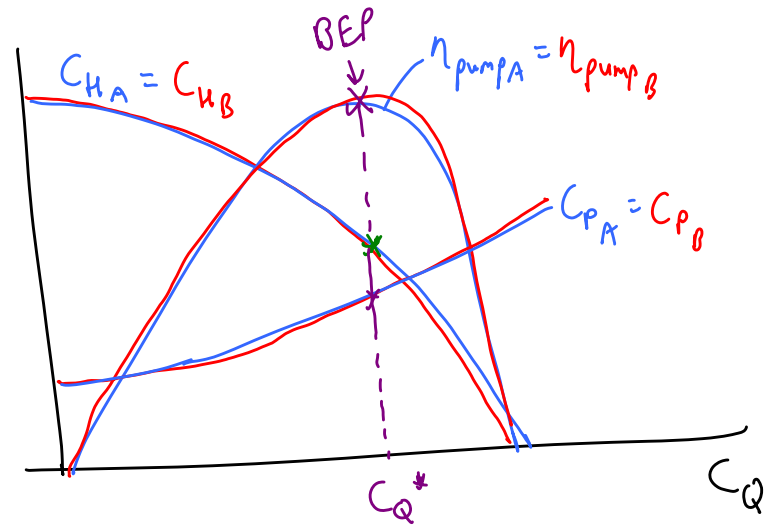
Pump A



Pump B



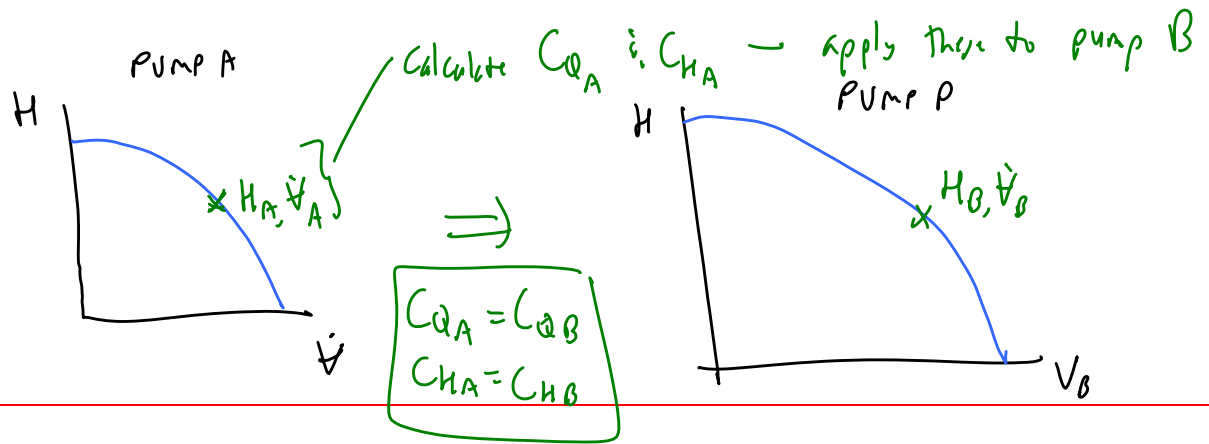
Plot both on same plot non dimensionally



★ ONE PLOT HOW FOR A WHOLE FAMILY OF GEOMETRICALLY SIMILAR PUMPS!

The Affinity Laws:

At some operating point for pump A  
 $(\dot{V}_A, H_A, \eta_A \dots)$



The two operating points for pump A & pump B are called

Homologous Points \*

i.e. if we set  $Q_A = Q_B$ , then  $C_{HA} = C_{HB}$ ,  $C_{PA} = C_{PB}$

$$C_{QA} = \frac{\dot{V}_A}{\omega_A D_A^3} = C_{QB} = \frac{\dot{V}_B}{\omega_B D_B^3} \Rightarrow \frac{\dot{V}_B}{\dot{V}_A} = \frac{\omega_B}{\omega_A} \left( \frac{D_B}{D_A} \right)^3$$

Do similarly for  $C_H$  &  $C_P$  :

THE AFFINITY LAWS:

\*

$$\frac{\dot{V}_B}{\dot{V}_A} = \left( \frac{\omega_B}{\omega_A} \right)^1 \left( \frac{D_B}{D_A} \right)^3$$

$$\frac{H_B}{H_A} = \left( \frac{\omega_B}{\omega_A} \right)^2 \left( \frac{D_B}{D_A} \right)^2$$

$$\frac{bhp_B}{bhp_A} = \left( \frac{\omega_B}{\omega_A} \right)^3 \left( \frac{D_B}{D_A} \right)^5 \frac{\rho_B}{\rho_A}$$

"Jingle" → "Very Hard Problems are as easy as 1, 2, 3!"

Volume flow rate (1)    
 Head (2)    
 Power (3)    
 exponent on  $\omega$  ratio

Holds for cases where all you change is the RPM ( $\omega$ )  
(For a given pump)



Similarly  $H_B = H_A \left( \frac{\dot{n}_B}{\dot{n}_A} \right)^2 \left( \frac{D_B}{D_A} \right)^2 = 3.193 \text{ m}$

$H_B = 3.12 \text{ m}$  (more than 2x as much)

(b) To do - estimate the % increase in required bhp

Soln  $\frac{bhp_B}{bhp_A} = \frac{\rho_B}{\rho_A} \left( \frac{\dot{n}_B}{\dot{n}_A} \right)^3 \left( \frac{D_B}{D_A} \right)^5 = 5.0739$

% increase =  $\frac{bhp_B - bhp_A}{bhp_A} \times 100\% = \left( \frac{bhp_B}{bhp_A} - 1 \right) \times 100\%$

% increase = 407%

TURBINES

- See pdf file on website

Turbine\_lecture.pdf