

Today, we will:

- Continue to discuss **inertial separation** (particles in curved flows)
- Discuss the analogy between gravimetric settling and inertial separation
- Compare laminar vs. well-mixed inertial separation in curved ducts

Review of equations so far for inertial separation in a curved duct:

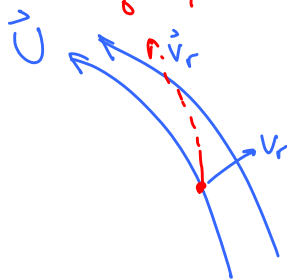
$$\vec{F}_{\text{centrifugal}} = (m_p - m_{\text{air}}) \frac{U_\theta^2}{r} = \pi \frac{D_p^3}{6} (\rho_p - \rho) \frac{U_\theta^2}{r} = \text{centrifugal force, radially outward}$$

$$\vec{F}_{\text{drag}} = -\frac{1}{8} \rho \frac{C_D}{C} \pi D_p^2 \vec{v}_r |\vec{v}_r| = -\frac{1}{8} \rho \frac{C_D}{C} \pi D_p^2 v_r^2 = \text{aerodynamic drag force, radially inward}$$

(same aerodynamic drag force that we used previously)

Consider the simplest case in which v_r is constant, and the two above forces must balance:

$$\pi \frac{D_p^3}{6} (\rho_p - \rho) \frac{U_\theta^2}{r} = \frac{1}{8} \rho \frac{C_D}{C} \pi D_p^2 v_r^2 \Rightarrow \frac{8}{6} D_p \frac{\rho_p - \rho}{\rho} \frac{C}{C_D} \frac{U_\theta^2}{r} = v_r^2$$



$$v_r = \sqrt{\frac{4 \rho_p - \rho}{3 \rho} \frac{U_\theta^2}{r} D_p \frac{C}{C_D}}$$

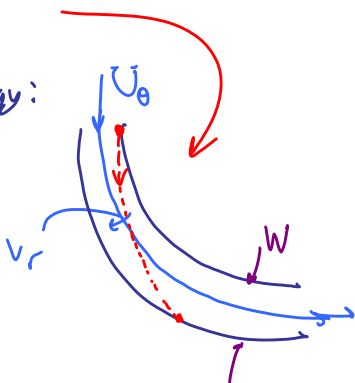
= radial "settling" velocity in a curved duct due to inertial separation

Compare to gravimetric settling in quiescent air (from a previous lecture):

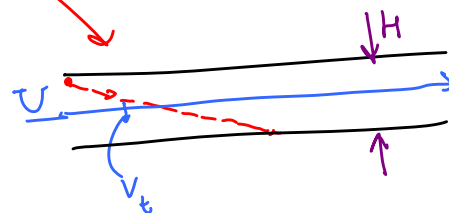
terminal settling velocity $V_t = \sqrt{\frac{4 \rho_p - \rho}{3 \rho} g D_p \frac{C}{C_D}}$

Radial settling is identical to gravimetric settling except replace g by $\frac{U_\theta^2}{r}$

Analogy:



