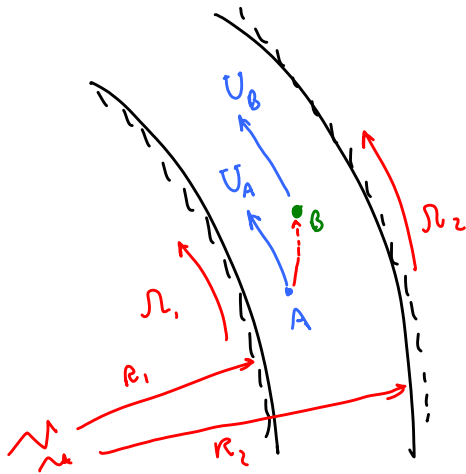


Today, we will:

- Continue to discuss the centrifugal instability (Taylor instability)
- Begin a discussion about stability of locally parallel flows – the Orr-Sommerfeld Eq.



Basic state  $U_\theta(r)$  for a given  $\Omega_1, \Omega_2$

Angular momentum:  $r \tilde{U}_\theta = \text{constant}$

$$r_A U_{\theta A} = r_B \tilde{U}_{\theta B} \quad (\text{ignoring viscosity effects})$$

$$\therefore \tilde{U}_{\theta B} = \frac{r_A U_{\theta A}}{r_B}$$

But, at radius B,  $U_\theta = U_{\theta B}$

Stability  $\rightarrow$  if the actual  $\tilde{U}_{\theta B} > U_{\theta B}$  then the flow is potentially unstable

Stability criterion is if  $r_A U_{\theta A} > r_B U_{\theta B}$  it is potentially unstable

Viscosity effects will try to keep it stable

Cases: 1) Solid Body rotation  $U_\theta = r\Omega$  ( $\Omega_1 = \Omega_2 = \Omega$ )

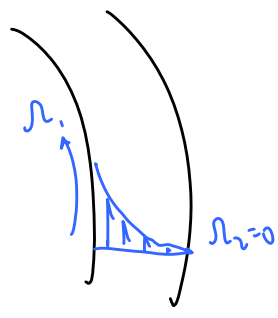
$$r_A^2 \Omega < r_B^2 \Omega \quad \text{since } r_B > r_A$$

This basic state is stable

2) Outer cyl rotating, inner cyl. stationary

$$U_{\theta B} > U_{\theta A} \quad ; \quad r_B > r_A \quad \rightarrow \quad r_A U_{\theta A} < r_B U_{\theta B} \quad \rightarrow \quad \text{Stable}$$

3) Inner cyl. rotating, outer cyl. stationary



$r_A U_{\theta A}$  ?  $r_B U_{\theta B}$   
 $r_A < r_B$   
 but  $U_{\theta A} > U_{\theta B}$

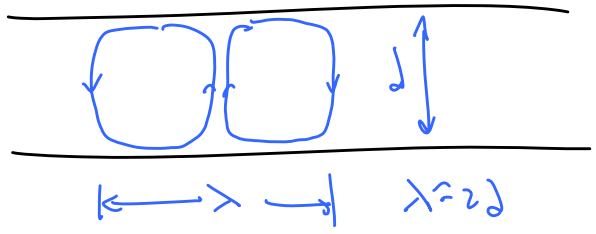
Potentially unstable

Define a Taylor #

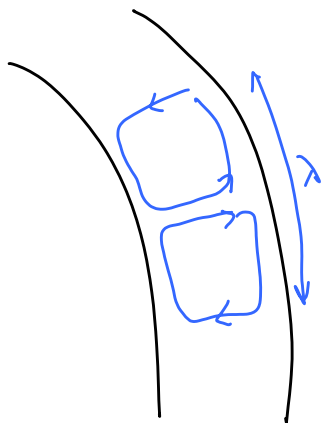
$$T_a = 2 \left( \frac{V_1 d}{\nu} \right)^2 \frac{d}{R_1}$$

