

**Today, we will:**

- Discuss applications of the Bernoulli equation
- Derive and discuss the linear momentum equation for a control volume (Chapter 6)
- Discuss the momentum flux correction factor,  $\beta$
- Discuss all the various forces acting on a control volume, and do some examples

**Recall, the beloved Bernoulli equation:**

$$\frac{P_1}{\rho g} + \frac{V_1^2}{2g} + z_1 = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + z_2 = \text{constant along a streamline}$$

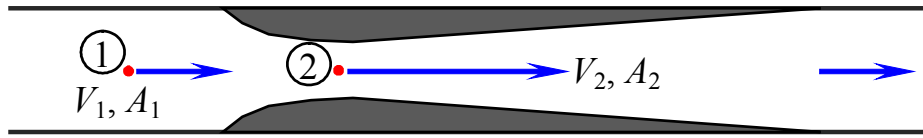
Note that the Bernoulli equation is valid *only* if *all* of the following limitations are met:

- no pumps or turbines
- steady
- incompressible
- negligible irreversible head losses (this is the limitation that usually restricts its use)

**2. Applications of the Bernoulli equation**

**Example: Pressure drop through a Venturi tube**

**Given:** Water flows horizontally in a round pipe with a converging-diverging section (a Venturi tube) as sketched. Cross-sectional area  $A_1$  is four times larger than cross-sectional area  $A_2$  (at the throat). Neglect any irreversible losses in the flow. The average speed at Section 1 is  $V_1 = 2.00$  m/s.



**To do:** If  $P_{1,\text{gage}} = 50,000$  Pa, estimate  $P_{2,\text{gage}}$  in units of Pa.

**Solution:**

## E. The Linear Momentum Equation for a Control Volume (Chapter 6)

### 1. Equations and Definitions

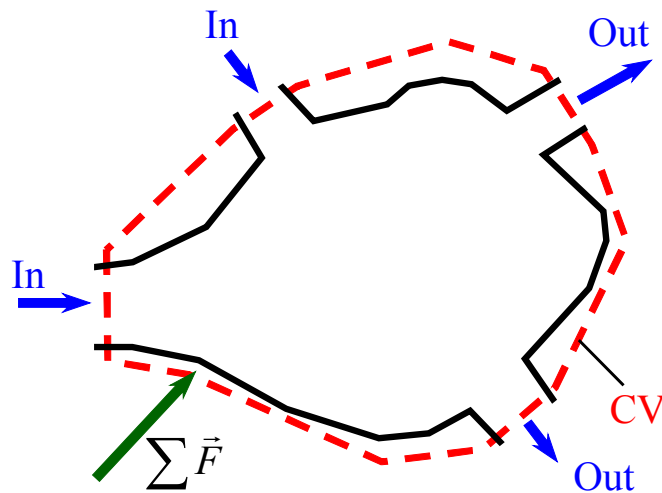
Recall the RTT at the end of Chapter 4, applied to linear momentum:

$$\sum \vec{F} = \frac{d}{dt} \int_{CV} \rho \vec{V} dV + \int_{CS} \rho \vec{V} (\vec{V} \cdot \vec{n}) dA$$

Diagram illustrating the components of the Linear Momentum Equation for a Control Volume (CV):

- Total force (*vector*) acting on the control volume** (points to  $\sum \vec{F}$ )
- Rate of change of linear momentum inside the control volume** (points to  $\frac{d}{dt} \int_{CV} \rho \vec{V} dV$ )
- Net rate of linear momentum flow out of the control volume** (points to  $\int_{CS} \rho \vec{V} (\vec{V} \cdot \vec{n}) dA$ )
- Use *relative velocity*  $\vec{V}_r$  here if we have a moving or deforming control volume** (points to  $\vec{V}$  in the integrand)