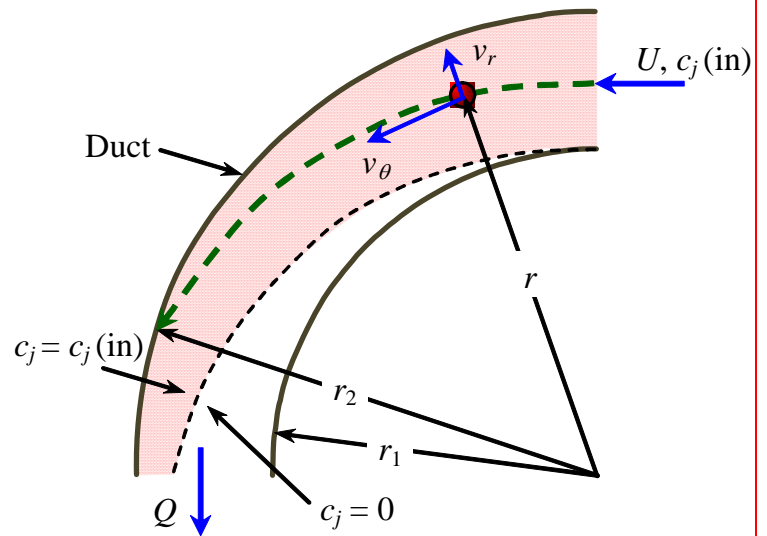
↔
Analogy
to



Example: Comparison of Centrifugal and Gravitational Settling

Given: Dusty air enters a curved duct at average speed U . Aerosol particles of a certain diameter D_p have a terminal settling speed of $V_t = 0.00025$ m/s in quiescent air. At the instant of time shown, a particle of diameter D_p is at radius $r = 0.32$ m.

To do: Calculate the air speed U such that the radial velocity v_r of the particle is the *same* as its terminal settling velocity. Give your answer in m/s to three significant digits.



Solution:

• We showed that v_r & V_t have the same equation, except g is replaced by

$$\frac{U_\theta^2}{r}$$

$$\text{For } v_r = V_t \rightarrow \frac{U_\theta^2}{r} = g \quad - \quad U_\theta = \sqrt{rg}$$

$$= \sqrt{(0.32 \text{ m})(9.807 \text{ m/s}^2)}$$

$$= 1.7715 \text{ m/s}$$

$$\boxed{U_\theta = 1.77 \text{ m/s}}$$

Not very large

$$\text{For } U_\theta = 10 \text{ m/s} \quad - \quad \frac{U_\theta^2}{r} = \frac{(10 \text{ m/s})^2}{0.32 \text{ m}} = 312.5 \frac{\text{m}}{\text{s}^2} = \underline{\underline{32g}}$$

Laminar vs. well-mixed settling:

We discussed this twice previously:

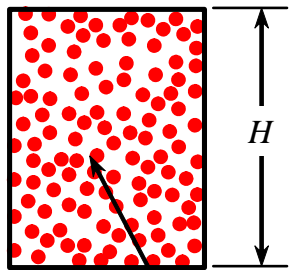
1. Gravimetric settling in a room or container
2. Gravimetric settling in a horizontal duct

Now we apply the same principles to

3. Inertial separation in a curved duct.

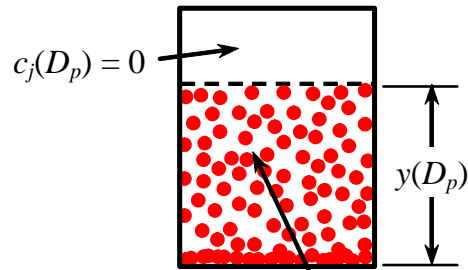
1. Gravimetric settling in a room or container:

Initial state ($t = 0$)



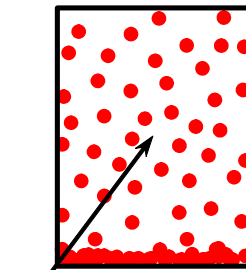
$$c_j(D_p) = c_j(D_p)_0$$

Laminar settling ($t = t_1$)



$$c_j(D_p) = c_j(D_p)_0$$

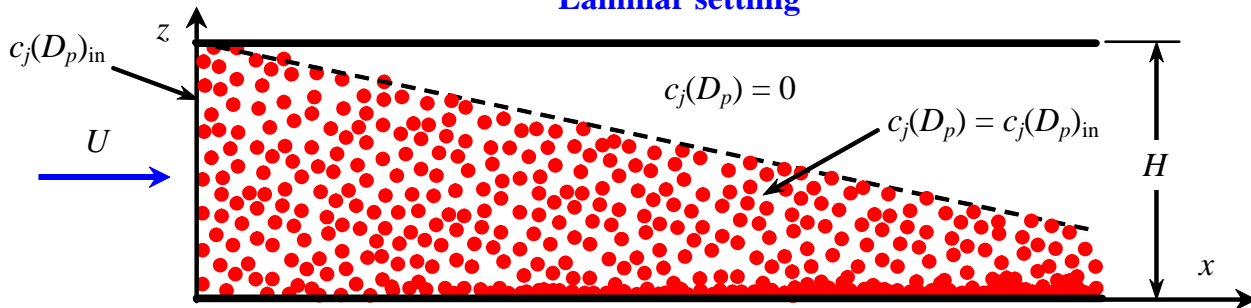
Well-mixed settling ($t = t_1$)



