

We can conclude

(a) $Pr < 1$

(b) $Pr \approx 1$

(c) $Pr > 1$

$$Pr = \frac{\nu}{K}$$

ν is bigger than K since momentum diffuses faster than heat energy

Eg. water - $Pr \approx 7$

air - $Pr \approx 0.7$ (opposite)

Reynolds Analogy

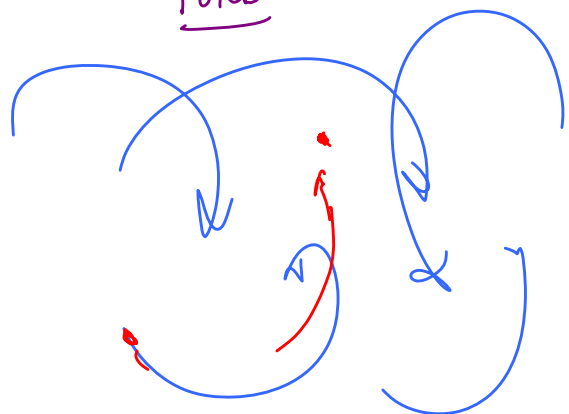
- For turbulent flow, diffusion is dominated by large eddies mixing up the flow

LAM



molecular diffusion

TURB



Diffusion coefficients for turbulent flow \gg those of laminar flow

Reynolds analogy \rightarrow energy, momentum, & mass diffusion all occur at similar rates in turbulent flow (due to the eddies)

Usefulness \rightarrow easy to measure heat transfer characteristics
hard " " " species " "

We can use heat transfer correlations to predict mass transfer (species) diffusion

Define	turbulent Prandtl #	$Pr_t = \frac{\nu_t}{K_t}$
"	Schmidt #	$Sc_t = \frac{\nu_t}{D_{aj,t}}$
"	turb. Lewis #	$Le_t = \frac{K_t}{D_{aj,t}}$

Mixing or Diffusion is dominated by the turbulent eddies

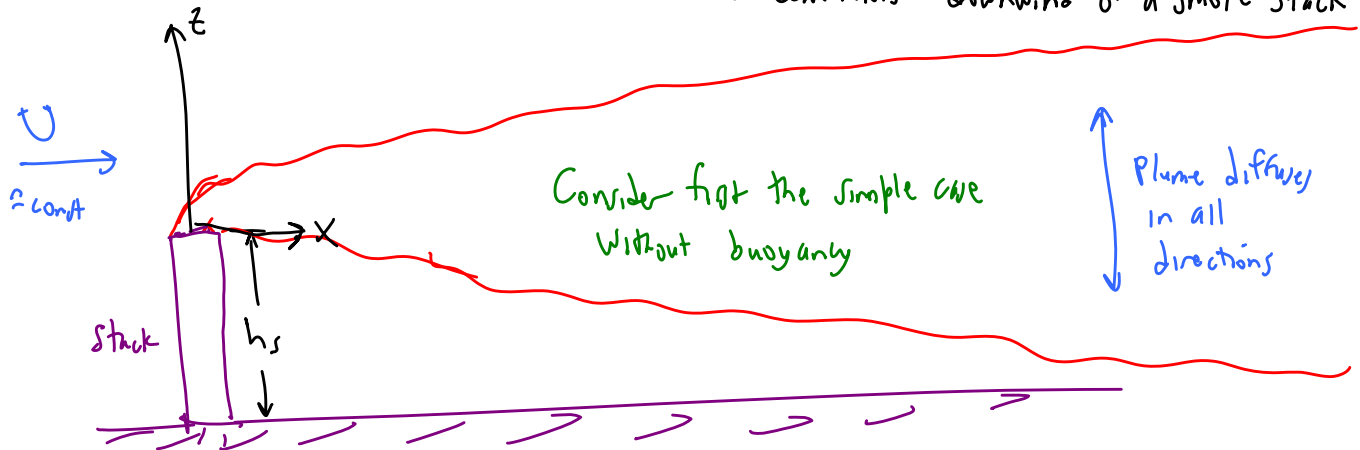
What is the approx. value of $Pr_t \approx Sc_t \approx Le_t \approx 1$

