

Lapple Cyclones **A PRACTICAL APPLICATION OF INERTIAL SEPARATION !**

Today, we will:

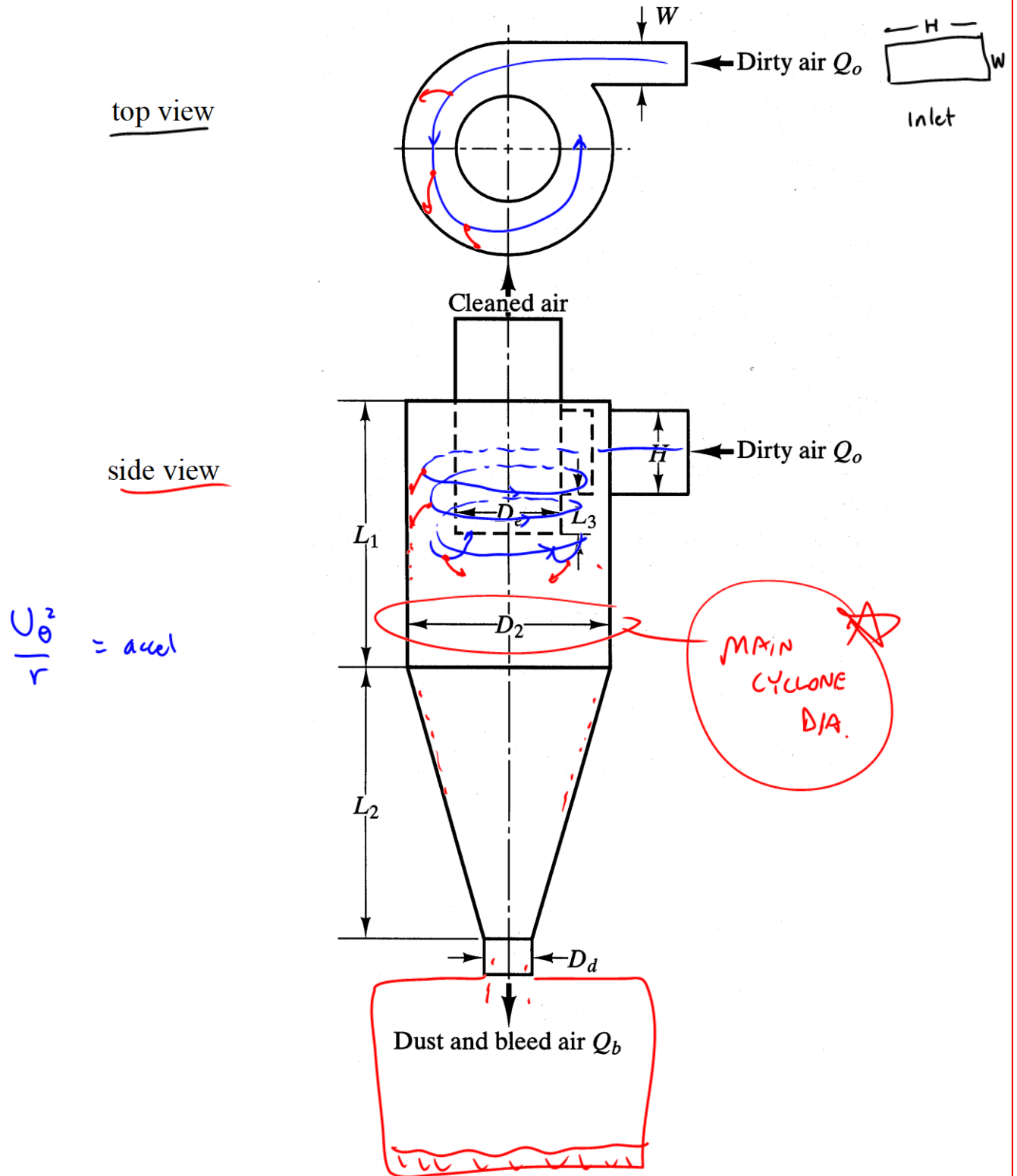
- Introduce **Cyclones**, discuss how they work, and provide equations
- Discuss **Lapple Cyclone Performance** when parameters are varied
- Do an example problem



**Introduction to Cyclones/Principle of operation:** Make the dusty air flow around in circles so that **particles are flung towards the outside of the unit** (inertial separation), and then the particles fall to the bottom of the unit by gravity. They come in all sizes.



