

Today, we will:

- Begin Chapter 5 – Conservation of mass and energy for control volumes
- Do some example problems, conservation of mass
- If time, begin to discuss conservation of energy

III. Conservation Laws and the Control Volume (Integral) Technique (Chapter 5)

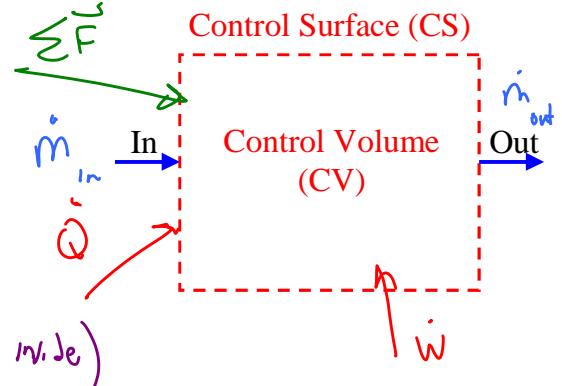
A. Introduction

1. Overview – Techniques for solving fluid flow problems

a. Control volume analysis (Ch. 5, 6, 8)



- We solve the integral (CV) equations
- We calculate gross (overall) properties only
- Treat CV as a "black box" (we care about the boundaries, not the details inside)

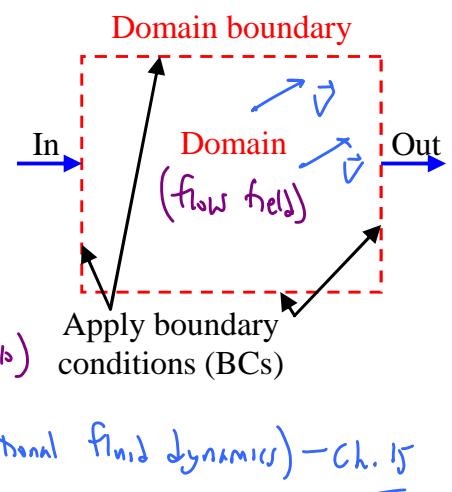


b. Dimensional analysis and experiment (Ch. 7)

- Don't solve any eq's
- Use Dimension to form nondimensional parameters – helping design experiments
- Use wind tunnel, etc. to measure the flow

c. Differential analysis (Ch. 9, 10, 15)

- Solve the differential eqs of motion
- Get details everywhere in the domain
- Can do analytically (simple problems) (Ch. 9; 10)
- ... Computationally CFD (Computational fluid dynamics) – Ch. 15



B. Conservation of Mass

1. Equations and definitions

From previous lecture... **the conservation of mass equation for a fixed control volume:**

RTE gives →

$$\frac{d}{dt} \int_{CV} \rho dV + \int_{CS} \rho (\vec{V} \cdot \vec{n}) dA = 0$$

Cons. of mass

(1)

$$\underbrace{\text{rate of change}}_{\text{of mass}} + \underbrace{\text{net rate of}}_{\text{mass flow}} = 0$$

Within the CV out of the CV through the CS

$$\text{if } \oplus + \ominus = 0$$

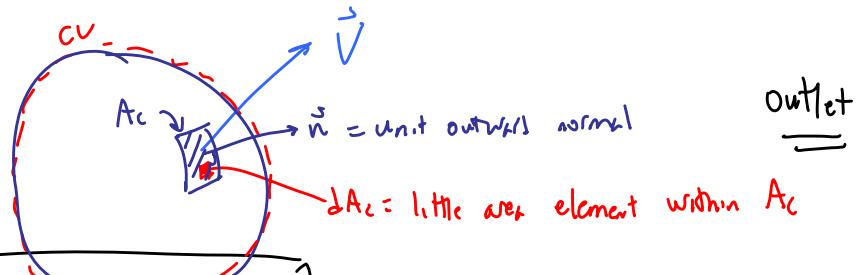
$$\text{if } \ominus + \oplus = 0$$

$$\text{if } 0 + 0 = 0$$

Steady

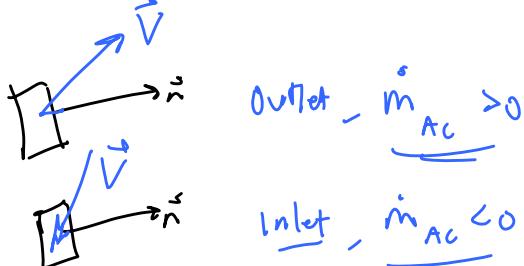
↓
no net mass flow out of CV

• Mass flow rate



$$\dot{m}_{Ac} = \int_{Ac} \rho (\vec{V} \cdot \vec{n}) \Delta A_c = \text{mass flow rate out of area } Ac$$

