

**Today, we will:**

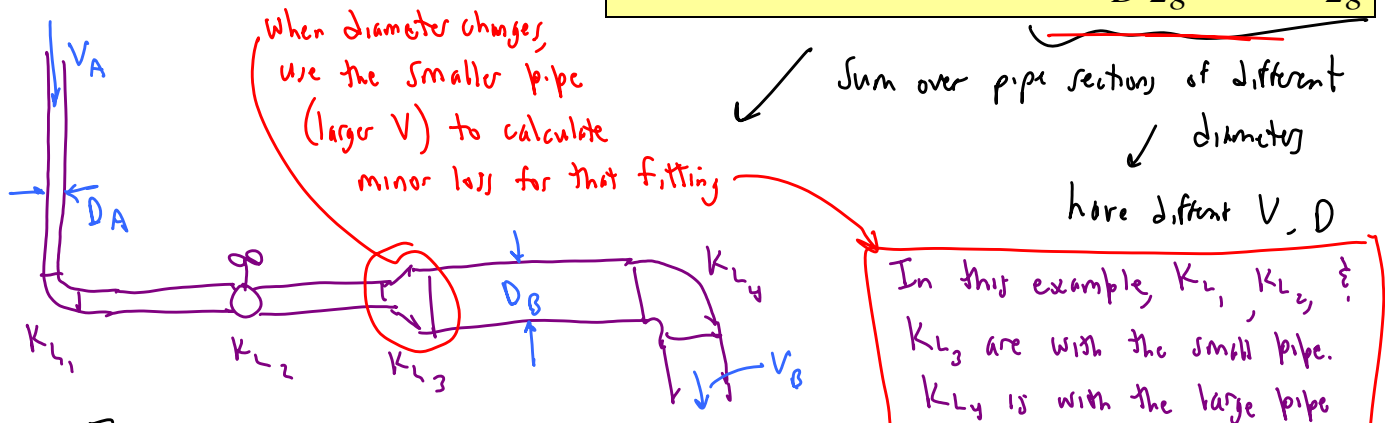
- Continue discussing minor losses in pipe flows, and do some example problems

Recall, major and minor head losses:

Major:  $h_{L,\text{major}} = f \frac{L V^2}{D 2g}$  where  $f = \text{fnc}\left(\text{Re}, \frac{\varepsilon}{D}\right)$  from Moody chart or Colebrook equation.

Minor:  $h_{L,\text{minor}} = K_L \frac{V^2}{2g}$  where  $K_L$  = minor loss coefficient, from tables and charts.

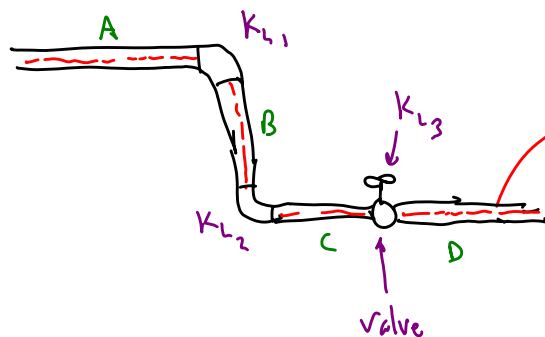
In the head form of the energy equation,  $h_L = \sum h_{L,\text{major}} + \sum h_{L,\text{minor}} = \sum f \frac{L V^2}{D 2g} + \sum K_L \frac{V^2}{2g}$ .



- In most problems,  $D = \text{constant everywhere}$ ,  $\therefore V$  is  $\text{const everywhere}$

