

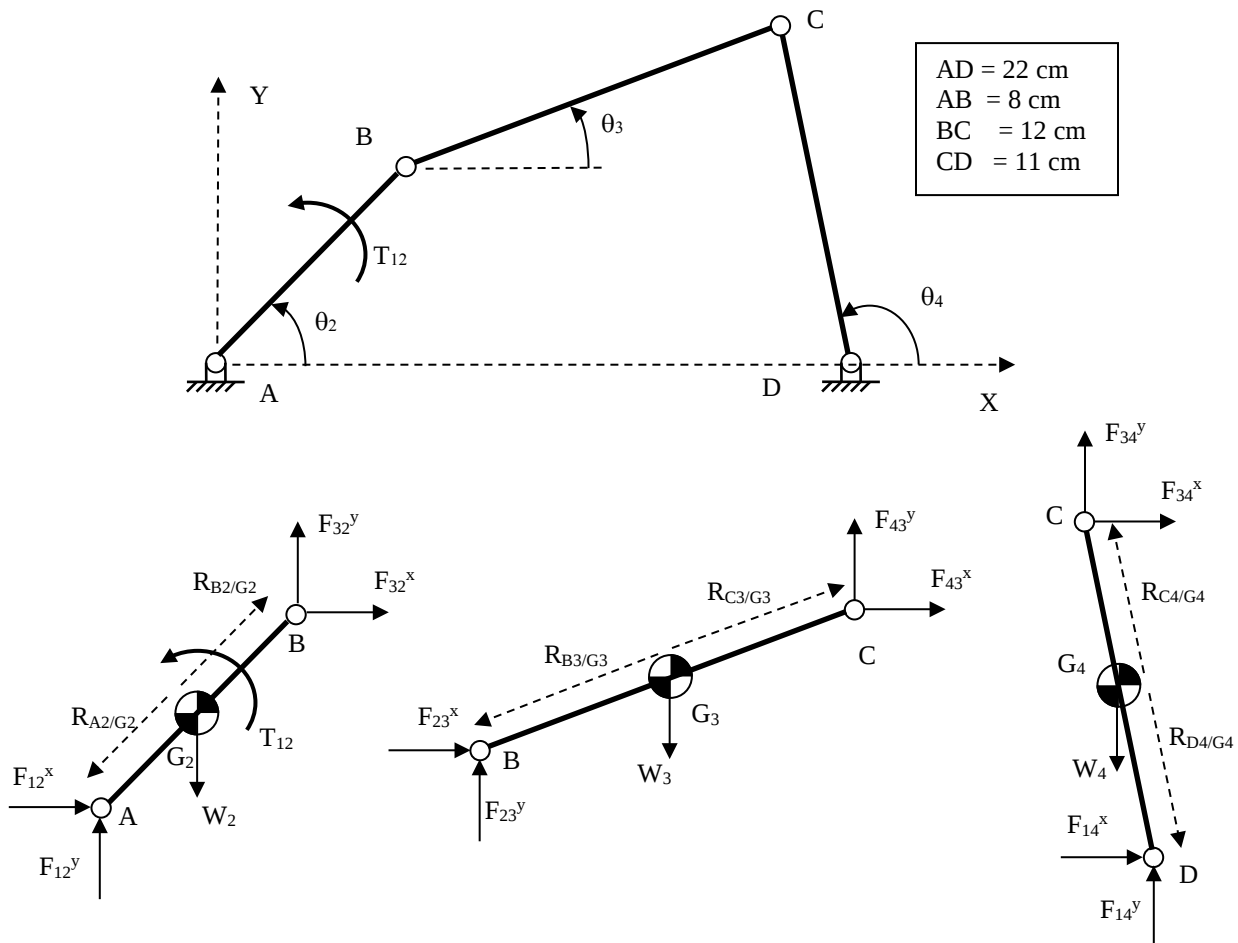
Matrix Dynamic Analysis for Four Bar

The four bar linkage shown below operates in a vertical plane. Each link is a uniform bar with 2 cm by 2 cm square cross-section stainless steel. Assume that the masses of the bearings and the effects of friction are negligible. Do not neglect the effects of gravity.