Simplification for well-defined inlets and outlets

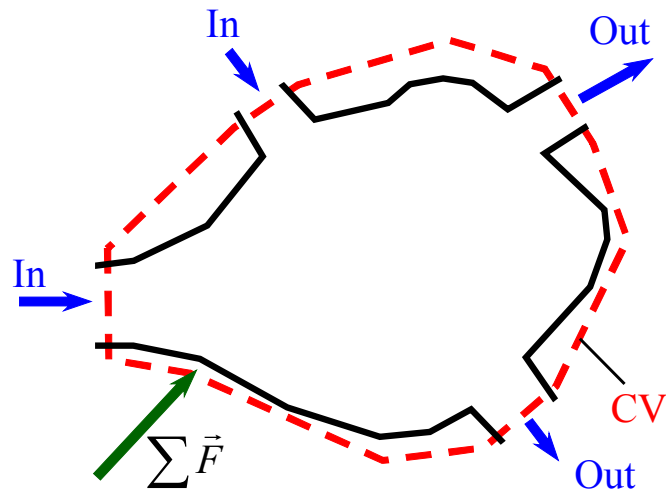


$$\sum \vec{F} = \frac{d}{dt} \int_{CV} \rho \vec{V} dV + \sum_{out} \dot{m} \vec{V} - \sum_{in} \dot{m} \vec{V}$$

## 2. The momentum flux correction factor

$$\sum \vec{F} = \frac{d}{dt} \int_{CV} \rho \vec{V} dV + \sum_{\text{out}} \beta \dot{m} \vec{V} - \sum_{\text{in}} \beta \dot{m} \vec{V}$$

### 3. Forces acting on a control volume



The approximate, most useful form of the linear momentum equation:

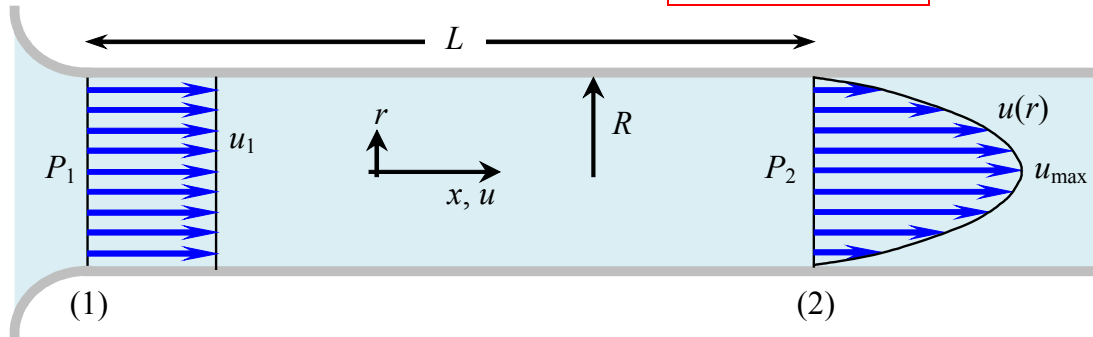
$$\sum \vec{F} = \sum \vec{F}_{\text{gravity}} + \sum \vec{F}_{\text{pressure}} + \sum \vec{F}_{\text{viscous}} + \sum \vec{F}_{\text{other}} = \frac{d}{dt} \int_{CV} \rho \vec{V} dV + \sum_{\text{out}} \beta \dot{m} \vec{V} - \sum_{\text{in}} \beta \dot{m} \vec{V}$$

### 4. Examples

### Example: Friction force in a pipe

**Given:** Consider steady, laminar, incompressible, axisymmetric flow of a liquid in a pipe as sketched. At the inlet (1) there is a nice bell mouth, and the velocity is nearly uniform (except for a very thin boundary layer, not shown).

- At (1),  $u = u_1 = \text{constant}$ ,  $v = 0$ , and  $w = 0$ .  $P_1$  is measured.
- At (2), the flow is fully developed and parabolic:  $u_2 = u_{\max} \left( 1 - \frac{r^2}{R^2} \right)$ .  $P_2$  is measured.