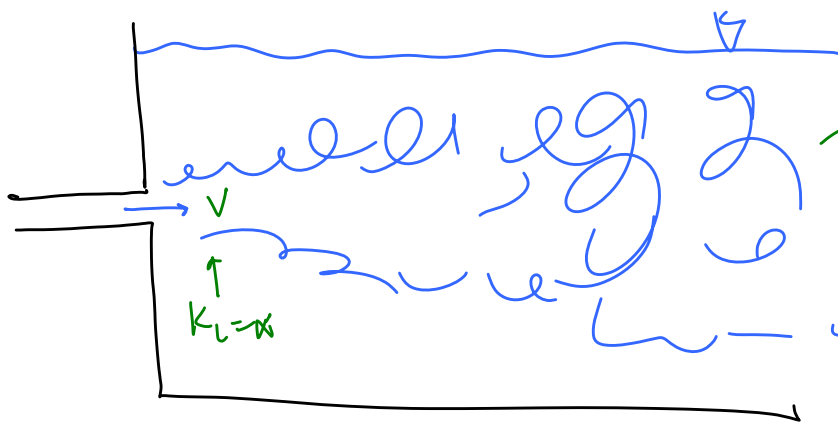
$$h_L = \frac{V^2}{2g} \left( f \frac{L}{D} + \sum K_L \right)$$

Total length of pipe, adding all sections



★ This is the most common form that we will use in this course

Head loss at outlets



turbulent eddies  
waste energy!  
eventually dissipate  
to heat energy

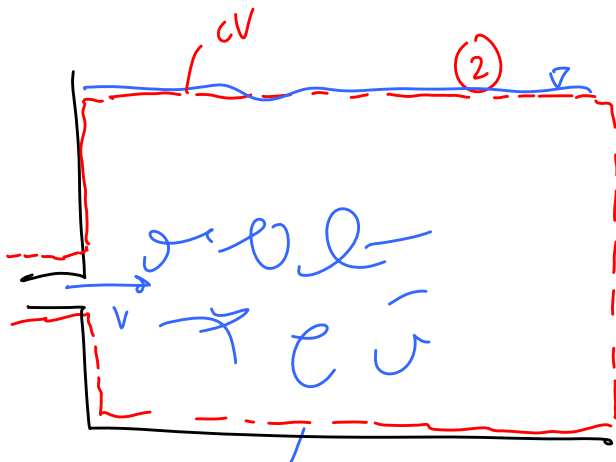
In energy eq.,

$$\sim + \alpha \frac{V^2}{2g}$$

all of this kinetic energy is wasted

$\therefore K_L$  @ an outlet is equal to  $\alpha$

Minor loss @ an outlet  $\therefore h_L = K_L \frac{V^2}{2g}$   $K_L = \alpha$

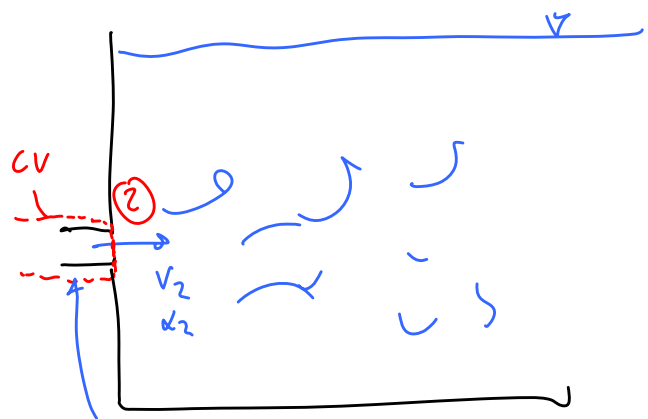


With this CV, include  $\alpha$   
as one of our  $K_L$ 's

Energy eq.  
 $+ \dots \alpha \frac{V^2}{2g} + \dots$  @ (2)

But,  $K_L = \alpha$  in tank, so get

$$\alpha \frac{V^2}{2g}$$



With this CV Do not include  
 $\alpha$  in the sum of  $K_L$ 's

However in energy eq.

$$+ \dots \alpha \frac{V^2}{2g} + \dots$$

include this term

b. Equivalent length — an alternative to using  $K_L$  for minor losses

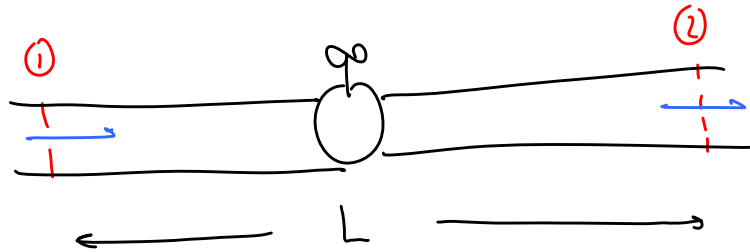
$$h_{L_{\text{minor}}} = f \frac{L_{\text{equiv}}}{D} \frac{V^2}{2g}$$