Typical **vertical reverse-flow cyclone** geometry and dimensions, rectangular inlet



**Figure 9.2** Lapple standard reverse-flow cyclone collector with tangential entry, and with characteristic dimensions given by Eqs. (9-5) and (9-6). From H&C textbook.

Equations for a general *Lapple* reverse-flow cyclone of any dimensions:

$$\eta(D_p) = \frac{1}{1 + \left(\frac{D_{p,\text{cut}}}{D_p}\right)^2}$$

$$D_{p,\text{cut}} = \sqrt{\frac{9\mu HW^2}{2\pi N_e Q (\rho_p - \rho)}}$$

$$\Delta P = 40.96\rho \left(\frac{Q}{WH}\right)^2$$

$$\dot{W}_{\text{blower}} = \frac{Q\Delta P}{\eta_{\text{blower}}}$$

*Grain eff*      *η = 50%*      "minor loss"      *power*

Dimensions for the *standard* Lapple reverse-flow cyclone:

$$L_1 = L_2 = 2D_2 \quad W = D_d = D_2/4 \quad H = D_e = D_2/2 \quad L_3 = D_2/8 \quad N_e \approx 6 \quad \underline{\underline{=6}}$$

*# of swirls*

Plug these into the above general equations to get everything in terms of main cyclone diameter  $D_2$ :

e.g.  $D_{p,\text{cut}}$

$$D_{p,\text{cut}} = \sqrt{\frac{9\mu \frac{D_2}{2} \left(\frac{D_2}{4}\right)^2}{2\pi (6) Q (\rho_p - \rho)}}$$

$$D_{p,\text{cut}} = \sqrt{\frac{9\mu D_2^3}{2\pi (6)(2)(16) Q (\rho_p - \rho)}}$$

$$D_{p,\text{cut}} = \sqrt{\frac{3\mu D_2^3}{128\pi Q (\rho_p - \rho)}}$$

*We assume spherical particles*

Final equations for a *standard* reverse flow Lapple cyclone of *any* size in terms of  $D_2$ :

$$D_{p,\text{cut}} = \sqrt{\frac{3\mu D_2^3}{128\pi Q (\rho_p - \rho)}}$$

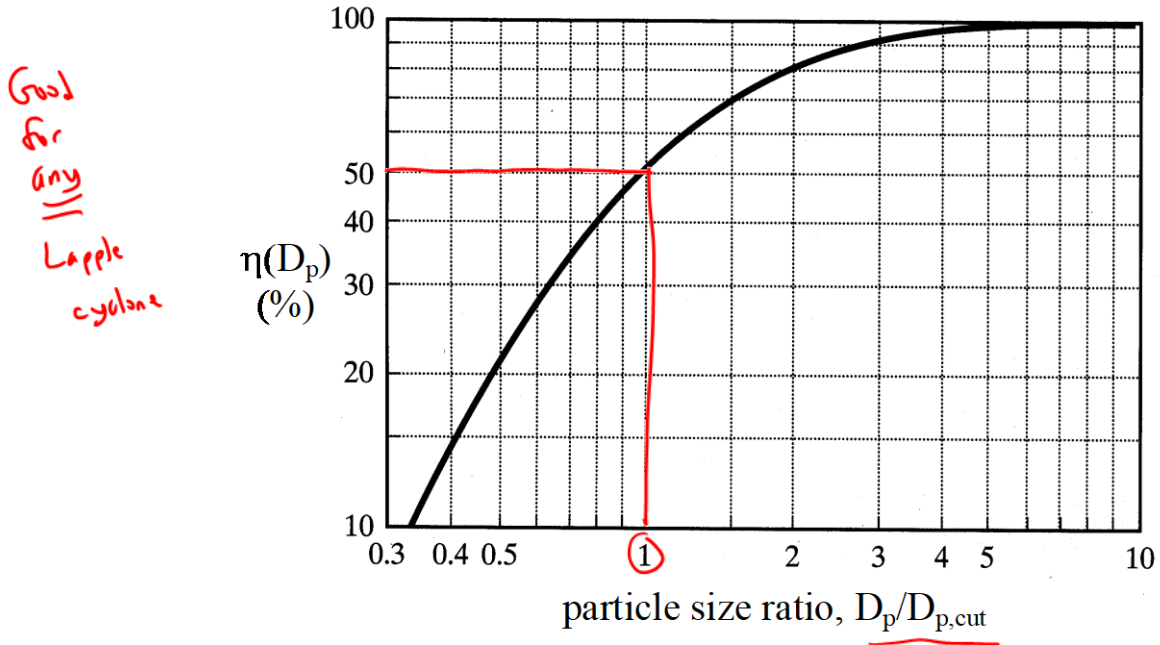
$$\eta(D_p) = \frac{1}{1 + \left(\frac{D_{p,\text{cut}}}{D_p}\right)^2}$$

