

- 1) Program your constraints and Jacobian for the web cutter into a Newton-Raphson iterative algorithm to solve position kinematics for any desired crank angle. To check your work, when $\phi_2 = 90$ degrees, $\phi_3 = 65.3$ degrees and $\phi_4 = -69.0$ degrees.
- 2) Develop the velocity right-hand-side vector $\{v\}$ for your constraints, and program them to solve for the generalized coordinate velocities $\{\dot{q}\}$. To check your work, when $\phi_2 = 90$ degrees, $\dot{\phi}_3 = 0.88$ rad/s CW and $\dot{\phi}_4 = 0.72$ rad/s CCW.
- 3) Develop the acceleration right-hand-side vector $\{a\}$ for your constraints, and program them to solve for the generalized coordinate accelerations $\{\ddot{q}\}$. To check your work, when $\phi_2 = 90$ degrees, $\ddot{\phi}_3 = 14.2$ rad/s/s CCW and $\ddot{\phi}_4 = 10.1$ rad/s/s CCW.
- 4) Place your position, velocity and acceleration algorithms within an outer loop to drive the crank through one complete revolution, and plot $\ddot{\phi}_4$ as a function of crank angle. Also plot the determinant of your Jacobian as a function of crank angle. Start the crank at $\phi_2 = 0$ degrees in your plots.
- 5) Determine the speed of the web.

$V_{WEB} < 9.37 \text{ cps}$

EXTRA CREDIT

Modify your code to simulate an in-line slider crank with $R = 4.00$ cm and $L = 14.23$ cm operating at constant 60 rpm CCW crank speed. Validate your results by plotting piston acceleration as a function of crank angle compared to simple geometric equations.

Closing $\phi_2 = 85.5^\circ$

$$\{r_3\}^P = \begin{Bmatrix} 18.0651 \text{ cm} \\ 13.8931 \text{ cm} \end{Bmatrix} \quad \{r_4\}^Q = \begin{Bmatrix} 18.0993 \text{ cm} \\ 13.8936 \text{ cm} \end{Bmatrix} \quad \{\dot{r}_3\}^P = \begin{Bmatrix} -14.50 \text{ cps} \\ -16.95 \text{ cps} \end{Bmatrix} \quad \{\dot{r}_4\}^Q = \begin{Bmatrix} -9.37 \text{ cps} \\ 2.88 \text{ cps} \end{Bmatrix}$$

Opening $\phi_2 = 257.4^\circ$

$$\{r_3\}^P = \begin{Bmatrix} 8.7160 \text{ cm} \\ 14.0208 \text{ cm} \end{Bmatrix} \quad \{r_4\}^Q = \begin{Bmatrix} 8.7511 \text{ cm} \\ 14.0194 \text{ cm} \end{Bmatrix} \quad \{\dot{r}_3\}^P = \begin{Bmatrix} -16.73 \text{ cps} \\ +16.59 \text{ cps} \end{Bmatrix} \quad \{\dot{r}_4\}^Q = \begin{Bmatrix} -10.33 \text{ cps} \\ -2.87 \text{ cps} \end{Bmatrix}$$

```

% sc_geometric.m - in-line slider crank geometric equations
% HJSIII, 14.02.22

clear

% constants
d2r = pi / 180;

% geometry and driver
R = 4;           % crank length [inch]
L = 14.23;       % connecting rod length [inch]
w = 60 * 2*pi / 60; % constant crank speed - 60 rpm CCW converted to rad/sec

% constant speed rotation driver motion
theta_deg = ( 0 : 6 : 360 )';
theta = theta_deg * d2r;
st = sin(theta);
ct = cos(theta);

thetad = w * ones( size( theta ) );
thetadd = zeros( size( theta ) );

% position
phi = asin( R * sin(theta) / L );
sp = sin(phi);
cp = cos(phi);

phid = R*thetad.*ct ./ (L*cp);
sd = -R*thetad.*st -L*phid.*sp;

phidd = ( R*thetadd.*ct -R*thetad.*thetad.*st +L*phid.*phid.*sp ) ./ (L*cp);
sdd = -R*thetadd.*st -R*thetad.*thetad.*ct -L*phidd.*sp -L*phid.*phid.*cp;

figure( 1 )
plot( theta_deg, sdd, 'r' )
axis( [ 0 360 -250 150 ] )
title( 'Slider crank geometric solution - 60 rpm CCW' )
xlabel( 'Crank angle [deg]' )
ylabel( 'Piston acceleration [ipss]' )

% bottom of sc_geometric