Equivalent dia

→ Treat the minor loss as if it were a longer pipe

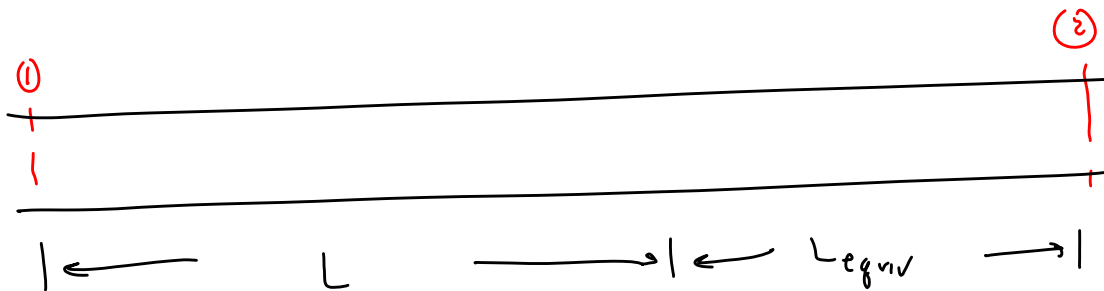
eg. Valve

Real case



Imaginary replacement case

[Pretend the pipe is longer by  $L_{\text{equiv}}$ ]



In energy eq., we

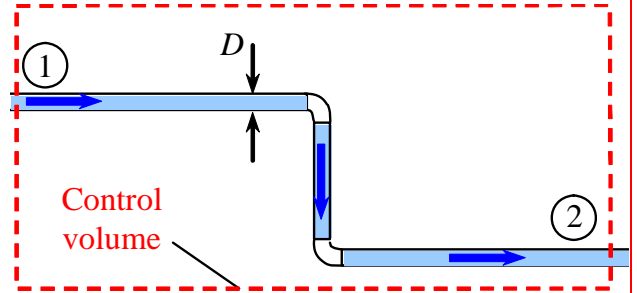
$$\underline{L_{\text{total}} = L + L_{\text{equiv}}}$$

$$h_L = f \frac{L_{\text{total}}}{D} \frac{V^2}{2g}$$

2. Example

### Example: Major and minor losses

**Given:** Water ( $\rho = 998 \text{ kg/m}^3$ ,  $\mu = 1.00 \times 10^{-3} \text{ kg/m}\cdot\text{s}$ ) flows at a steady average velocity of  $6.45 \text{ m/s}$  through a smooth pipe of diameter  $2.54 \text{ cm}$ . The flow is fully developed through the entire section of pipe. The total pipe length is  $10.56 \text{ m}$ , and there are two elbows, each with  $K_L = 0.90$ .



**To do:**

(a) Calculate the total <sup>irreversible</sup> head loss in meters through this section of piping due to both major and minor losses.

**Solution:**

• Draw a CV — see diagram

$$Re = \frac{\rho V D}{\mu} = \frac{(998 \text{ kg/m}^3)(6.45 \text{ m/s})(0.0254 \text{ m})}{1.00 \times 10^{-3} \text{ kg/m}\cdot\text{s}} = 163,502 \quad \text{TURBULENT} \quad (\epsilon/D = 0)$$