Mass, momen., & heat are diffused by the turbulent eddies, all at \approx same rate

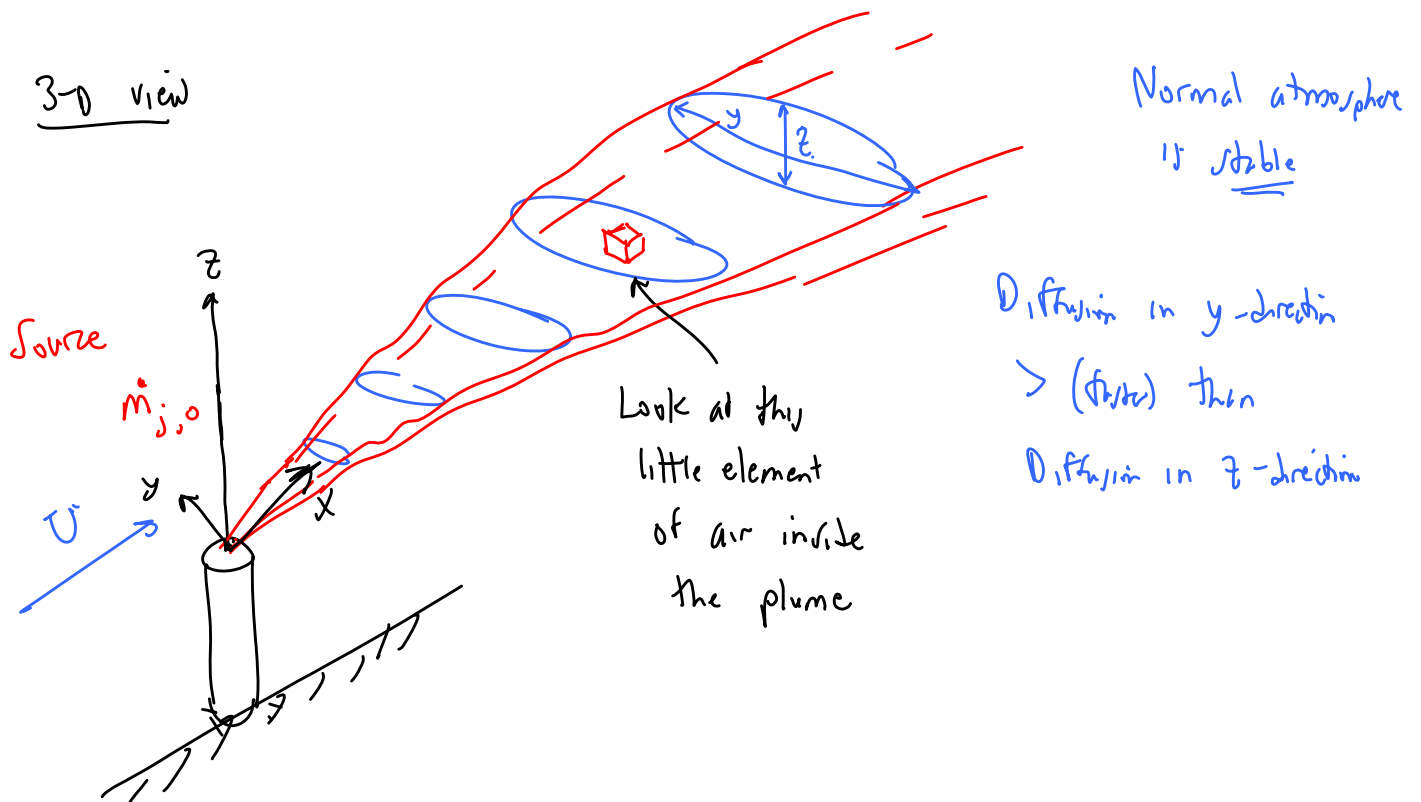
Reynolds analogy

Gaussian Plume Model

→ useful model to predict air pollution concentration downwind of a smoke stack



3-D view

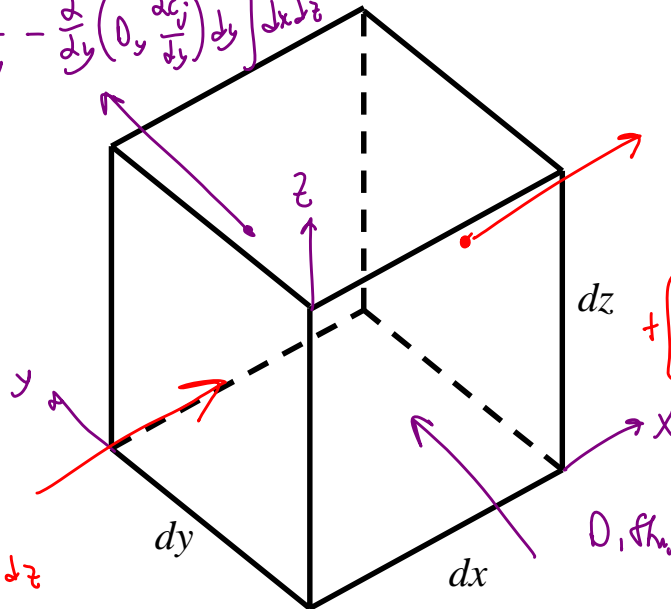


Consider a small element of air in the plume of dimensions dx , dy , and dz as sketched here.

Consl. of mass balance of species $j \rightarrow$ Use Taylor series expansion, truncate

(Notation $\rightarrow D_y = D_{aj,y} \rightarrow$ Diffusion coeff. in y -direction) to first-order

$$\dot{m}_{out} = \left[-D_y \frac{\partial c_j}{\partial y} - \frac{\partial}{\partial y} \left(D_y \frac{\partial c_j}{\partial y} \right) dy \right] dx dz$$



$$\dot{m}_{out} = \left[U c_j + \frac{\partial}{\partial x} (U c_j) dx \right] dy dz + \left[-D_x \frac{\partial c_j}{\partial x} - \frac{\partial}{\partial x} \left(D_x \frac{\partial c_j}{\partial x} \right) dx \right] dy dz$$

"Advection"

$$\dot{m}_{in} = U c_j dy dz$$

+

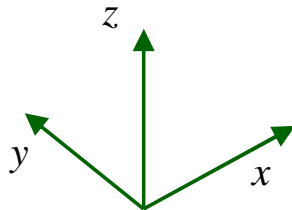
Diffusion