$V_1 = \Omega_1 R_1$      $d = R_2 - R_1 = \text{gap thickness}$

There is a critical  $T_a$  for which flow is unstable



Bénard



$\lambda \approx 2d$

Taylor

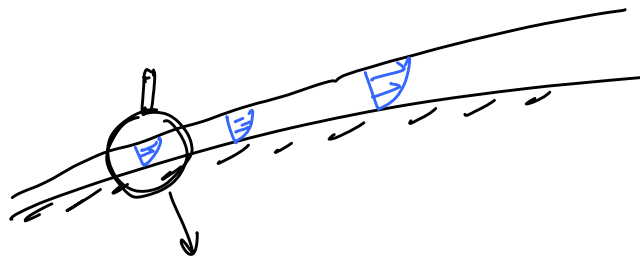
See Kundu for details

## D. Stability of locally parallel flows (Kundu - sec. 12.8)

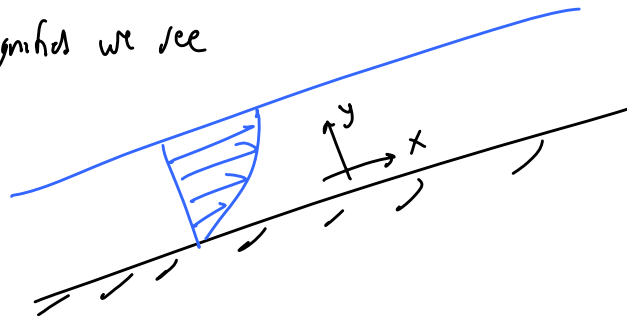
1. Intro Some flows are parallel e.g. fully developed channel flow  
Couette flow, etc



Other flows are nearly parallel e.g. thin BLs, thin wakes, jets, etc.



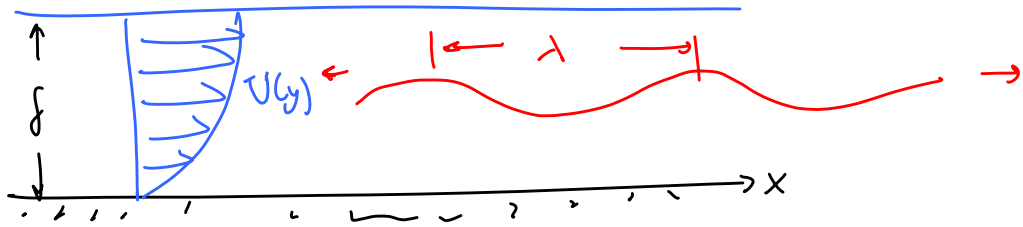
Magnified we see



Approx. the basic state as  $\vec{U} = (U(y), 0, 0)$   $V, W$  are very small compared to  $U$

Locally Parallel Flow Approximation  $\rightarrow U \neq \text{fcn. of } x$   
(local analysis only)

- Advantage
- simpler math
  - We can examine temporal stability with the method of normal modes



## 2. Linear Stability Analysis (temporal analysis)

• Step 0 → set of eqs → Use N-S ; ignore gravity

notation →  $\tilde{u}_{d,i}$  =

- total velocity (tildes)
- dimensional (subscript d)
- i component (tensor notation)

Cont

$$\frac{\partial \tilde{u}_{d,i}}{\partial x_{d,i}} = 0$$

4 eqs, 4 unknowns (1d)

Mom

$$\frac{\partial \tilde{u}_{d,i}}{\partial t_d} + \tilde{u}_{d,j} \frac{\partial \tilde{u}_{d,i}}{\partial x_{d,j}} = -\frac{1}{\rho} \frac{\partial \tilde{p}_d}{\partial x_{d,i}} + \nu \frac{\partial^2 \tilde{u}_{d,i}}{\partial x_{d,j} \partial x_{d,j}}$$

(2d)

Non-dimensionalize everything

let  $L =$  characteristic length scale →  $x_i = \frac{x_{d,i}}{L}$

$U_0 =$  " velocity "  $\tilde{u}_i = \frac{\tilde{u}_{d,i}}{U_0}$

$\frac{L}{U_0} =$  " time "  $t = t_d \frac{U_0}{L}$

$\rho U_0^2 =$  pressure  $\tilde{p} = \frac{\tilde{p}_d}{\rho U_0^2}$

Plug these into (1d) & (2d) } see handout, get Eqs (1) & (2)