• Moody chart or Colebrook eq.  $\rightarrow f = 0.0163$

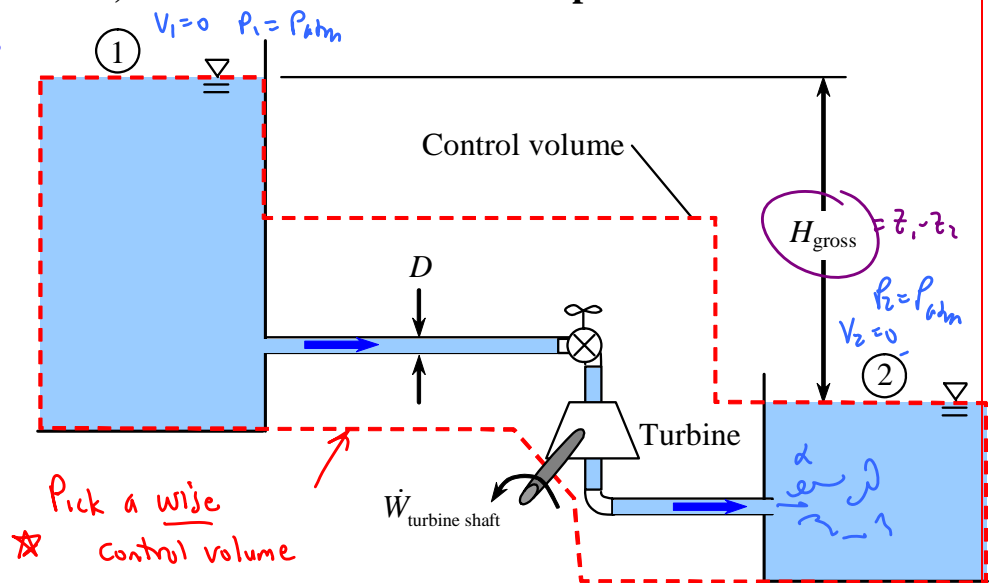
• Minor losses too.

$$h_L = \frac{V^2}{2g} \left( f \frac{L}{D} + \sum K_L \right)$$
$$= \frac{(6.45 \text{ m/s})^2}{2(9.807 \text{ m/s}^2)} \left( 0.0163 \frac{10.56 \text{ m}}{0.0254 \text{ m}} + 2(0.9) \right) = 18.2 \text{ m}$$

Comment: This is just the irreversible head loss. The flow from ① to ② also includes an elevation or potential energy head loss  $\rightarrow$  need to use the head form of the energy equation to deal with that

### Example: Major and minor losses, calculation of turbine shaft power

**Given:** Water ( $\rho = 998 \text{ kg/m}^3$ ,  $\mu = 1.00 \times 10^{-3} \text{ kg/m}\cdot\text{s}$ ) flows from one large reservoir to another, and through a turbine as sketched. The elevation difference between the two reservoir surfaces is  $H_{\text{gross}} = 120.0 \text{ m}$ . The pipe is  $5.0 \text{ cm}$  I.D. cast iron pipe. The total pipe length is  $30.8 \text{ m}$ . The entrance is slightly rounded; the exit is sharp. There is one regular flanged 90-degree elbow, and one fully open flanged angle valve. The turbine is 81% efficient. The volume flow rate through the turbine is  $0.0045 \text{ m}^3/\text{s}$ .



**To do:** Calculate the shaft power produced by the turbine in units of kilowatts.

#### Solution:

- First we draw a control volume, as shown by the dashed line. We cut through the surface of both reservoirs (inlet 1 and outlet 2), where we know that the velocity is nearly zero and the pressure is atmospheric. We also slice through the turbine shaft. The rest of the control volume simply surrounds the piping system.
- We apply the head form of the energy equation from the inlet (1) to the outlet (2):

$$\frac{P_1}{\rho g} + \alpha_1 \frac{V_1^2}{2g} + z_1 + h_{\text{pump,u}} = \frac{P_2}{\rho g} + \alpha_2 \frac{V_2^2}{2g} + z_2 + h_{\text{turbine,e}} + h_L \rightarrow h_{\text{turbine,e}} = (z_1 - z_2) - h_L$$

Handwritten notes:  $P_1 = P_2 = P_{\text{atm}}$  (in a yellow box),  $V_1 = V_2 \approx 0$  (in a yellow box), and  $H_{\text{gross}}$  above the head difference.