$$-D_x \frac{\partial c_j}{\partial x} dy dz$$

$\frac{m^2}{s} \quad \frac{m}{m^3} \quad \frac{m}{m} \quad \frac{m}{m}$

Diffusion only (no advection)

$$\dot{m}_{in} = -D_y \frac{\partial c_j}{\partial y} dx dz$$



+ Similar terms in z -direction

Let's sum up all the mass flow rates into our little element

$$\frac{dm_j}{dt} = \forall \frac{dc_j}{dt} = \underline{dx dy dz} \frac{dc_j}{dt} = \overset{IN_x}{U c_j dy dz} - \overset{OUT_x}{\left[U c_j + \frac{\partial}{\partial x} (U c_j) dx \right] dy dz} - \underline{D_x \frac{\partial c_j}{\partial x} dy dz} - \left[-D_x \frac{\partial c_j}{\partial x} - \frac{\partial}{\partial x} \left(D_x \frac{\partial c_j}{\partial x} \right) dx \right] dy dz$$

+ y -terms + z -terms

Add up all terms (all 6 of them) (6 func), $\div dx dy dz$

$$\star \quad \frac{\partial c_j}{\partial t} = -\frac{\partial}{\partial x}(U c_j) + \frac{\partial}{\partial x}\left(D_x \frac{\partial c_j}{\partial x}\right) + \frac{\partial}{\partial y}\left(D_y \frac{\partial c_j}{\partial y}\right) + \frac{\partial}{\partial z}\left(D_z \frac{\partial c_j}{\partial z}\right)$$