$\theta_2 = 45 \text{ deg}$	$\omega_2 = 20 \text{ rad/s CW}$	$\alpha_2 = 100 \text{ rad/s/s CCW}$
$\theta_3 = 20 \text{ deg}$	$\omega_3 = 12.82 \text{ rad/s CCW}$	$\alpha_3 = 39.6 \text{ rad/s/s CW}$
$\theta_4 = 117.4 \text{ deg}$	$\omega_4 = 6.20 \text{ rad/s CW}$	$\alpha_4 = 482.5 \text{ rad/s/s CCW}$

$m_2 = 0.248 \text{ kg}$	$J_{G2}' = 1.405 \text{ kg.cm}^2$	$\rho = 7.75 \text{ g/cm}^3$
$m_3 = 0.372 \text{ kg}$	$J_{G3}' = 4.588 \text{ kg.cm}^2$	
$m_4 = 0.341 \text{ kg}$	$J_{G4}' = 3.552 \text{ kg.cm}^2$	

$V_{G2} = 56.57 - j 56.57 \text{ cps}$	$A_{G2} = -1414.2 - j 848.5 \text{ cps}^2$
$V_{G3} = 86.83 - j 40.86 \text{ cps}$	$A_{G3} = -3672.5 - j 2260.9 \text{ cps}^2$
$V_{G4} = 30.27 - j 15.71 \text{ cps}$	$A_{G4} = -2262.4 - j 1412.4 \text{ cps}^2$



$$\begin{aligned}
\Sigma F \text{ on 2 right} + & F_{12}^x + F_{32}^x = m_2 A_{G2}^x \\
\Sigma F \text{ on 2 up} + & F_{12}^y + F_{32}^y + W_2 = m_2 A_{G2}^y \\
\Sigma M \text{ on 2 about } G_2 \text{ CCW} + & -F_{12}^x r_{A2/G2}^y + F_{12}^y r_{A2/G2}^x - F_{32}^x r_{B2/G2}^y + F_{32}^y r_{B2/G2}^x + T_{12} = J_{G2}' \alpha_2
\end{aligned}$$

$$\begin{aligned}
\Sigma F \text{ on 3 right} + & F_{23}^x + F_{43}^x = m_3 A_{G3}^x \\
\Sigma F \text{ on 3 up} + & F_{23}^y + F_{43}^y + W_3 = m_3 A_{G3}^y \\
\Sigma M \text{ on 3 about } G_3 \text{ CCW} + & -F_{23}^x r_{B3/G3}^y + F_{23}^y r_{B3/G3}^x - F_{43}^x r_{C3/G3}^y + F_{43}^y r_{C3/G3}^x = J_{G3}' \alpha_3
\end{aligned}$$

$$\begin{aligned}
\Sigma F \text{ on 4 right} + & F_{34}^x + F_{14}^x = m_4 A_{G4}^x \\
\Sigma F \text{ on 4 up} + & F_{34}^y + F_{14}^y + W_4 = m_4 A_{G4}^y \\
\Sigma M \text{ on 4 about } G_4 \text{ CCW} + & -F_{34}^x r_{C4/G4}^y + F_{34}^y r_{C4/G4}^x - F_{14}^x r_{D4/G4}^y + F_{14}^y r_{D4/G4}^x = J_{G4}' \alpha_4
\end{aligned}$$

