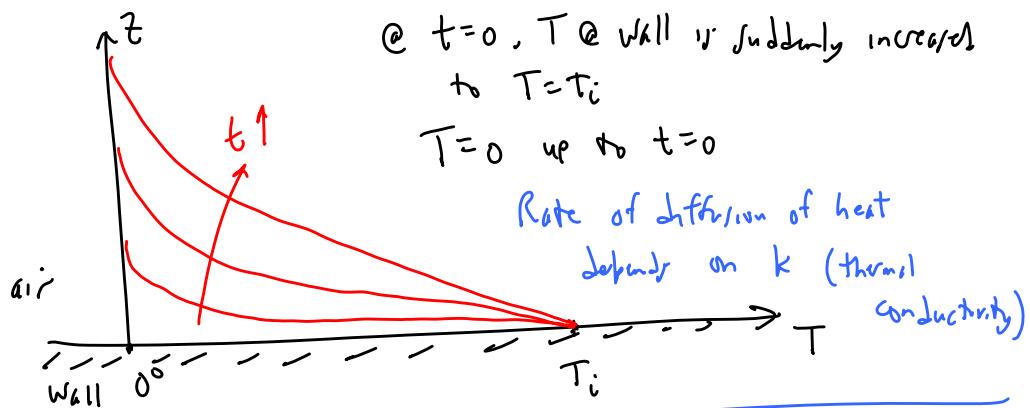


Today, we will:

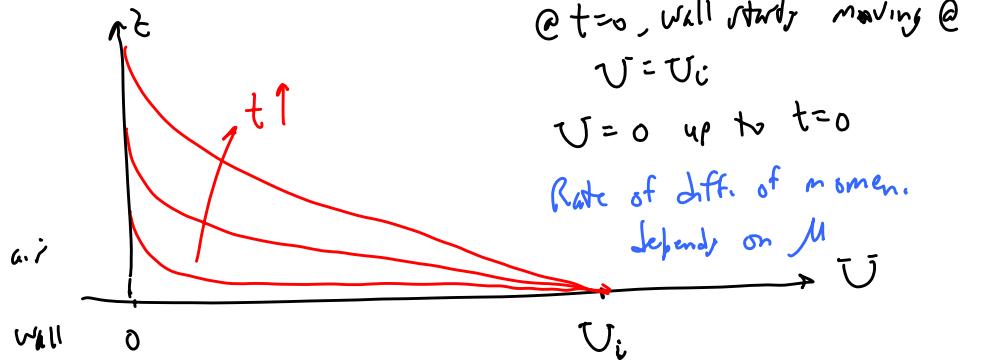
- Continue our discussion of gradient diffusion
- Discuss the **Reynolds analogy**
- Discuss **evaporation of a pure liquid in stagnant air – Section 4.5**
- Do some example problems

Example: m_{ij}/ρ_j - momentum - energy analogy for a step change

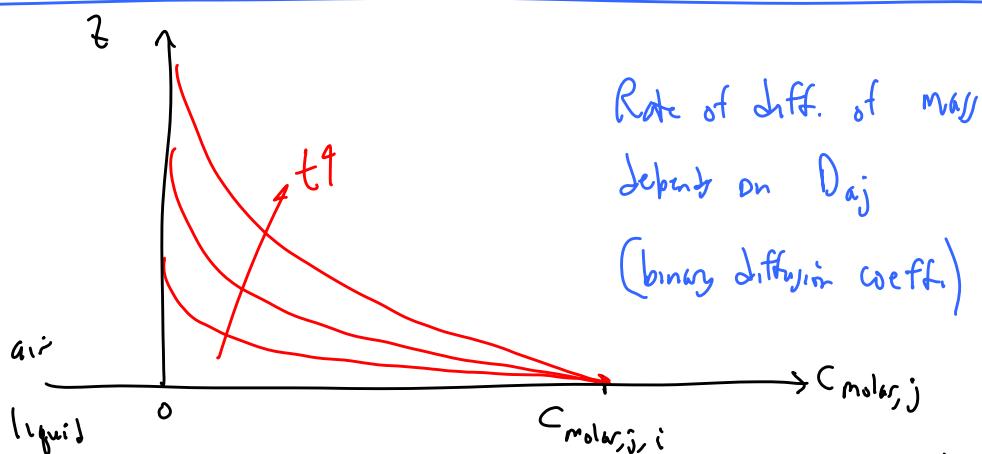
Energy:



Momentum



m_{ij}/ρ_j



Imagine a thin membrane at the interface that is suddenly removed @ $t=0$

The behavior of m_{ij}/ρ_j , momen., & energy diffusion is very similar, but with different rates, because of different diffusion coefficients.