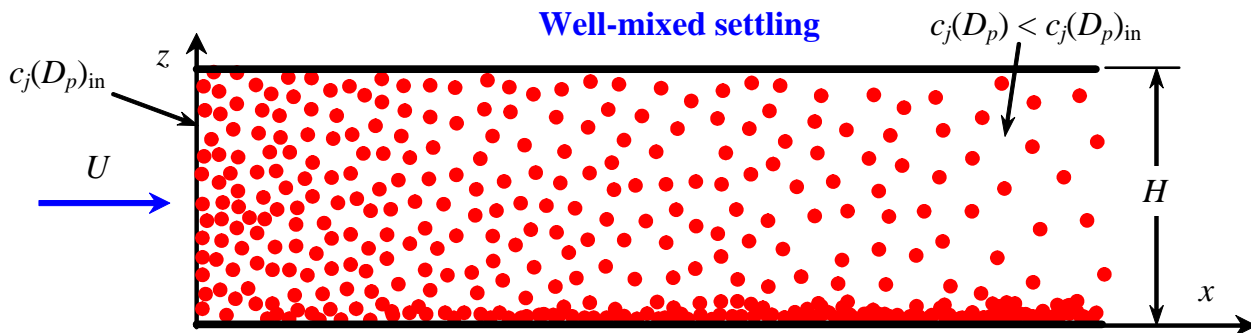
$$c_j(D_p) < c_j(D_p)_0$$

2. Gravimetric settling in a horizontal duct:

Laminar settling

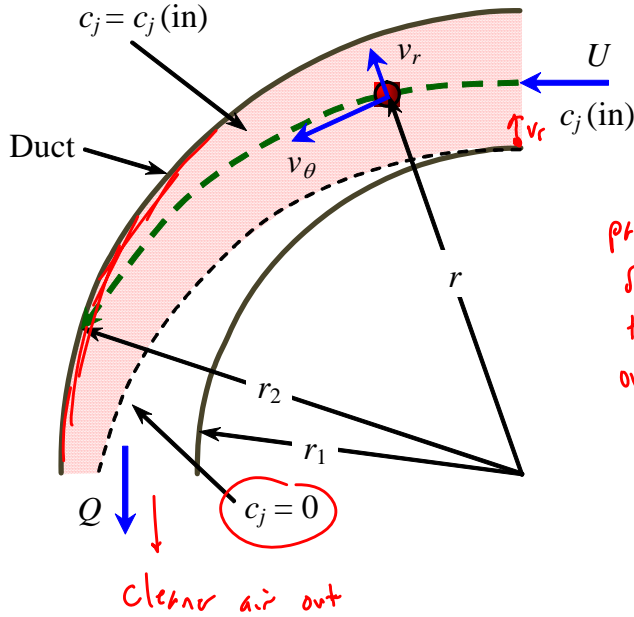


Well-mixed settling

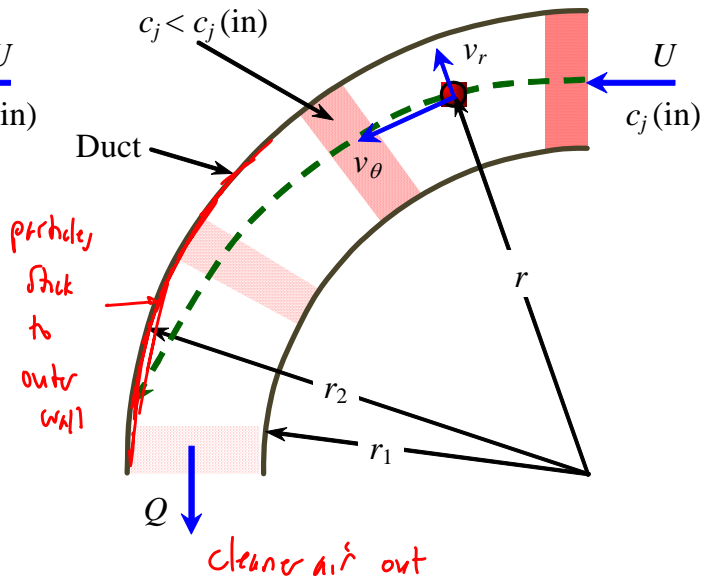


3. Inertial separation in a curved duct:

Laminar settling



Well-mixed settling



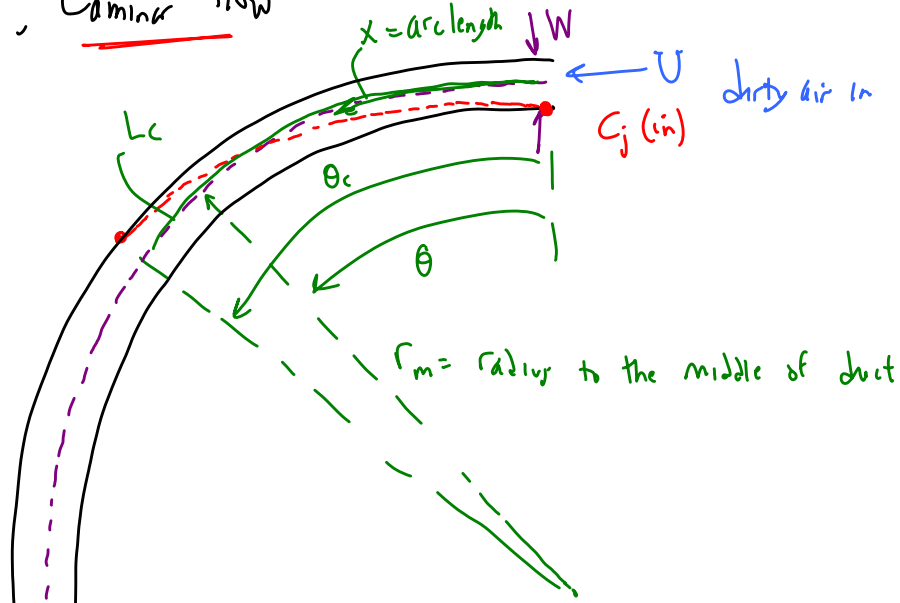
Simplest Approx, Laminar flow

$$r_m \gg W$$

Then we can use $r \approx r_m = \text{constant}$

$$x = r_m \theta$$

θ in radians



L = total arc length from inlet to outlet @ the centerline
 L_c = critical arc length at which all particles are cleaned up

At $r = r_m \rightarrow$ let's use $r = r_m = \text{constant}$ in our eq.

$$V_r = \sqrt{\frac{4}{3} \frac{\rho_f - \rho}{\rho} \frac{U_0^2}{r_m} D_p \frac{C}{C_0}} \approx \text{const}$$

Worst case particle travels distance W radially outward in some time t

$$\underline{W = v_r t}$$

$$\therefore \underline{L_c = U_0 t} \text{ or } Ut$$

equating t

$$\underline{L_c = \frac{W U_0}{v_r}}$$

$$\theta_c = \frac{L_c}{r_m}$$

Critical arc length

Removal efficiency:

$$\text{if } x < L_c, \frac{C_i}{C_j(\text{in})} = 1 - \frac{x}{L_c} \rightarrow E = 1 - \frac{C_j}{C_j(\text{in})}$$

