

**Today, we will:**

- Start Chapter 12 – Compressible Flow
- Discuss isentropic compressible flow, converging-diverging ducts

**X. INTRODUCTION TO COMPRESSIBLE FLOW (Chapter 12)**A. Introduction

- Everything so far has been incompressible ( $\rho \approx \text{constant}$ )
  - liquids
  - gases @ low Mach #'s
- Compressibility effects cause some new phenomena.

1. Definition & Reviewa. Mach #

$$Ma = \frac{V}{c}$$

★ most important parameter

If  $Ma \lesssim 0.3$  incompressible approx. is reasonable ( $\approx 5\%$  error)

In air @ room temp.  $c \approx 1100 \text{ ft/s} \approx 750 \frac{\text{mi}}{\text{hr}} \approx 335 \text{ m/s}$

@ 100 mph  $\rightarrow Ma \approx 0.133$

@ 600 mph  $\rightarrow Ma \approx 0.8$

Flow regimes: $Ma \lesssim 0.3$  incompressible $Ma = 1.0 \rightarrow$  sonic $0.3 \lesssim Ma < 1.0$  subsonic $Ma \gtrsim 3 \rightarrow$  hypersonic $Ma > 1.0$  supersonic $Ma$  near 1.0 transonic

b. Thermodynamic relationships:

Ideal gases

$$P = \rho R T$$

$$k = \frac{C_p}{C_v}$$

(Some books use  $\gamma$  instead of  $k$ )

$$R = C_p - C_v$$

$$R = \text{specific gas constant} = \frac{R_u}{M}$$

Use absolute temp!

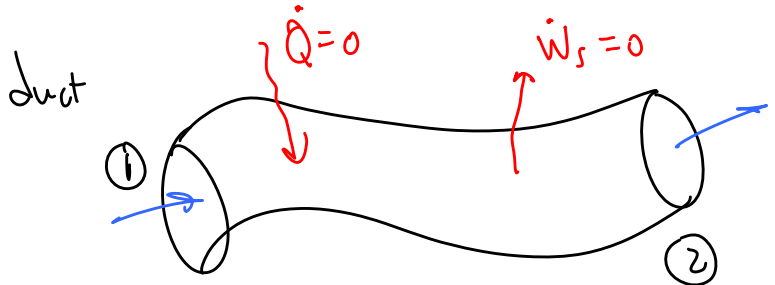
$$c = \sqrt{k R T}$$

For isentropic flow (neglect friction & other losses)

From ① to ②

$$\frac{P_2}{P_1} = \left(\frac{T_2}{T_1}\right)^{\frac{k}{k-1}} \quad \frac{\rho_2}{\rho_1} = \left(\frac{T_2}{T_1}\right)^{\frac{1}{k-1}}$$

Energy eq.



For isentropic, adiabatic, no work (neglecting gravity)

$$h_1 + \frac{1}{2} V_1^2 = h_2 + \frac{1}{2} V_2^2$$

$h_{o1}$  → Stagnation enthalpy       $h_{o2}$        $h_{o1} = h_{o2}$  ☆

• Stagnation temperature ☆

$T_o \equiv$  The temp. you get when you bring the flow to rest isentropically

Ideal gas →  $h = C_p T + \text{const} \rightarrow h_o = C_p T_o + \text{const}$

in a duct like this,  $T_o = \text{constant}$  ( $T_{o2} = T_{o1}$ )

energy eq.

$$h_o = h + \frac{1}{2} V^2 = \text{const}$$

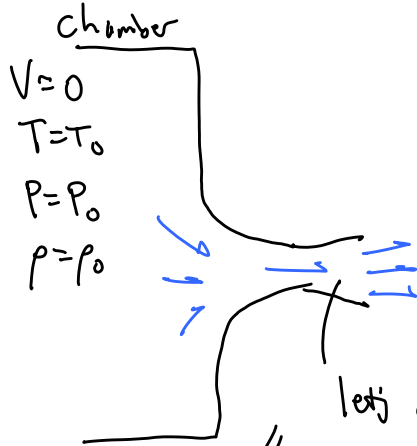
$$C_p T_o = C_p T + \frac{1}{2} V^2 = \text{const} \quad \therefore$$

$$\left[ C_p = \frac{kR}{k-1}, \quad c = \sqrt{kRT} \right]$$

$$\star \frac{T_o}{T} = 1 + \frac{k-1}{2} (Ma)^2 \quad (3)$$

## 2. 1-D Isentropic Adiabatic Flow in Ducts

a. Eqs.