Step 1 Basic State  $\rightarrow \vec{U} = (U(y), 0, 0)$

pressure = P

Plug into eqs (1) & (2)  $\rightarrow$  get (1b) & (2b) on handout

Cont  $\rightarrow \frac{\partial U_i}{\partial x_i} = 0 \rightarrow \frac{\partial U}{\partial x} + \frac{\partial U}{\partial y} + \frac{\partial U}{\partial z} = 0 \rightarrow \underline{0=0}$  (1b)  
 $U = U(y)$

x-mom  $\rightarrow \frac{\partial U}{\partial t} + U \frac{\partial U}{\partial x} + V \frac{\partial U}{\partial y} + W \frac{\partial U}{\partial z} = -\frac{\partial P}{\partial x} + \frac{1}{Re} \nabla^2 U = 0$  (2b)

y-mom  $\rightarrow 0 = -\frac{\partial P}{\partial y} \rightarrow P \neq \text{func of } y$   
z-mom  $\rightarrow 0 = -\frac{\partial P}{\partial z} \rightarrow P \neq \text{func of } z$   
 $\left. \begin{array}{l} P \neq \text{func of } y \\ P \neq \text{func of } z \end{array} \right\} P = P(x) \text{ only}$

So  $-\frac{\partial P}{\partial x} + \frac{1}{Re} \nabla^2 U = 0$  (2b)

Step 2 Add disturbance

$\tilde{u} = U + u$   
 $\tilde{v} = 0 + v$   
 $\tilde{w} = 0 + w$   
 $\tilde{p} = P + p$   
*lower case without tilde = disturbance*  
*in general func of (x, y, z, t)*

Plug these into (1) & (2) to get (1t) & (2t)

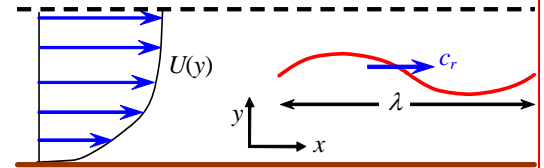
Step 3  $\rightarrow$  subtract (1t)-(1b), (2t)-(2b)  $\rightarrow$  Step 4 Linearize  $\rightarrow$  get (1d) & (2d)

# Temporal Stability of Locally Parallel Flow – The Orr-Sommerfeld Equation

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Latest revision: 16 February 2008

## 1. Problem Setup:

Consider an incompressible, locally parallel flow with some known steady basic state  $U(y)$ . We examine this problem using linear stability analysis. *Note:* A boundary layer type of flow is sketched, but the procedure applies to *any* kind of parallel or nearly parallel flow.



## 2. Summary of Linear Stability Analysis:

The in-class analysis follows Kundu, Section 12.8 closely, filling in some of the details. Start with the normalized incompressible Navier-Stokes equations for *total* flow variables ( $\tilde{q}$ ):

$$\frac{\partial \tilde{u}_i}{\partial x_i} = 0 \quad (1) \quad \text{and} \quad \frac{\partial \tilde{u}_i}{\partial t} + \tilde{u}_j \frac{\partial \tilde{u}_i}{\partial x_j} = -\frac{\partial \tilde{p}}{\partial x_i} + \frac{1}{\text{Re}} \frac{\partial^2 \tilde{u}_i}{\partial x_j \partial x_j} \quad (2) \quad \text{where} \quad \text{Re} \equiv \frac{U_0 L}{\nu}$$

and  $U_0$  and  $L$  are a characteristic velocity and a characteristic length, respectively. This represents 4 equations and 4 unknowns, nonlinear p.d.e.s.

- **Step 1.** Start with the basic state ( $Q$ ):  $U_i = (U(y), 0, 0)$ . Continuity yields  $\nabla \cdot Q = 0$  (1b). The  $y$  and  $z$  momentum equations show

that  $P = P(x)$  only, and the  $x$ -momentum reduces to  $0 = -\frac{dP}{dx} + \frac{1}{\text{Re}} \nabla^2 U$  (2b).

- **Step 2.** Add disturbances ( $\tilde{u} = U + u, \tilde{v} = 0 + v, \tilde{w} = 0 + w, \tilde{p} = P + p$ ), and plug them into (1) & (2): This generates the *total equations* (1t) and (2t).