$$\boxed{E = \frac{x}{L_c}}$$

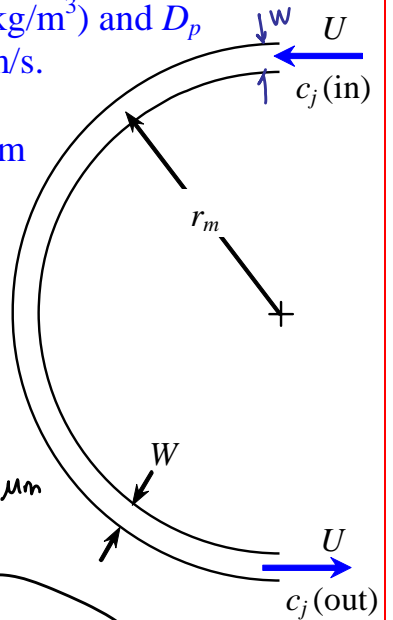
$$\underline{\text{If } x > L_c, E = 1 \text{ or } \underline{\underline{100\%}}}$$

Example: Removal efficiency of a curved duct as a function of particle diameter

Given: Monodisperse aerosol particles of unit density ($\rho_p = 1000 \text{ kg/m}^3$) and $D_p = 15.0$ microns enter a 180° curved duct at average speed $U = 10.3 \text{ m/s}$. The air is at STP ($\rho = 1.184 \text{ kg/m}^3$, $\mu = 1.849 \times 10^{-5} \text{ kg/(m s)}$). The middle duct radius is $r_m = 0.500 \text{ m}$ and the duct width is $W = 22.5 \text{ mm}$ (0.0225 m). We assume laminar settling, and we assume that the particles stick to the outer wall when they hit, and are therefore removed from the flow.

To do: Calculate your best estimate of the predicted removal efficiency E of these particles (% to three significant digits).

Solution: The Cunningham correction factor is $C = 1.0168$, and Stokes flow is appropriate ($C_D = 24/\text{Re}$).



Equations: $v_r = \sqrt{\frac{4 \rho_p - \rho}{3} \frac{\rho U_\theta^2}{\rho} \frac{D_p}{r} \frac{C}{C_D}}$, $\text{Re} = \frac{\rho v_r D_p}{\mu}$, $C_D = \frac{24}{\text{Re}}$

Laminar settling model: $E = 1 - \frac{c_j}{c_j(\text{in})} = \frac{x}{L_c}$, where $L_c = W \frac{U_\theta}{v_r}$, $x = r_m \theta$. (plug in C_D too)

Solve for $v_r \rightarrow v_r^2 = \frac{4}{3} \frac{\rho_p - \rho}{\rho} \frac{U_\theta^2}{r} D_p \frac{C}{\mu} \Rightarrow v_r = \frac{1}{18} \frac{(\rho_p - \rho)}{\mu r_m} U_\theta^2 D_p^2 C$

for $D_p = 15 \mu\text{m} \rightarrow v_r = \frac{1}{18} \frac{(1000 - 1.184) \text{ kg/m}^3 (10.3 \text{ m/s})^2 (15 \times 10^{-6} \text{ m})^2 (1.0112)}{(1.849 \times 10^{-5} \text{ kg/m s})(0.500 \text{ m})} = 0.1449 \text{ m/s}$

But $x = (0.50 \text{ m}) \pi^{180^\circ} = 1.5708 \text{ m}$

Then $L_c = \frac{W U_\theta}{v_r}$; $E = \frac{x}{L_c} = \frac{x v_r}{W U_\theta}$

So $E = \frac{(1.5708 \text{ m})(0.1449 \text{ m/s})}{(0.0225 \text{ m})(10.3 \text{ m/s})} = 0.982 = \boxed{98.2\%}$

Check $\text{Re} \rightarrow \text{Re} = \frac{\rho D_p v_r}{\mu} = \frac{(1.184 \text{ kg/m}^3)(15 \times 10^{-6} \text{ m})(0.1449 \text{ m/s})}{1.849 \times 10^{-5} \text{ kg/m s}} = \boxed{0.139 = \text{Re}}$

Ans. $E \approx 98\%$

A little too big $\rightarrow \text{Re} \approx 0.1$ for Stokes flow, but this should be a reasonable estimate