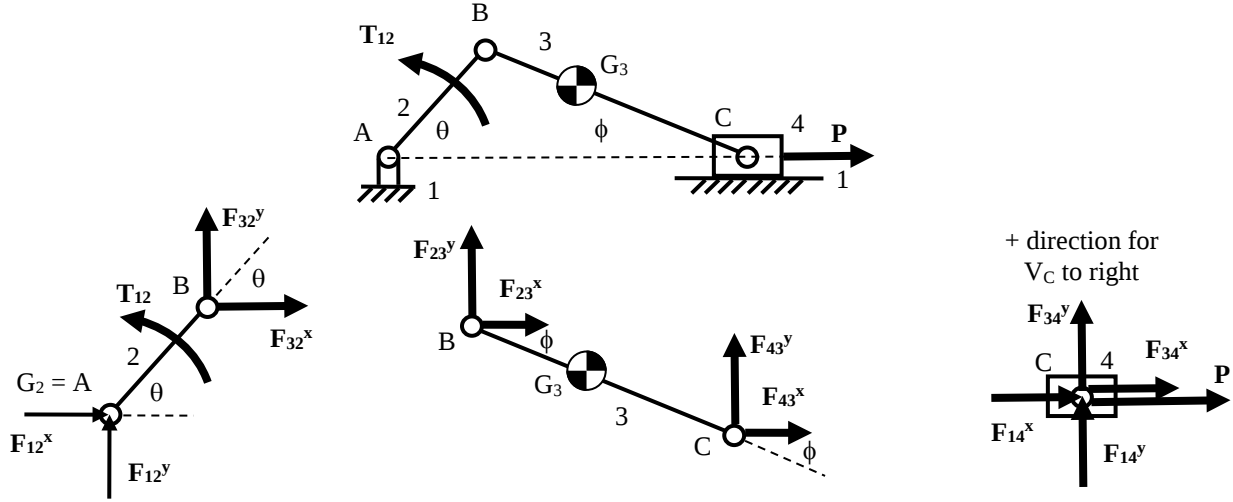
$$\begin{bmatrix} 1 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & -1 & 0 & 0 & 0 & 0 & 0 \\ +r_{A2/G2}^y & -r_{A2/G2}^x & r_{B2/G2}^y & -r_{B2/G2}^x & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 & -1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & -1 & 0 & 0 & 0 \\ 0 & 0 & -r_{B3/G3}^y & r_{B3/G3}^x & r_{C3/G3}^y & -r_{C3/G3}^x & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & -r_{C4/G4}^y & r_{C4/G4}^x & -r_{D4/G4}^y & r_{D4/G4}^x & 0 \end{bmatrix} \begin{bmatrix} F_{12}^x \\ F_{12}^y \\ F_{23}^x \\ F_{23}^y \\ F_{34}^x \\ F_{34}^y \\ F_{14}^x \\ F_{14}^y \\ T_{12} \end{bmatrix} = \begin{bmatrix} m_2 A_{G2}^x \\ m_2 A_{G2}^y - W_2 \\ J_{G2}' \alpha_2 \\ m_3 A_{G3}^x \\ m_3 A_{G3}^y - W_3 \\ J_{G3}' \alpha_3 \\ m_4 A_{G4}^x \\ m_4 A_{G4}^y - W_4 \\ J_{G4}' \alpha_4 \end{bmatrix}$$

$$\begin{aligned}
W_2 = -j \, 2.433 \, \text{N} & \quad m_2 A_{G2} = -3.507 - j \, 2.104 \, \text{N} & \quad J_{G2}' \alpha_2 = 1.405 \, \text{N.cm} \\
W_3 = -j \, 3.649 \, \text{N} & \quad m_3 A_{G3} = -13.662 - j \, 8.411 \, \text{N} & \quad J_{G3}' \alpha_3 = -1.817 \, \text{N.cm} \\
W_4 = -j \, 3.345 \, \text{N} & \quad m_4 A_{G4} = -7.715 - j \, 4.816 \, \text{N} & \quad J_{G4}' \alpha_4 = 17.138 \, \text{N.cm}
\end{aligned}$$

$$\begin{bmatrix} 1 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & -1 & 0 & 0 & 0 & 0 & 0 \\ 2.828 & -2.828 & 2.828 & -2.828 & 0 & 0 & 0 & 0 & 1 \\ 0 & 0 & 1 & 0 & -1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & -1 & 0 & 0 & 0 \\ 0 & 0 & 2.052 & -5.638 & 2.052 & -5.638 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & -4.883 & -2.531 & 4.883 & 2.531 & 0 \end{bmatrix} \begin{bmatrix} F_{12}^x \\ F_{12}^y \\ F_{23}^x \\ F_{23}^y \\ F_{34}^x \\ F_{34}^y \\ F_{14}^x \\ F_{14}^y \\ T_{12} \end{bmatrix} = \begin{bmatrix} -3.507 \\ 0.329 \\ 1.405 \\ -13.662 \\ -4.762 \\ -1.817 \\ -7.715 \\ -1.471 \\ 17.138 \end{bmatrix}$$