- **Step 3.** Subtract the basic state equations from the total equations: This generates the *disturbance equations* (1d) and (2d).

- **Step 4.** Linearize the disturbance equations to generate the *linearized disturbance equations*  $\frac{\partial u_i}{\partial x_i} = 0$  (11) and  $\star$

$$\frac{\partial u}{\partial t} + U \frac{\partial u}{\partial x} + v \frac{dU}{dy} = -\frac{\partial p}{\partial x} + \frac{1}{\text{Re}} \nabla^2 u, \quad \frac{\partial v}{\partial t} + U \frac{\partial v}{\partial x} = -\frac{\partial p}{\partial y} + \frac{1}{\text{Re}} \nabla^2 v, \quad \frac{\partial w}{\partial t} + U \frac{\partial w}{\partial x} = -\frac{\partial p}{\partial z} + \frac{1}{\text{Re}} \nabla^2 w \quad (21). \quad \star$$

This still represents 4 equations and 4 unknowns, but the equations are now *linear*. (*Note:* the *disturbance* variables are now the unknowns since the basic state is known.) These are still p.d.e.s since  $u, v, w$ , and  $p$  are functions of  $(x, y, z, t)$ .

- **Step 5.** Solve the linearized disturbance equations (11) and (21): We use the method of normal modes.

**Method of Normal Modes:** Assume disturbances that are *periodic* in  $x$  and  $z$ , but *not growing or decaying* in  $x$  or  $z$ , and *may be periodic and may be growing or decaying* in  $t$ . (*temporal instability*.) Specifically, let the disturbances be of the form

$$u(x, y, z, t) = \hat{u}(y) e^{i(kx + mz - ckt)}, \quad v(x, y, z, t) = \hat{v}(y) e^{i(kx + mz - ckt)}, \quad w(x, y, z, t) = \hat{w}(y) e^{i(kx + mz - ckt)}, \quad \text{and} \quad \text{here } \sigma = -ikc$$

$$p(x, y, z, t) = \hat{p}(y) e^{i(kx + mz - ckt)},$$

where variables with hats are **complex amplitudes**.  $k$  and  $m$  are the  $x$  and  $z$  components, respectively, of **wavenumber vector**  $\vec{K}$ . For temporal stability analysis, both  $k$  and  $m$  must be *real*, while **complex wave speed**  $c$  can be *complex*. (Otherwise spatial instability would also be possible.) Plug these disturbances into Eqs. (11) and

(21) to get the *normal mode equations*:  $ik\hat{u} + \hat{v}_y + im\hat{w} = 0$  (1n),  $ik(U - c)\hat{u} + \hat{v}U_y = -ik\hat{p} + \frac{1}{\text{Re}} [\hat{u}_{yy} - (k^2 + m^2)\hat{u}]$ ,

$$ik(U - c)\hat{v} = -\hat{p}_y + \frac{1}{\text{Re}} [\hat{v}_{yy} - (k^2 + m^2)\hat{v}], \quad \text{and} \quad ik(U - c)\hat{w} = -im\hat{p} + \frac{1}{\text{Re}} [\hat{w}_{yy} - (k^2 + m^2)\hat{w}] \quad (2n).$$

*Note:* For convenience in Eqs. (1n) and (2n), subscript  $y$  denotes differentiation with respect to  $y$ . We are now down to 4 o.d.e.s and 4 unknowns since  $U(y)$  is known, along with its derivatives.

**Squire's Theorem:** In 2-D parallel flow, for each unstable 3-D disturbance, there corresponds a *more unstable* 2-D

**disturbance**. In other words, the *most unstable* case is the 2-D one:  $m = 0$  &  $\hat{w} = 0$ . The normal mode equations simplify:

$$ik\hat{u} + \hat{v}_y = 0 \quad (4), \quad ik(U - c)\hat{u} + \hat{v}U_y = -ik\hat{p} + \frac{1}{\text{Re}} [\hat{u}_{yy} - k^2\hat{u}] \quad (5), \quad \text{and} \quad ik(U - c)\hat{v} = -\hat{p}_y + \frac{1}{\text{Re}} [\hat{v}_{yy} - k^2\hat{v}] \quad (6).$$

We are now down to 3 o.d.e.s and 3 unknowns,  $\hat{u}(y)$ ,  $\hat{v}(y)$ , and  $\hat{p}(y)$ .