- But by definition of turbine efficiency,  $h_{\text{turbine,e}} = \frac{\dot{W}_{\text{turbine shaft}}}{\eta_{\text{turbine}} \dot{m} g}$  where  $\dot{m} = \rho \dot{V}$ . Also, since the reference velocity is the same for all the major and minor losses (the pipe diameter is constant throughout), we may use the simplified version of the equation for  $h_L$ , i.e., Eq. 8-59:

$$h_L = \frac{V^2}{2g} \left( f \frac{L}{D} + \sum K_L \right). \text{ Therefore, we solve the energy equation for the desired unknown,}$$

namely, turbine shaft power,  $\dot{W}_{\text{turbine shaft}} = \eta_{\text{turbine}} \rho \dot{V} g \left[ H_{\text{gross}} - \frac{V^2}{2g} \left( f \frac{L}{D} + \sum K_L \right) \right]$ . This is our answer in variable form, but we still need to calculate the values of some of the variables.

The rest of this problem will be solved in class.

$$V = \frac{\dot{V}}{A} = \frac{4\dot{V}}{\pi D^2} = \frac{4(0.0045 \text{ m}^3/\text{s})}{\pi (0.050 \text{ m})^2} = 2.29183 \text{ m/s} = V$$

$$\cdot Re = \frac{\rho V D}{\mu} = \frac{(998 \text{ kg/m}^3)(2.29183 \text{ m/s})(0.050 \text{ m})}{0.001 \text{ kg/m.s}} = \frac{1.144 \times 10^5}{1} = Re$$

(turbulent)

$$\cdot \epsilon = \rightarrow \text{look up Table 8-2} \rightarrow \epsilon = 0.26 \text{ mm} \rightarrow \frac{\epsilon}{D} = \frac{0.26 \text{ mm}}{50 \text{ mm}} = \underline{\underline{0.0052}}$$

$$\cdot \text{At this } Re \text{ \& } \epsilon/D \rightarrow \text{Moody chart} \rightarrow \underline{\underline{f = 0.03154}}$$

$$\cdot \sum K_L = 0.12 + 5 + 0.3 + \alpha = 6.47$$

↑  
slightly rounded inlet
↑  
angle valve
↑  
flanged elbow
↑  
outlet into a tank

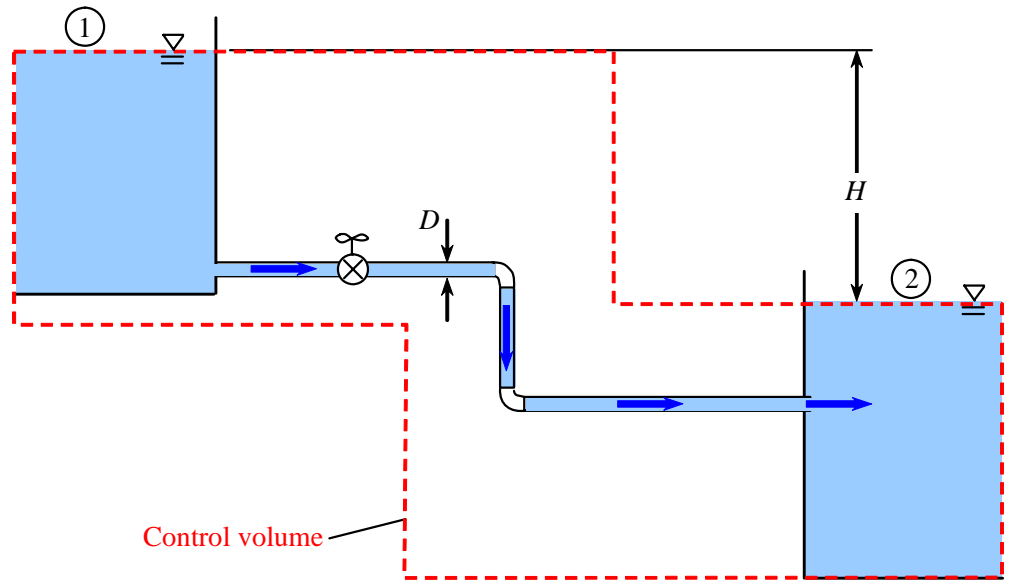
From Table

$$\dot{W}_{\text{turbine shaft}} = \eta_{\text{turbine}} \rho V g \left[ H_{\text{gross}} - \frac{V^2}{2g} \left( f \frac{L}{D} + \sum K_L \right) \right]$$