$$\Delta P = 2621.44\rho \frac{Q^2}{D_2^4}$$

$$\dot{W}_{\text{blower}} = \frac{Q\Delta P}{\eta_{\text{blower}}}$$

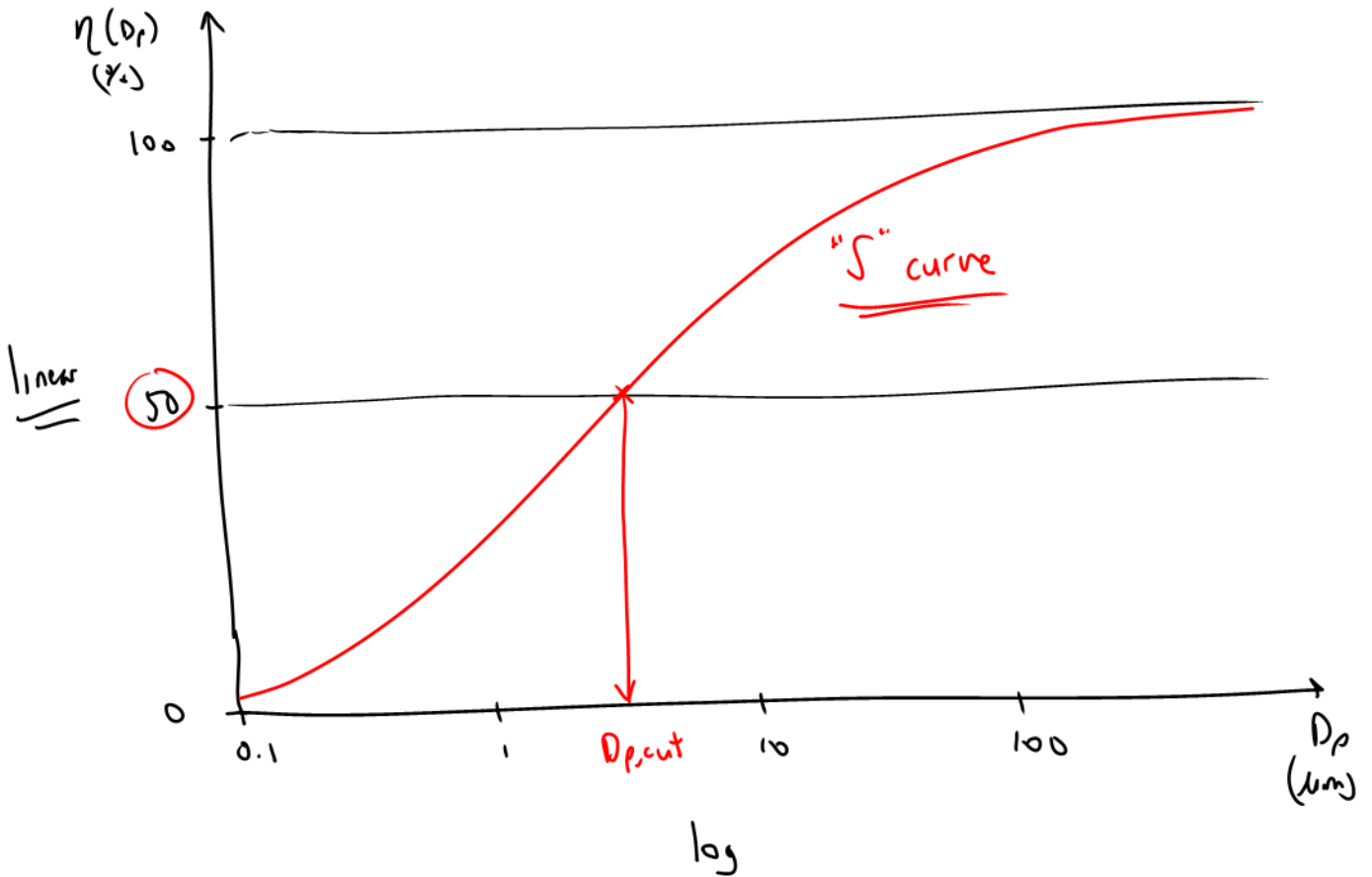
*any Q, ρ, ρ<sub>p</sub>, μ*      *blower/motor*

