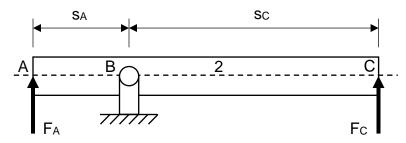
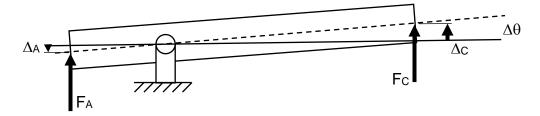
Virtual Work

Rigid bar in horizontal plane



Newtonian
$$\sum M$$
 on 2 about B CCW + $-F_A s_A + F_C s_C = 0$

Infinitesimal kinematically consistent displacements



Virtual work

$$\left\{F_{_{\!A}}\right\}\circ\left\{\Delta_{_{\!A}}\right\}+\left\{F_{_{\!C}}\right\}\circ\left\{\Delta_{_{\!C}}\right\}=0 \\ -F_{_{\!A}}\!\left(s_{_{\!A}}\right.\Delta\theta\right)+F_{_{\!C}}\!\left(s_{_{\!C}}\right.\Delta\theta\right)=0 \\ -F_{_{\!A}}\!\left(s_{_{\!A}}\right.\Delta\theta\right)=0 \\ -F_{_{\!A}}\!\left(s_{_{\!A}}\right.\Delta\theta$$

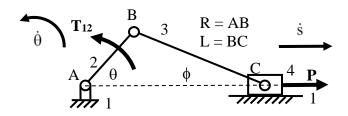
Virtual power

$$\{F_{A}\} \circ \frac{\{\Delta_{A}\}}{\Delta t} + \{F_{C}\} \circ \frac{\{\Delta_{C}\}}{\Delta t} = 0$$
 $\{F_{A}\} \circ \{\dot{r}_{A}\} + \{F_{C}\} \circ \{\dot{r}_{C}\} = 0$

Virtual power for ground connections is zero because the velocity is zero. Virtual power across internal joints is zero because the force of link i on link j dotted with the velocity of the joint will be equal and opposite to the force of link j on link i dotted with the velocity of the joint. However virtual power across internal springs or dampers must be included.

$$\sum \left(\left\{ F_{\rm EXT} \right\} \circ \left\{ \dot{r}_{\rm APPLIED} \right\} \right) + \sum \left(\left\{ M_{\rm EXT} \right\} \circ \left\{ \omega_{\rm APPLIED} \right\} \right) = 0$$

Virtual Work for Slider Crank



$$\dot{s} = -R\dot{\theta}\sin\theta - L\dot{\phi}\sin\phi = -R\dot{\theta}\bigg(\frac{\sin\bigl(\theta+\phi\bigr)}{\cos\phi}\bigg) \qquad \quad \text{from Notes_03_01}$$

$$T_{12} \circ \dot{\theta} + P \circ \dot{s} = 0$$

$$T_{12} = -\frac{P \circ \dot{s}}{\dot{\theta}} = \frac{PR \sin(\theta + \phi)}{\cos \phi}$$
 matches Notes_06_01 for $\mu = 0$