**To do:** Calculate the total friction force acting on the fluid by the pipe wall from 1 to 2.

**Solution:**

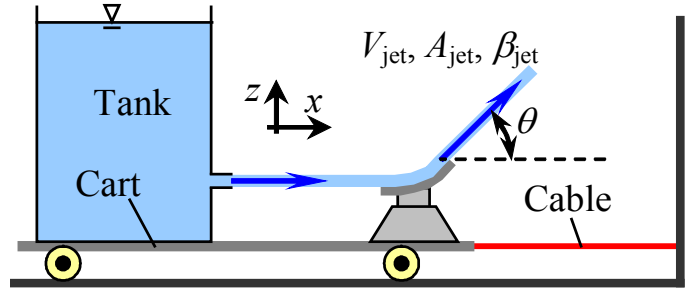
- First step:

- Now use the approximate, most useful form of the linear momentum equation,

$$\sum \vec{F} = \sum \vec{F}_{\text{gravity}} + \sum \vec{F}_{\text{pressure}} + \sum \vec{F}_{\text{viscous}} + \sum \vec{F}_{\text{other}} = \frac{d}{dt} \int_{CV} \rho \vec{V} dV + \sum_{\text{out}} \beta \dot{m} \vec{V} - \sum_{\text{in}} \beta \dot{m} \vec{V}$$

### Example: Tension in a cable

**Given:** A cart with frictionless wheels and a large tank shoots water at a deflector plate, turning it by angle  $\theta$  as sketched. The cart tries to move to the left, but a cable prevents it from doing so. At the exit of the deflector, the water jet area  $A_{\text{jet}}$ , its average velocity  $V_{\text{jet}}$ , and its momentum flux correction factor  $\beta_{\text{jet}}$  are known.



**To do:** Calculate the tension  $T$  in the cable.

**Solution:**

- First step:
- Second step: Use the approximate, most useful form of the linear momentum equation,

$$\sum \vec{F} = \sum \vec{F}_{\text{gravity}} + \sum \vec{F}_{\text{pressure}} + \sum \vec{F}_{\text{viscous}} + \sum \vec{F}_{\text{other}} = \frac{d}{dt} \int_{CV} \rho \vec{V} dV + \sum_{\text{out}} \beta \dot{m} \vec{V} - \sum_{\text{in}} \beta \dot{m} \vec{V}$$

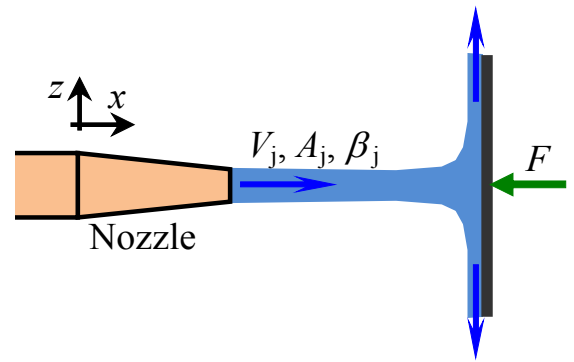
### Example: Force imparted by a water jet hitting a stationary plate

**Given:** A horizontal water jet of area  $A_j$ , average velocity  $V_j$ , and momentum flux correction factor  $\beta_j$  impinges normal to a stationary vertical flat plate.

**To do:** Calculate the horizontal force  $F$  required to keep the plate from moving.

**Solution:**

- First step:
- Second step: Use the approximate, most useful form of the linear momentum equation,



$$\sum \vec{F} = \sum \vec{F}_{\text{gravity}} + \sum \vec{F}_{\text{pressure}} + \sum \vec{F}_{\text{viscous}} + \sum \vec{F}_{\text{other}} = \frac{d}{dt} \int_{CV} \rho \vec{V} dV + \sum_{\text{out}} \beta \dot{m} \vec{V} - \sum_{\text{in}} \beta \dot{m} \vec{V}$$