1) compression spring

squared and ground ends

$$d = 0.105 \text{ in}$$

OK preferred wire size Table 14-2 Norton

$$OD = 0.755 \text{ in}$$

$$L_f = 2.25 \text{ in}$$

$$N_t = 11.75$$

assume A228 music wire

$$N_a = N_t - 2 = 9.75$$
 Fig. 14-9 Norton

$$D = OD - d = 0.650$$
 in

$$C = D / d = 6.1905$$
 Eq. 14-5

$$G = 11.7 \times 10^6 \text{ psi}$$
 Table A-1 Norton

$$k = \frac{d^4 G}{8 D^3 N_a} = \frac{(0.105 in)^4}{8 (0.650 in)^3 (9.75)} \left(\frac{11.7 \times 10^6 lbf}{in^2}\right) = 66.39 lbf/in$$
 Eq. 14.7 Norton

$$A = 184649 \text{ psi}$$
 $b = -0.162$

 $S_{ut} = A d^b = 266.3 \text{ ksi}$ A = 184649 psi b = -0.1625 Eq. 14.3 and Table 14-4 Norton

$$S_{ys} = 0.45 S_{ut} = 119.8 ksi$$

Table 14-8 Norton

$$K_{\text{W}} = \frac{4C - 1}{4C - 4} + \frac{0.615}{C} = 1.2438$$
 $\tau_{\text{MAX}} = K_{\text{W}} \frac{8 \text{ F D}}{\pi d^3} < S_{\text{ys}}$ Eq 14.8b Norton

$$\tau_{\text{MAX}} = K_{\text{W}} \frac{8 \text{ F D}}{\pi d^3} < S_{\text{ys}}$$

$$F_y < \frac{\pi d^3 S_{ys}}{8 K_W D} = \frac{\pi (0.105 in)^3}{8 (1.2438)(0.650 in)} \left(\frac{119.8 \times 10^3 lbf}{in^2} \right) = 67.36 lbf$$

$$L_s = d N_t = 1.234 in$$

 $L_s = d$ $N_t = 1.234$ in shut length (fully compressed) - squared and ground

$$y_s = L_f - L_s = 1.016$$
 in

$$F_s = k y_s = 67.45 \text{ lbf} > F_y$$

 $F_s = k y_s = 67.45 \text{ lbf} > F_y$ will be VERY close to yield at shut length

$$\rho = 0.28 \text{ lbm/in}^3$$

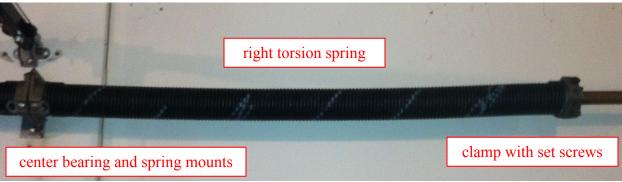
Table A-1 Norton

$$w = \rho (\pi d^2 / 4) (\pi D) N_t = 0.058 lbf$$

2) torsion spring garage door opener

rotating shaft crosses full width of door and has drums on each end three bearings for shaft – left, center, right steel cables connected to bottom of door (one on each side) are wound by drums to lift door two torsion springs – one RH and one LH springs fixed to front wall of garage above door at center springs connected to rotating shaft by clamps with two set screws at rotating end





d = 0.242 in OD = 2.484 in $N_a = 143$ not a preferred wire size Table 14-2 Norton

7 turns of preload when door closed

assume A229 oil tempered wire

D = OD - d = 2.242 in

C = D / d = 9.2645 Eq. 14-5

 $E = 30 \times 10^6 \text{ psi}$ Table A-1 Norton

$$k_{\theta} = \frac{d^4 E}{10.8 D N_a} = \frac{(0.242 in)^4}{10.8 (2.484 in) (143)} \left(\frac{30 \times 10^6 lbf}{in^2}\right) = 26.82 in.lbf/rev$$
 Eq. 14.29 Norton

 $\theta = 7 \text{ rev}$

 $M = k_T \theta = 187.7 \text{ in.lbf} = 15.65 \text{ ft.lbf}$

 $r_{DRUM} = 2$ in radius of drum for cable to lift door

each turn of drum lifts door 2 π r_{DRUM} = 12.57 in

 $F_{CABLE} = M / r_{DRUM} = 93.87 \text{ lbf}$ force in cable to lift door (one cable on each side of door)

static at inside of coil $K_{bi} = \frac{4C^2 - C - 1}{4C(C - 1)} = 1.0875$ Eq. 14.32a Norton

$$\sigma_{i \text{ max}} = K_{bi} \frac{32 \text{ M}}{\pi \text{ d}^3} = (1.0875) \frac{32 (187.7 \text{ in.lbf})}{\pi (0.242 \text{ in})^3} = 146.7 \text{ ksi}$$
 Eq. 14.33a Norton

 $S_{ut} = A d^b = 190.4 \text{ ksi}$ A = 146780 psi b = -0.1833 Eq. 14.3 and Table 14-4 Norton

 $S_y = 0.85 S_{ut} = 161.8 \text{ ksi}$ Table 14-15 Norton

 $N_{_{FS}}=S_{_y}\,/\,\sigma_{_{i\,max}}=1.10$