Signs take care of themselves



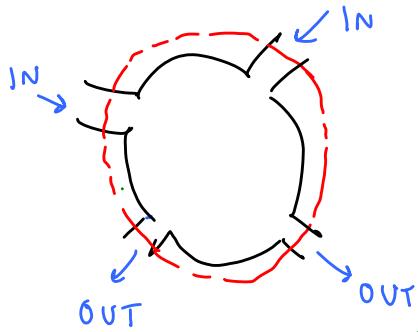
For the entire CS, we write

$$\dot{m}_{CS} = \int_{CS} \rho (\vec{V} \cdot \vec{n}) dA$$

= net mass flow rate out of the CV through the CS

It is easier if there are several separate inlet & outlet

Simplification



$$\dot{m}_{cv} = \sum_{in} \dot{m} - \sum_{out} \dot{m}$$

Then Eq (1) becomes

$$\frac{d}{dt} \int_{CV} \rho dV = \sum_{in} \dot{m} - \sum_{out} \dot{m}$$

or

$$\frac{d \dot{m}_{cv}}{dt} = \sum_{in} \dot{m} - \sum_{out} \dot{m}$$

⚡ Rate of change of mass within the CV = net rate of mass flow into the CV through inlet & outlets

If flow is steady, then $\frac{d \dot{m}_{cv}}{dt} = 0 \rightarrow \sum_{in} \dot{m} = \sum_{out} \dot{m}$ Steady CV
 "What goes in must go out"

• Volume flow rate (usually work with incompressible flow - const. density)

$$\dot{V}_{Ac} = \int_{A_c} (\vec{V} \cdot \vec{n}) dA_c$$

Same as \dot{m}_{Ac} but without the ρ

[We use \dot{V} for volume flow rate.

• Define Average Velocity through A_c

Some other textbooks use Q for \dot{V}

$$V_{avg, Ac} = \frac{1}{A_c} \int_{A_c} \vec{V} \cdot \vec{n} dA_c$$

$$V_{avg, Ac} = \frac{\dot{V}}{A_c}$$

- For a given inlet or outlet, A_c , we can make this approximation:

$$\dot{m}_{A_c} = \rho_{avg} V_{avg} A_c$$

- We usually drop the "avg" subscript (to be lazy)

$$\dot{m}_{A_c} = \rho V A_c$$

implies

$$V = V_{avg}$$

$$\rho = \rho_{avg}$$

or

$$\dot{m}_{A_c} = \rho \dot{V} A_c$$

Finally, if flow is also incompressible [$\rho \approx \text{const}$] and steady

$$\sum_{out} \dot{m} = \sum_{in} \dot{m}$$

$$\sum_{out} (\cancel{\rho} \cancel{\dot{V}}) = \sum_{in} (\cancel{\rho} \cancel{\dot{V}}) \quad (\rho \approx \text{const})$$

So,

$$\sum_{in} \dot{V} = \sum_{out} \dot{V}$$

cons. of volume flow rate

Volume flow rate in = volume flow rate out

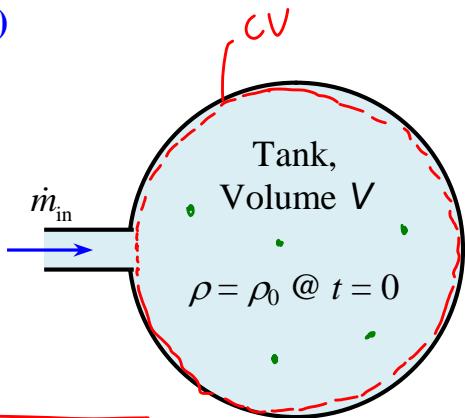
2. Examples

Example: Unsteady conservation of mass (flow into a tank)

Given: Air is pumped into a rigid tank of volume V . The mass flow rate of the air entering the tank is constant, \dot{m}_{in} . We assume that the process is slow enough that the air in the tank remains at the same temperature (isothermal conditions).

To do: Generate an equation for density ρ in the tank as a function of time.