**Grade efficiency for a Lapple standard reverse-flow cyclone:**



**Figure 9.3** Normalized grade efficiency of a Lapple standard reverse-flow cyclone.

log-linear plot:



### Example: Lapple Cyclone

**Given:** A standard reverse flow Lapple cyclone is used to clean up a dusty air flow exhausted by a sanding machine in a wood shop. The main body diameter of the cyclone is  $D_2 = 45.0 \text{ cm}$  (0.450 m).

- Particle density  $\rho_p = 730 \text{ kg/m}^3$
- Bulk volume flow rate of air  $Q = 0.550 \text{ m}^3/\text{s}$
- Air is at SATP:  $\rho = 1.184 \text{ kg/m}^3$ ,  $\mu = 1.849 \times 10^{-5} \text{ kg/(m s)}$
- Blower efficiency (blower/motor combination) = 87.5%

**To do:** Calculate

- The cut diameter of this cyclone in units of microns
- The percent grade efficiency  $\eta(D_p)$  for 10- $\mu\text{m}$  particles
- The electrical power required to run this cyclone in units of kW

**Solution:** Some equations:

$$D_{p,\text{cut}} = \sqrt{\frac{3\mu D_2^3}{128\pi Q(\rho_p - \rho)}}$$

$$\eta(D_p) = \frac{1}{1 + \left(\frac{D_{p,\text{cut}}}{D_p}\right)^2}$$

$$\Delta P = 2621.44 \rho \frac{Q^2}{D_2^4}$$

$$\dot{W}_{\text{blower}} = \frac{Q \Delta P}{\eta_{\text{blower}}}$$

(a)  $D_{p,\text{cut}} = \sqrt{\frac{3(1.849 \times 10^{-5} \frac{\text{kg}}{\text{m}\cdot\text{s}})(0.450 \text{ m})^3}{128 \pi (0.550 \frac{\text{m}^3}{\text{s}})(730 - 1.184) \frac{\text{kg}}{\text{m}^3}}} = 5.59987 \times 10^{-6} \text{ m} = 5.59987 \mu\text{m}$

*We this sub. eqs*

$$D_{p,\text{cut}} = 5.60 \mu\text{m}$$

(b) @  $D_p = 10 \mu\text{m}$ ,

$$\eta(D_p) = \frac{1}{1 + \left(\frac{5.59987 \mu\text{m}}{10 \mu\text{m}}\right)^2} = 0.7613$$