$$\dot{W}_{\text{turbine shaft}} = 4.03 \text{ kW}$$

## Example: Major and minor losses, iterating to calculate the flow rate

**Given:** Water ( $\rho = 998$  kg/m<sup>3</sup>,  $\mu = 1.00 \times 10^{-3}$  kg/m·s) flows *by gravity alone* from one large tank to another, as sketched. The elevation difference between the two surfaces is  $H = 35.0$  m. The pipe is 2.5 cm I.D. with an average roughness of 0.010 cm. The total pipe length is 20.0 m. The entrance and exit are sharp. There are two regular threaded 90-degree elbows, and one fully open threaded globe valve.



**To do:** Calculate the volume flow rate through this piping system.

### Solution:

- First we draw a control volume, as shown by the dashed line. We cut through the surface of both reservoirs (inlet 1 and outlet 2), where we know that the velocity is nearly zero and the pressure is atmospheric. The rest of the control volume simply surrounds the piping system.
- We apply the head form of the energy equation from the inlet (1) to the outlet (2):

$$\frac{P_1}{\rho g} + \alpha_1 \frac{V_1^2}{2g} + z_1 + \cancel{h_{\text{pump,u}}} = \frac{P_2}{\rho g} + \alpha_2 \frac{V_2^2}{2g} + z_2 + \cancel{h_{\text{turbine,e}}} + h_L$$

$P_1 = P_2 = P_{\text{atm}}$   
 $V_1 = V_2 \approx 0$

Therefore, the energy equation reduces to  $h_L = z_1 - z_2 = H$

- Next, we add up all the irreversible head losses, both major and minor. Since the reference velocity is the same for all the major and minor losses (the pipe diameter is constant throughout), we may use the simplified version of the equation for  $h_L$ ,

$$(2) \rightarrow h_L = \left( f \frac{L}{D} + \sum K_L \right) \frac{V^2}{2g}, \quad \& \quad \text{Re} = \frac{\rho D V}{\mu} \quad \dot{V} = V \frac{\pi D^2}{4} \quad \frac{\varepsilon}{D} = \frac{0.010 \text{ cm}}{2.5 \text{ cm}} = 0.004$$

- We also need either the Moody chart or one of the empirical equations that can be used in place of the chart (e.g., the Colebrook equation).

The rest of this problem will be solved in class.

$$\sum K_L = \underset{\substack{\uparrow \\ \text{inlet}}}{0.50} + \underset{\substack{\uparrow \\ 2 \text{ elbows}}}{2(0.9)} + \underset{\substack{\uparrow \\ \text{globe valve}}}{10} + \underset{\substack{\uparrow \\ \text{outlet}}}{1.05} = \underline{\underline{13.35}}$$

Iteration:

Solve (2) for  $V \rightarrow$

$$V = \sqrt{\frac{2gH}{f \frac{L}{D} + \sum K_L}} \quad (2)$$

Procedure:

<u>Guess <math>f</math></u>	<u>Calc. <math>V</math> using (2) (m/s)</u>	<u>Calc <math>Re</math></u>	<u>Look up <math>f</math>, Moody chart</u>
Initial guess $\downarrow$ 0.03	4.287	$1.076 \times 10^5$	0.029
0.029	4.334	$1.081 \times 10^5$	0.0294
0.0294	4.315	$1.077 \times 10^5$	0.02943
0.02943	4.314	$1.076 \times 10^5$	0.02943
Converged!			
Final value $\rightarrow V = 4.314 \text{ m/s}$			

$$\dot{V} = V \frac{\pi D^2}{4} = 2.12 \times 10^{-3} \text{ m}^3/\text{s}$$

See also the solution using FES



See next pages



## EES Solution for Example Problem – Major and Minor Losses in a Piping System

Here is exactly what I typed into the main “Equations Window” of EES:

"EES Solution for the class example problem - major and minor losses in a piping system  
J. M. Cimbala, February 2005"

"Constants:"

h\_L = 35 [m]  
rho = 998 [kg/m^3]  
mu = 1.00e-3 [kg/(m\*s)]  
D = 0.025 [m]  
L = 20.0 [m]  
SigmaK = 13.35

Note: We could have used the EES function  
“MoodyChart” instead of the Colebrook  
equation; i.e.,  
 $f = \text{MoodyChart}(\text{Re}, \text{eps\_by\_D})$   
which gives slightly different answers.