**Orr-Sommerfeld Equation:** Define a disturbance stream function,  $\psi(x, y, t) = \phi(y) e^{ik(x - ct)}$ . *Note:*  $\phi(y)$  is *not* a velocity potential function, but simply the magnitude of the disturbance stream function. Plugging this into Eqs. (4) to (6) yields *one*

*o.d.e. and one unknown:*  $(U - c)(\phi_{yyy} - k^2\phi) - U_{yy}\phi = \frac{1}{ik \text{Re}} [\phi_{yyyy} - 2k^2\phi_{yy} + k^4\phi]$  (7), the **Orr-Sommerfeld equation**.

- **Step 6.** Examine stability: Finally, we examine solutions of the Orr-Sommerfeld equation (to be done in class).

$C = \text{complex wave speed}$

$$C = C_r + iC_i$$

For temporal instability analysis,  $k$  &  $\omega$  are real, but  $C$  may be complex

Examine  $e^{-ikt}$

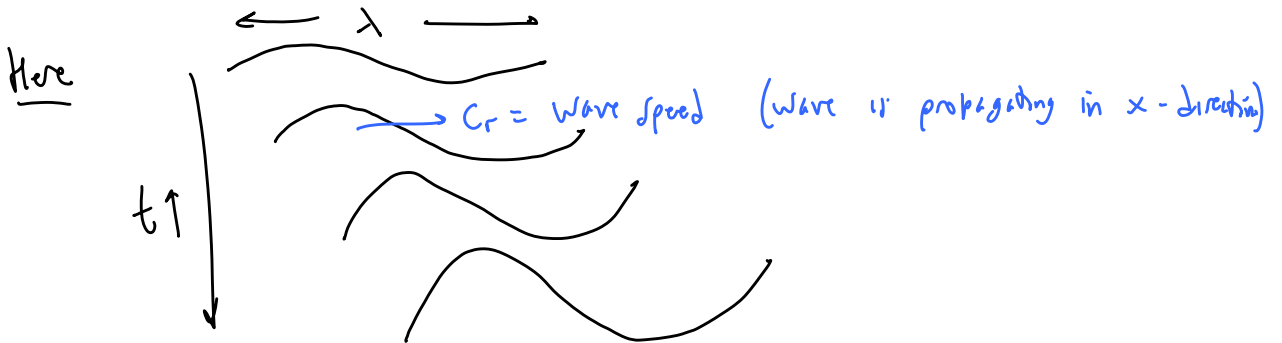
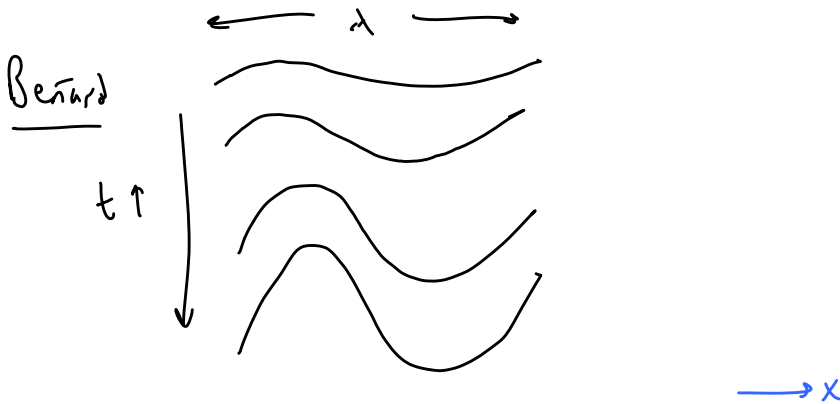
$$e^{-ikt} = e^{-ikC_r t} e^{kC_i t}$$

oscillating in time  
(periodic in time)

represents the growth  
or decay - the  
stability

$C_r$  represents the wave propagation speed.

if  $C_i < 0$  stable  
if  $C_i > 0$  unstable



$C_r$  determines the wave speed  
 $C_i$  determines the stability