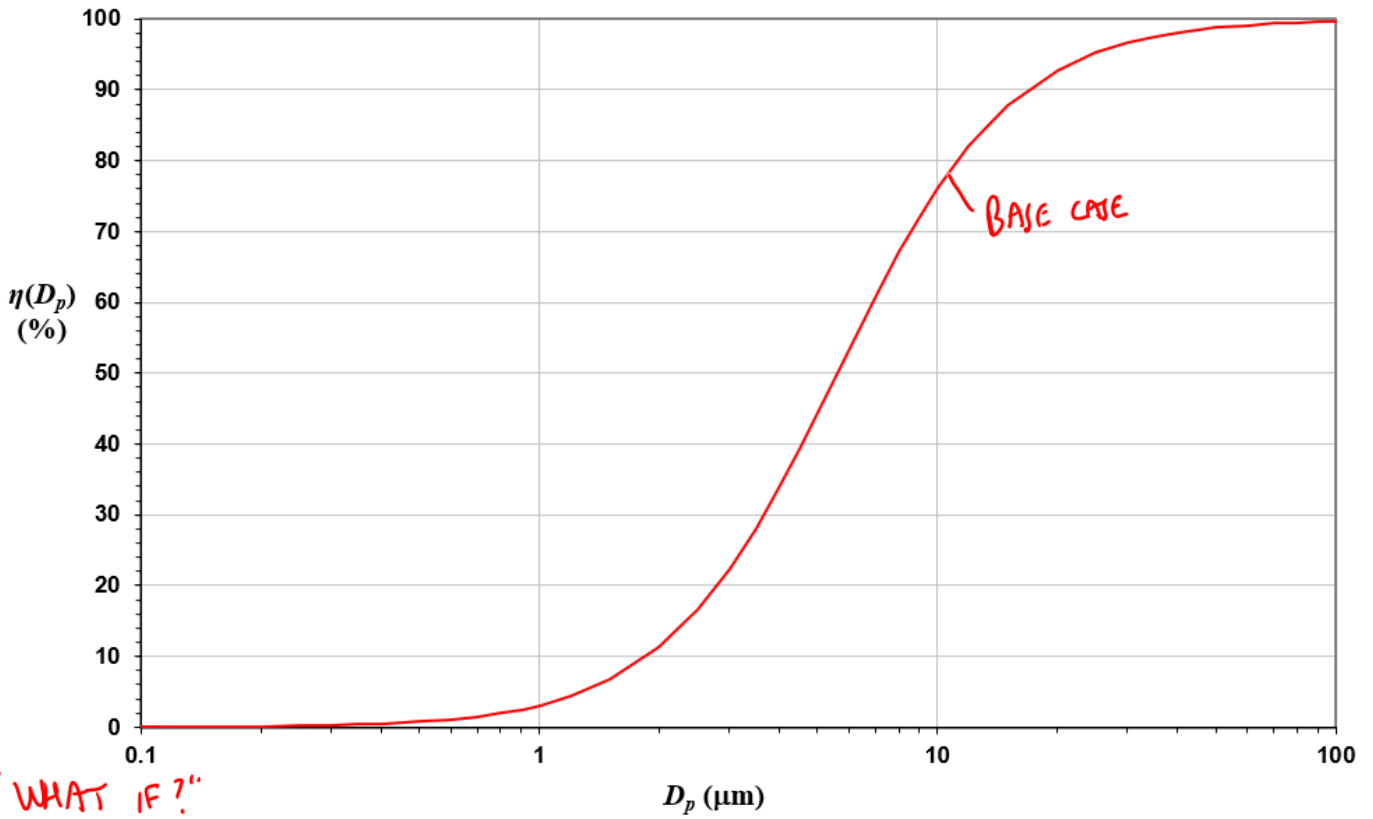
$$\eta(10\text{-}\mu\text{m}) = 76.1\%$$

(c)  $\Delta P = (2621.44)(1.184 \frac{\text{kg}}{\text{m}^3}) \frac{(0.550 \frac{\text{m}^3}{\text{s}})^2}{(0.450 \text{ m})^4} \left(\frac{\text{N}\cdot\text{s}^2}{\text{kg}\cdot\text{m}}\right) = 22896 \frac{\text{N}}{\text{m}^2}$