$$\left\{ \begin{array}{l} F_{12}^x \\ F_{12}^y \\ F_{23}^x \\ F_{23}^y \\ F_{34}^x \\ F_{34}^y \\ F_{14}^x \\ F_{14}^y \\ T_{12} \end{array} \right\} = \left\{ \begin{array}{l} -22.236 \text{ N} \\ -6.221 \text{ N} \\ -18.729 \text{ N} \\ -6.550 \text{ N} \\ -5.067 \text{ N} \\ -1.788 \text{ N} \\ -2.648 \text{ N} \\ +0.317 \text{ N} \\ +81.135 \text{ N.cm} \end{array} \right\}$$

Matrix Dynamic Analysis for Slider Crank



$$\begin{aligned}
 \Sigma F \text{ on 2 right} + & F_{12}^x + F_{32}^x = m_2 A_{G2}^x = 0 \\
 \Sigma F \text{ on 2 up} + & F_{12}^y + F_{32}^y = m_2 A_{G2}^y = 0 \\
 \Sigma M \text{ on 2 about A CCW} + & -(F_{32}^x \sin \theta) AB + (F_{32}^y \cos \theta) AB + T_{12} = J_{G2} \alpha_2
 \end{aligned}$$

$$\begin{aligned}
 \Sigma F \text{ on 3 right} + & F_{23}^x + F_{43}^x = m_3 A_{G3}^x \\
 \Sigma F \text{ on 3 up} + & F_{23}^y + F_{43}^y = m_3 A_{G3}^y \\
 \Sigma M \text{ on 3 about G}_3 \text{ CCW} + & -(F_{23}^x \sin \phi) BG_3 - (F_{23}^y \cos \phi) BG_3 \\
 & + (F_{43}^x \sin \phi) CG_3 + (F_{43}^y \cos \phi) CG_3 = J_{G3} \alpha_3
 \end{aligned}$$

$$\begin{aligned}
 \Sigma F \text{ on 4 right} + & F_{14}^x + F_{34}^x + P = m_4 A_{G4}^x \\
 \Sigma F \text{ on 4 up} + & F_{14}^y + F_{34}^y = m_4 A_{G4}^y = 0 \\
 \text{friction} & F_{14}^x = -\mu \text{abs}(F_{14}^y) \text{sign}(V_C)
 \end{aligned}$$

$$\begin{bmatrix}
 1 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 & 0 \\
 0 & 1 & 0 & -1 & 0 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & +AB \sin \theta & -AB \cos \theta & 0 & 0 & 0 & 0 & 1 & 0 \\
 0 & 0 & 1 & 0 & -1 & 0 & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 1 & 0 & -1 & 0 & 0 & 0 & 0 \\
 0 & 0 & -BG_3 \sin \phi & -BG_3 \cos \phi & +CG_3 \sin \phi & +CG_3 \cos \phi & 0 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 1 & 0 & 1 & 0 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 1 & 0 & 1 & 0 & 0 \\
 0 & 0 & 0 & 0 & 0 & 0 & 1 & +\mu \text{sign}(V_C) & 0 & 0
 \end{bmatrix}
 \begin{bmatrix}
 F_{12}^x \\
 F_{12}^y \\
 F_{23}^x \\
 F_{23}^y \\
 F_{34}^x \\
 F_{34}^y \\
 F_{14}^x \\
 F_{14}^y \\
 T_{12}
 \end{bmatrix}
 =
 \begin{bmatrix}
 0 \\
 0 \\
 J_{G2} \alpha_2 \\
 m_3 A_{G3}^x \\
 m_3 A_{G3}^y \\
 J_{G3} \alpha_3 \\
 m_4 A_{G4}^x - P \\
 0 \\
 0
 \end{bmatrix}$$