$P_b =$  back pressure  
 (in the downstream volume)

See Table A-13

let's calculate  $T, P, \rho, Ma$ , etc. in the duct

ISENTROPIC RELATIONSHIPS

for ideal gas  
 (adiabatic)

$$\frac{T_0}{T} = 1 + \frac{k-1}{2} (Ma)^2$$

$$\frac{c_0}{c} = \left(\frac{T_0}{T}\right)^{\frac{1}{2}}$$

$$\frac{P_0}{P} = \left(\frac{T_0}{T}\right)^{\frac{k}{k-1}}$$

$$\frac{\rho_0}{\rho} = \left(\frac{T_0}{T}\right)^{\frac{1}{k-1}}$$

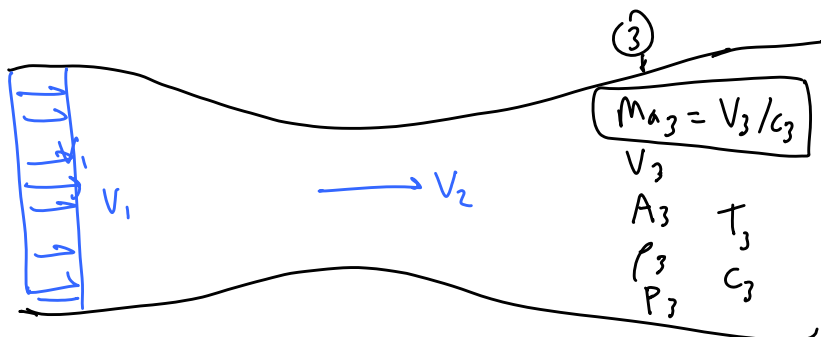
for a given  $Ma$ , we can calculate all these values

$k$   
 $[k=1.4 \text{ for air}]$

How do we calc.  $Ma$ ?

Cons. of mass

b. Isentropic duct flow with area changes



Approx:

- 1) 1-D (uniform)
- 2) steady
- 3) isentropic
- 4) adiabatic
- 5) ideal gas

Cons. of mass:

$$\dot{m} = \rho VA = \text{constant}$$

} algebra (see text)

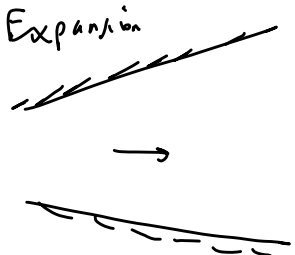
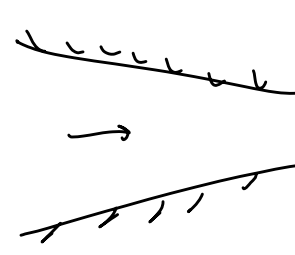
$$\star \frac{dV}{V} = \frac{1}{M_a^2 - 1} \frac{dA}{A} \quad (4)$$

• if  $M_a < 1$  (subsonic)  $M_a^2 - 1$  is negative  $\rightarrow \frac{dV}{V} \propto -\frac{dA}{A}$

as  $A \uparrow$  (diffuser),  $V \downarrow$  } same as  
 as  $A \downarrow$  (nozzle),  $V \uparrow$  } incomp flow