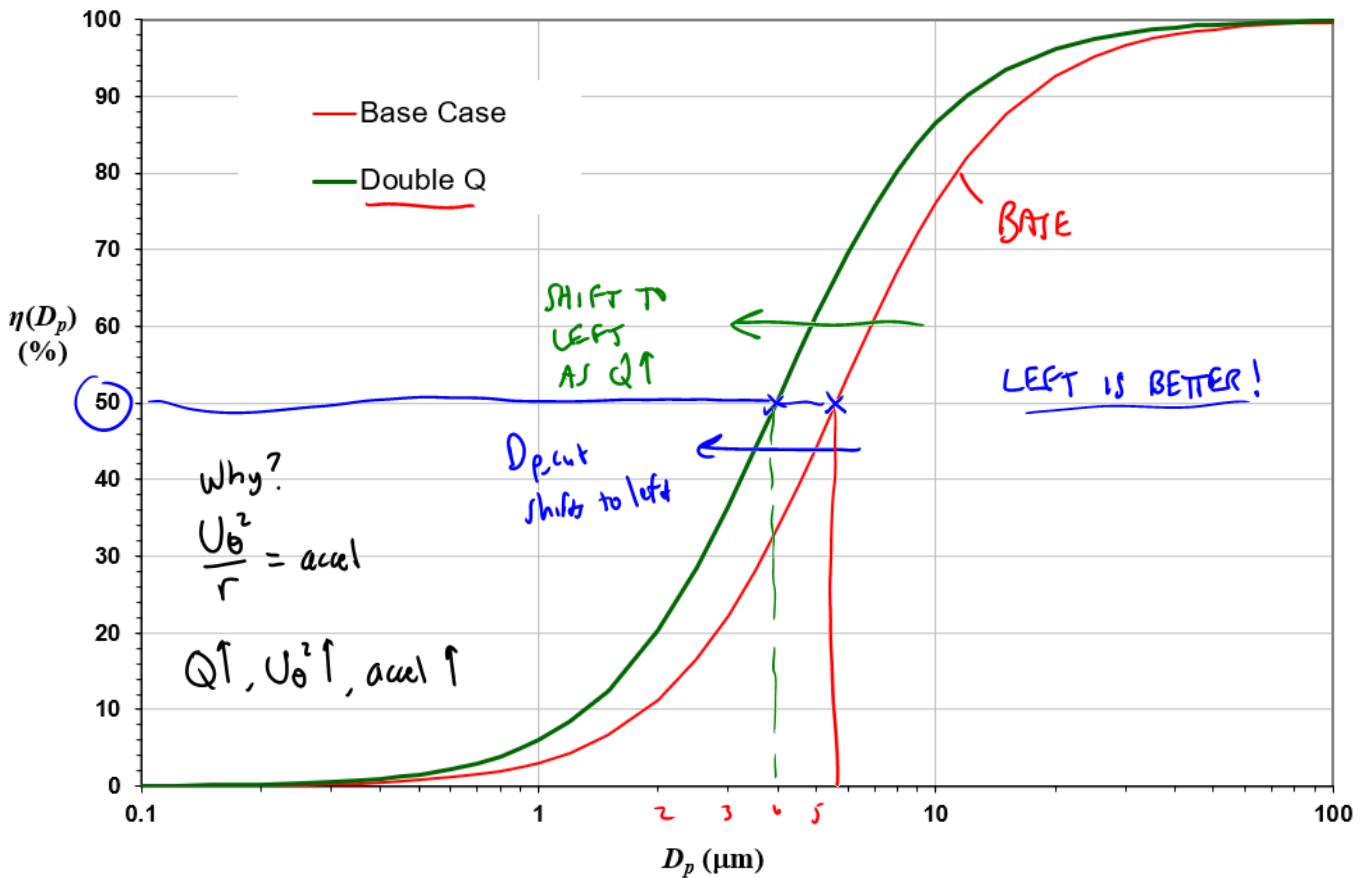
$$\dot{W}_{\text{blower}} = \frac{(0.550 \frac{\text{m}^3}{\text{s}})(22896 \frac{\text{N}}{\text{m}^2})}{0.875} \left(\frac{\text{W}\cdot\text{s}}{\text{N}\cdot\text{m}}\right) \left(\frac{1 \text{ kW}}{1000 \text{ W}}\right) = 14.4 \text{ kW} = \dot{W}_{\text{blower}}$$