```

$$\{\Phi\} = \begin{Bmatrix} \{\Phi\}_{\text{KINEMATIC}} \\ \{\Phi\}_{\text{DRIVER}} \end{Bmatrix} = \begin{Bmatrix} \{\Phi\}_{\text{REV_A}} \\ \{\Phi\}_{\text{REV_B}} \\ \{\Phi\}_{\text{REV_C}} \\ \{\Phi\}_{\text{REV_D}} \\ \Phi_{\text{DRIVER}} \end{Bmatrix} = \begin{Bmatrix} \{\mathbf{r}_2\}^A - \{\mathbf{r}_1\}^A \\ \{\mathbf{r}_3\}^B - \{\mathbf{r}_2\}^B \\ \{\mathbf{r}_4\}^C - \{\mathbf{r}_3\}^C \\ \{\mathbf{r}_4\}^D - \{\mathbf{r}_1\}^D \\ \phi_2 - \phi_{2_START} - \omega_2 t \end{Bmatrix} = \{0\}$$

$$[\Phi_q]\{\dot{\mathbf{q}}\} = \begin{Bmatrix} \{\mathbf{v}\}_{\text{KINEMATIC}} \\ \{\mathbf{v}\}_{\text{DRIVER}} \end{Bmatrix} = \begin{Bmatrix} \{\mathbf{v}\}_{\text{REV_A}} \\ \{\mathbf{v}\}_{\text{REV_B}} \\ \{\mathbf{v}\}_{\text{REV_C}} \\ \{\mathbf{v}\}_{\text{REV_D}} \\ \mathbf{v}_{\text{DRIVER}} \end{Bmatrix} = \begin{Bmatrix} \{0_{2 \times 1}\} \\ \{0_{2 \times 1}\} \\ \{0_{2 \times 1}\} \\ \{0_{2 \times 1}\} \\ \omega_2 \end{Bmatrix}$$

$$\{\dot{\mathbf{q}}\} = [\Phi_q]^{-1} \begin{Bmatrix} \{0_{8 \times 1}\} \\ \omega_2 \end{Bmatrix}$$