Introduce some nondimensional ratios of these diffusion coefficients

- Momen. i. mass ($\nu \nmid D_{\text{aj}}$)

D_{aj} has unit of m^2/s

ν has unit of $\text{kg}/\text{m}\cdot\text{s}$ → introduce $\nu = \text{kinematic viscosity}$

$$\nu \sim \dots \text{ m}^2/\text{s}$$

$$\nu \equiv \frac{\mu}{\rho}$$

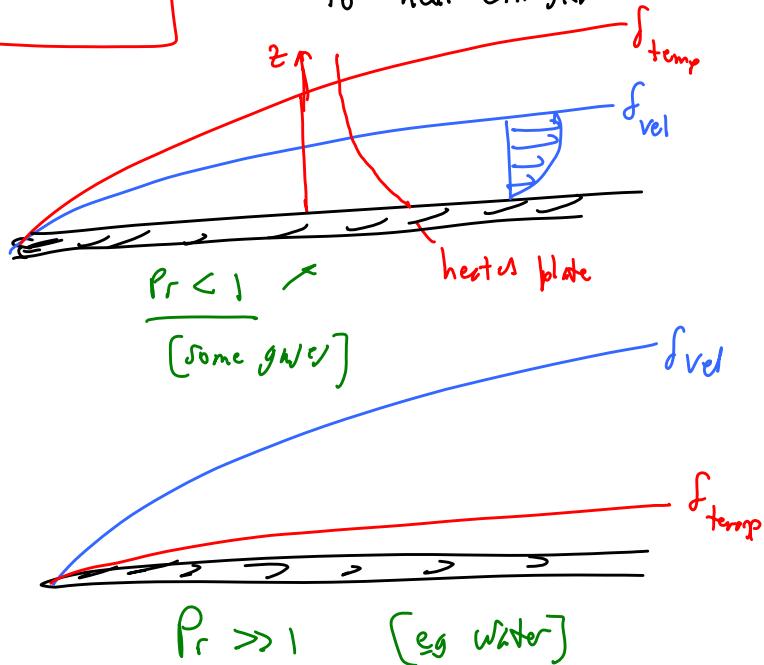
$$S_c = \text{Schmidt \#} \equiv \frac{\nu}{D_{\text{aj}}} = \text{ratio of momen. diffusim } \nmid \text{ to mass diffusion}$$

- Momen. i. energy ($\nu \nmid k$) — again we ν

define $K \equiv \frac{k}{\rho C_p}$ = thermal diffusivity units of m^2/s
 (kappa)

$$Pr = \text{Prandtl \#} \equiv \frac{\nu}{K} = \text{ratio of mom. diff. to heat diffusion}$$

e.g. Boundary layer
 (Laminar flow) →



In air, $\nu \nmid K$ are close to each other → ∴ $Pr \approx 1$

$$(Pr \approx 0.7)$$

Energy & mass

$$Le = \text{Lewis \#} = \frac{K}{D_{aj}}$$

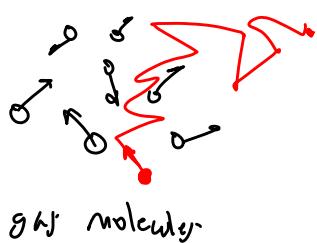
* = ratio of energy diffusion to mass (or species) diffusion

$$Le = \frac{Sc}{Pr}$$

REYNOLDS ANALOGY

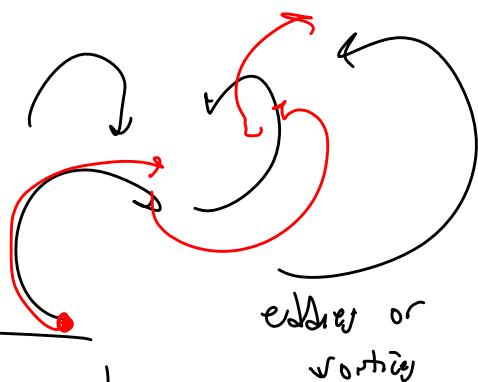
for turbulent flow, heat, mass, & momentum diffusion are still related, but diffusion is a macroscopic rather than microscopic phenomenon