★ REPEAT FOR MANY  $D_p$ 's

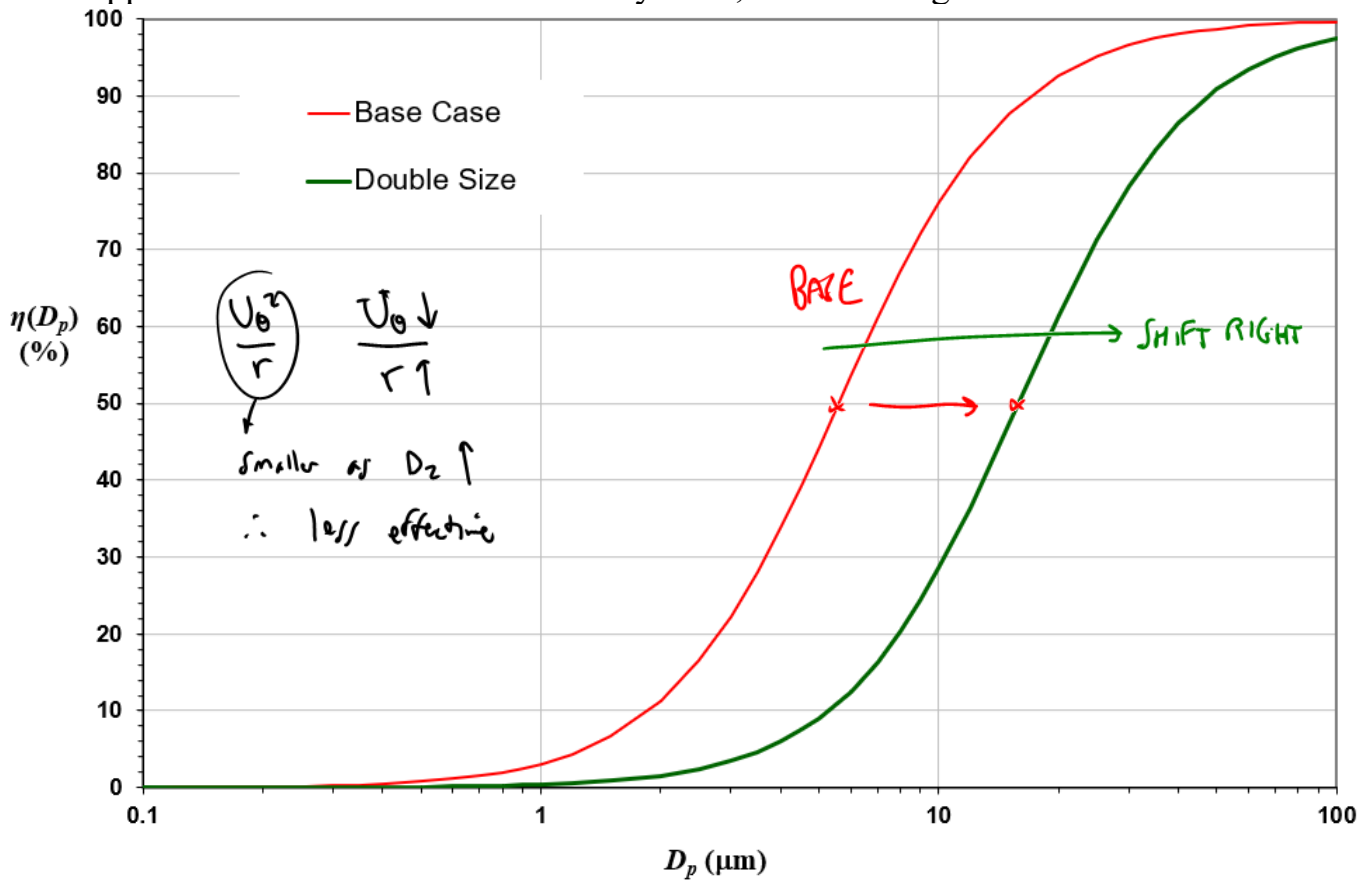
Grade efficiency plot (from Excel results at various particle diameters):



What happens if we *double the flow rate* through the cyclone, all else being the same?



What happens if we **double the size** of the cyclone, all else being the same as the **base case**?



What happens if we **halve the size** of the cyclone, all else being the same as the **base case**?