Solution:



* First step in any CV analysis is to pick & draw a CV! (Approx that $\rho \approx$ constant inside the CV, but changes with time)

Use cons. of mass Fixed control volume, but compressible is unsteady

$$\frac{d}{dt} \int_{CV} \rho dV = \sum_{in} \dot{m} - \sum_{out} \dot{m}^o \quad (\text{no outflow})$$

$$\frac{d}{dt} \int_{CV} \rho dV = \dot{m}_{in} - 0$$

t of tank

$$\left[\rho = \rho(t) \right] \rightarrow \frac{d\rho}{dt} = \frac{\dot{m}_{in}}{V} = \text{a const.} \rightarrow \text{integrate: from } t=0 \text{ (}\rho=\rho_0\text{)} \text{ to } t$$

$$\rho = \frac{\dot{m}_{in}}{V} t + \text{const}$$

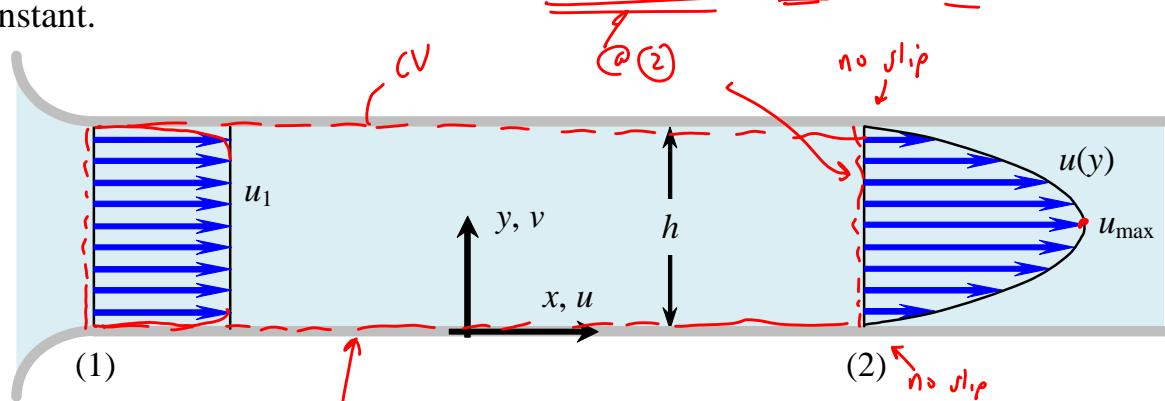
When $t=0, \rho=\rho_0$
 $\therefore \text{const} = \rho_0$

$$\boxed{\rho = \rho_0 + \frac{\dot{m}_{in}}{V} t}$$

Example: Velocity profiles in 2-D channel flow

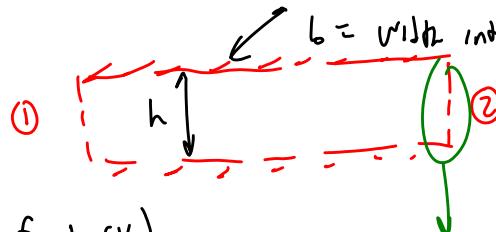
Given: Consider steady, incompressible, two-dimensional flow of a liquid between two very long parallel plates as sketched. At the inlet (1) there is a nice bell mouth, and the velocity is nearly uniform (except for a very thin boundary layer, not shown).

- At (1), $u = u_1 = \text{constant}$, $v = 0$, and $w = 0$.
- At (2), the flow is fully developed, and $u = ay(h - y)$, $v = 0$, and $w = 0$, where a is a constant.



To do: Generate expressions for constant a and speed u_{\max} in terms of the given variables.

Solution: For step: Draw a CV

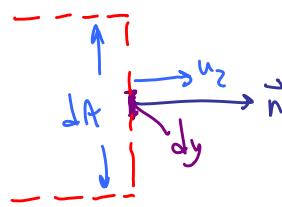


• Cons. of m6ll (steady, incomp, fixed CV)

$$\sum \dot{m} = \sum \dot{m}$$

$$u_1 h b = \int_A (\vec{V} \cdot \vec{n}) dA$$

$$A_2 \quad \vec{V} \cdot \vec{n} = u_2 \quad dA = b dy$$



$$u_1 h b = b \int_{y=0}^{y=h} u_2 dy$$

$$u_1 h b = b \int_{y=0}^{y=h} a y (h - y) dy$$

Integrate this (try it on your own for practice).

$$\text{Get } u_1 h = \frac{ah^3}{6}$$

$$a = \frac{6u_1}{h^2}$$

Answer for const. a