Laminar diffusion



gas molecule

Turbulent Diffusion



eddy or vortex

Diffusion coefficient for turbulent flow \gg
.. laminar ..

* Reynolds
Analogy

Usefulness

- Can easily measure heat transfer characteristics (lots of data)
We have correlations (Nusselt # vs Reynolds #, etc.)
- We can apply these heat xfer correlations to species transfer, which are harder experiments to conduct

[This is what we do in Chap. 4]

~~★ EXAM 1 MATERIAL ENDS HERE~~

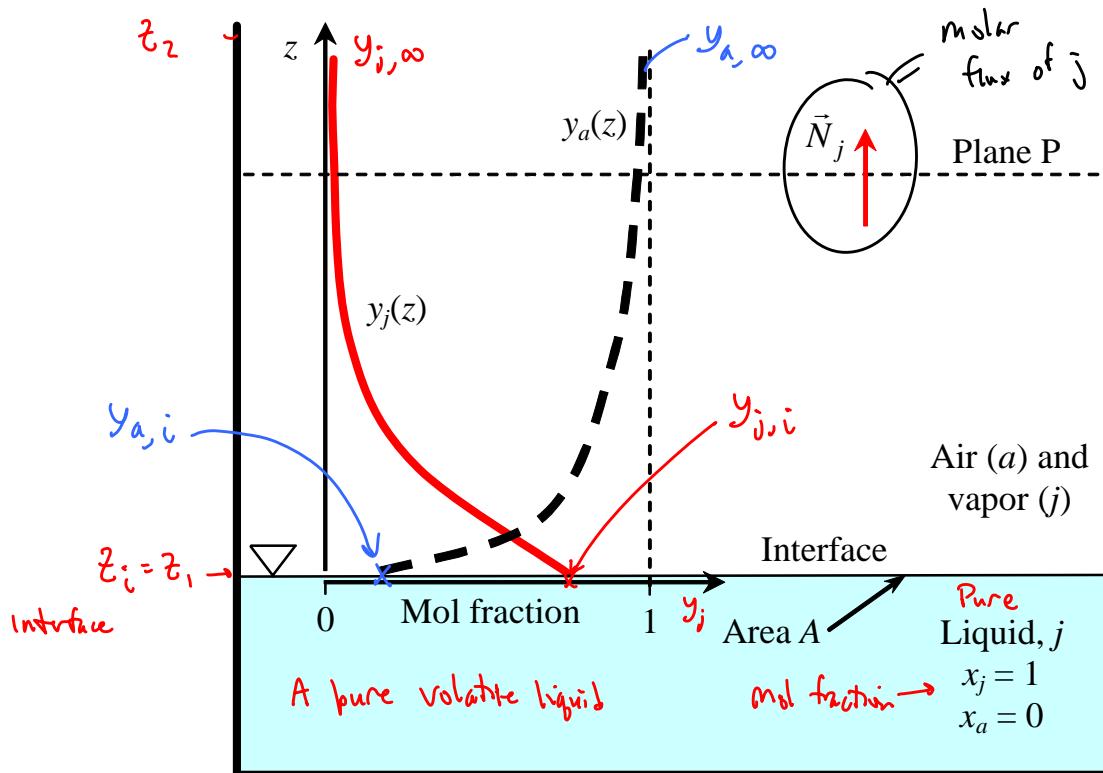
[Up to Sec. 4.5]

↑ Exam 1

↓ Exam 2

Sec. 4.5 Evaporation of a liquid from a container;

Section 4.5.3 – Evaporation of a liquid from a container, open to nearly stagnant air on top:



$$\sum y_j = 1 \rightarrow \therefore \boxed{y_a + y_j = 1}$$

For a pure liquid (species j), $\underline{\underline{P_{j,i}}} = \underline{\underline{P_{v,j}}}$ at the interface