"Equations:"

$h_L = (f \cdot L / D + \text{SigmaK}) \cdot (V^2) / (2 \cdot g\#)$  "Note that g# is the gravitational constant, pre-defined by EES"  
Re = rho \* D \* V / mu  
eps\_by\_D = 0.004  
 $V_{\text{dot}} = V \cdot \text{PI} \cdot (D^2) / 4$

"Colebrook equation:"  $1/\text{sqrt}(f) = -2.0 \cdot \log_{10}(\text{eps\_by\_D} / 3.7 + 2.51 / (\text{Re} \cdot \text{sqrt}(f)))$


"To solve, click on Calculate and then Solve. Note that it does not converge unless you change the limits and guesses in Options-Variable Info"

Here is what the “Options-Variable Info” chart looks like:

Variable	Guess	Lower	Upper	Display	Units	Key	Comment
D	1	-infinity	infinity	A 3 N	m		
eps_by_D	1	-infinity	infinity	A 3 N			
f	0.02	1.0000E-03	1.0000E-01	A 3 N			
h_L	1	-infinity	infinity	A 3 N	m		
L	1	-infinity	infinity	A 3 N	m		
mu	1	-infinity	infinity	A 3 N	kg/(m*s)		
Re	10000	4.0000E+03	infinity	A 3 N			
rho	1	0.0000E+00	infinity	A 3 N	kg/m^3		
SigmaK	1	0.0000E+00	infinity	A 3 N			
V	1	0.0000E+00	infinity	A 3 N	m/s		
V_dot	1	0.0000E+00	infinity	A 3 N	m^3/s		

Note: I had to change some of the initial guesses and some of the lower and upper limits in order for EES to converge on a solution. This takes some trial and error.

The Formatted Equations window looks like this (the equations appear in much more readable format):

 **Formatted Equations**

EES Solution for the class example problem - major and minor losses in a piping system  
 J. M. Cimbala, February 2005

Constants:

$h_L = 35 \text{ [m]}$   
 $\rho = 998 \text{ [kg/m}^3\text{]}$   
 $\mu = 0.001 \text{ [kg/(m*s)]}$   
 $D = 0.025 \text{ [m]}$   
 $L = 20 \text{ [m]}$   
 $\text{SigmaK} = 13.35$

Equations:

$$h_L = \left[ f \cdot \frac{L}{D} + \text{SigmaK} \right] \cdot \frac{V^2}{2 \cdot 9.807 \text{ [m/s}^2\text{]}}$$

Note that g# is the gravitational constant, pre-defined by EES

$$\text{Re} = \rho \cdot D \cdot \frac{V}{\mu}$$

$$\text{eps}_{\text{by,D}} = 0.004$$

$$\dot{V} = V \cdot \pi \cdot \frac{D^2}{4}$$

Colebrook equation:  $\frac{1}{\sqrt{f}} = -2 \cdot \log \left[ \frac{\text{eps}_{\text{by,D}}}{3.7} + \frac{2.51}{\text{Re} \cdot \sqrt{f}} \right]$

To solve, click on Calculate and then Solve. Note that it does not converge unless you change the limits and guesses in Options-Variable Info

Finally, Calculate and Solve yields the solution:

D=0.025 [m]  
 eps\_by\_D=0.004  
 f=0.02943  
 h\_L=35 [m]  
 L=20 [m]  
 mu=0.001 [kg/(m\*s)]  
 Re=107627  
 rho=998 [kg/m^3]  
 SigmaK=13.35  
 V=4.314 [m/s]  
**V\_dot=0.002117 [m^3/s]**

This is our final result, i.e., the volume flow rate through the pipe. We can verify that all the variables are correct, and are the same as those calculated by “hand”, i.e.,

$$\dot{V} = 2.12 \times 10^{-3} \text{ m}^3/\text{s}$$