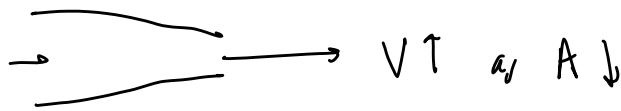
• if  $M_a > 1$  (supersonic)  $M_a^2 - 1$  is (+ve)  $\rightarrow \frac{dV}{V} \propto \frac{dA}{A}$

as  $A \uparrow$   $V \uparrow$  } opposite of  
 as  $A \downarrow$   $V \downarrow$  } our intuition

<u>COMPARISON</u>	<u>SUBSONIC</u>	<u>SUPERSONIC</u>
Expansion 	(diffuser) $A \uparrow$ $M_a \downarrow$ $V \downarrow$ $\rho \uparrow$ $P \uparrow$	(nozzle) $A \uparrow$ $M_a \uparrow$ $V \uparrow$ $\rho \downarrow$ $P \downarrow$
Contraction 	<u>SUBSONIC</u> $A \downarrow$ $M_a \uparrow$ $V \uparrow$ $\rho \downarrow$ $P \downarrow$ (nozzle)	<u>SUPERSONIC</u> $A \downarrow$ $M_a \downarrow$ $V \downarrow$ $\rho \uparrow$ $P \uparrow$ (diffuser)

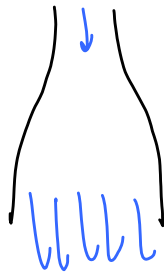
Nozzle:

Subsonic



Supersonic

rocket engine



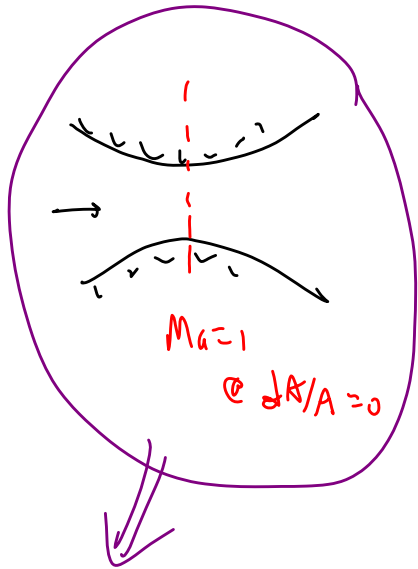
V ↑ as A ↑

What about when  $Ma = 1$ ? (Eq 4 has a zero in denom!)

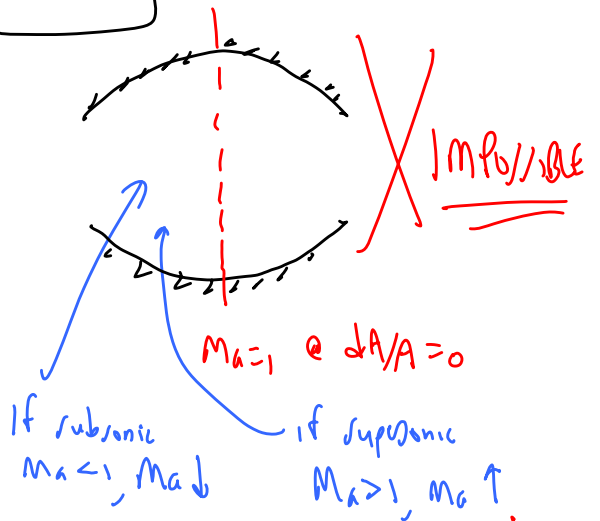
$$\text{Eq (4)} \rightarrow \frac{dA}{A} = \underbrace{(Ma^2 - 1)}_0 \frac{dV}{V} (= 0 \text{ when } Ma = 1)$$

$$\rightarrow \boxed{\frac{dA}{A} = 0} \text{ @ } Ma = 1 \star$$

i.e. either



or



For 1-D isentropic adiabatic duct flow, sonic conditions ( $Ma = 1$ ) can occur only at a throat (minimum area)  $\star$

See eqs in text

Sonic conditions (we  $\star$  for sonic)

$$\text{eg } \left[ \frac{P^*}{P_0} = 0.5283 \text{ for air} \right]$$

$$\frac{T^*}{T_0} = 0.8333$$