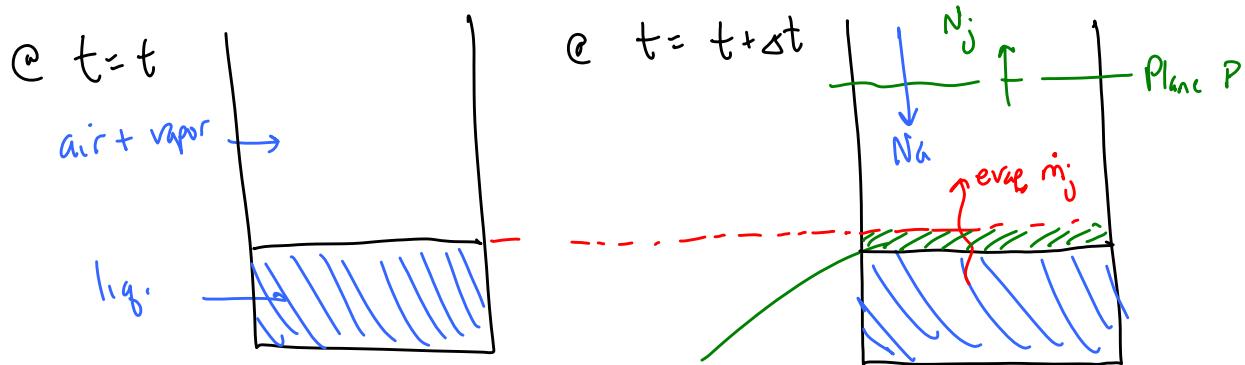
$$\text{Recall, } y_j = \frac{P_j}{P_{\text{atm}}} \rightarrow \therefore \boxed{y_{j,i} = \frac{P_{v,j}}{P_{\text{atm}}}}$$

$N_j = \underline{\text{molar flux}} = \# \text{ mol/s of species } j \text{ crossing a } \underline{\underline{\text{fixed plane}}} \text{ parallel to the interface per unit area per unit time}$

Units of N_j are $\frac{\text{kmol}}{\text{m}^2 \cdot \text{s}}$

N_j is similar to J_j except J_j is a relative molar flux

N_j is an absolute molar flux [fixed plane]



All of this liquid has evaporated

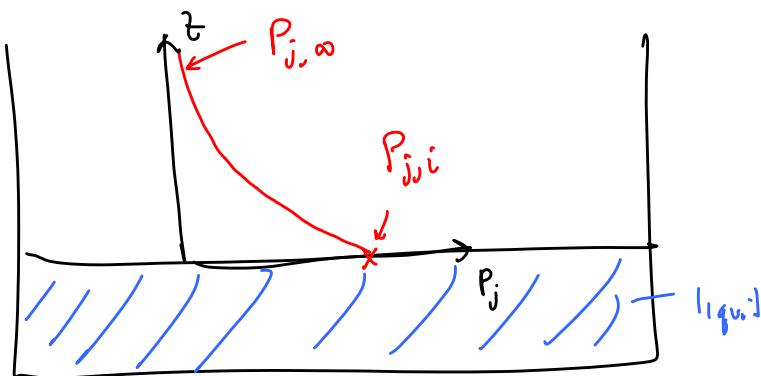
from the air's point of view,

Air must move down to replace the displaced liquid

$\therefore N_a = \text{molar flux of air } i. w \text{ in opposite direction of } N_j$

We can also plot in terms of P_j instead of y_j

$$y_j = \frac{P_j}{P} \text{ or } \frac{P_j}{P_{\text{atm}}}$$



The larger D_{aj}
the faster the
evaporation takes
place

[See App A-9 for]
 $\rightarrow D_{aj}$
(Also, some empirical eqs)
for D_{aj} in Ch.4

Equation for $m_{\text{evap}, j}$

• See book for empirical eqs for N_j

also for coefficients, sometimes using heat transfer data.

→ Bottom line:

eqs for $\underline{\underline{m_{j,\text{evap}}}}$