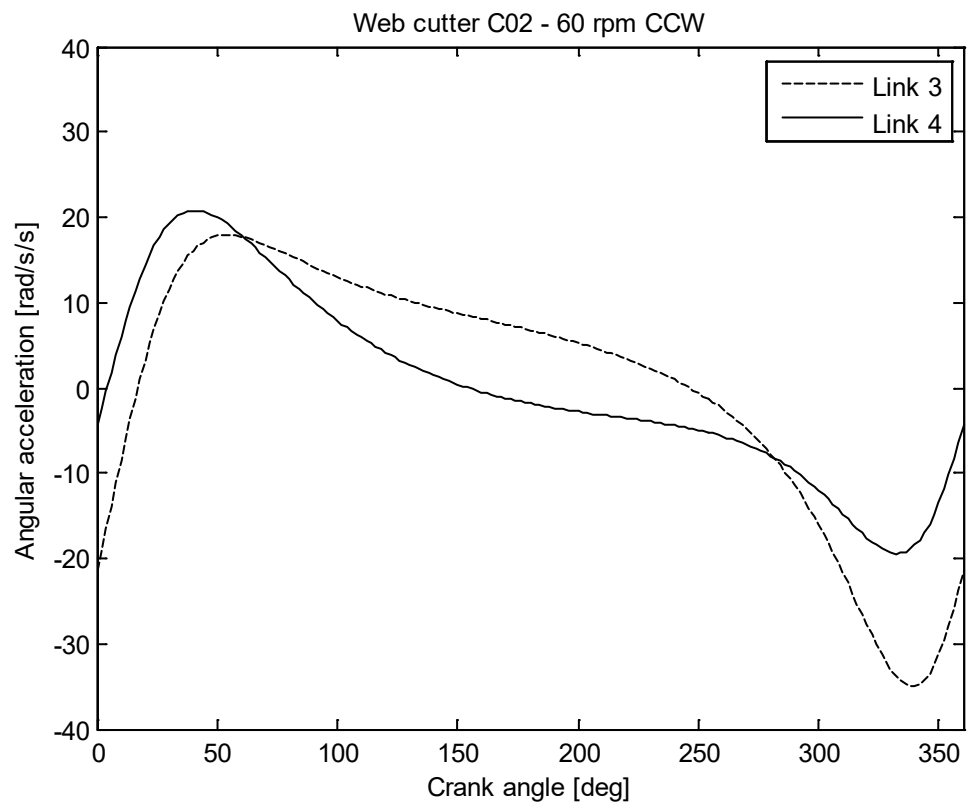
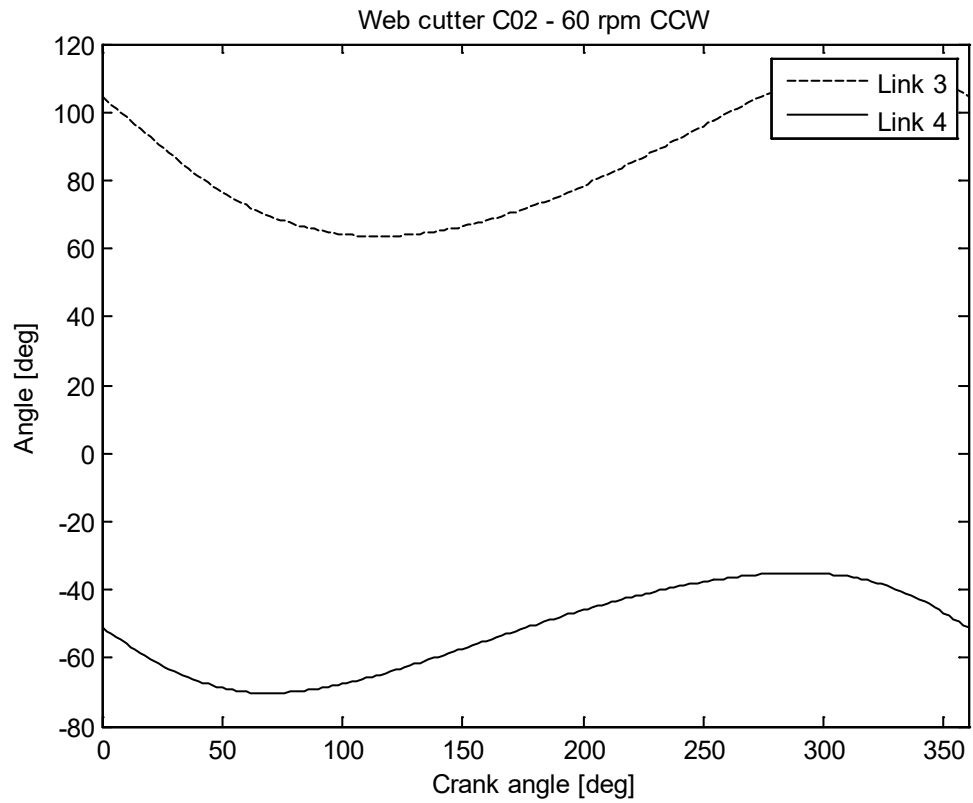
$$\{\Phi\}_{\text{REV}} = \{\mathbf{r}_{P_j}\} - \{\mathbf{r}_{P_i}\} = \{0_{2 \times 1}\}$$

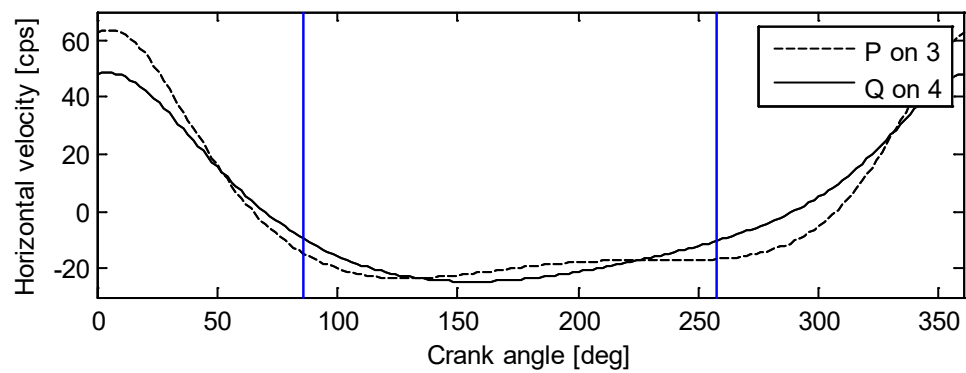
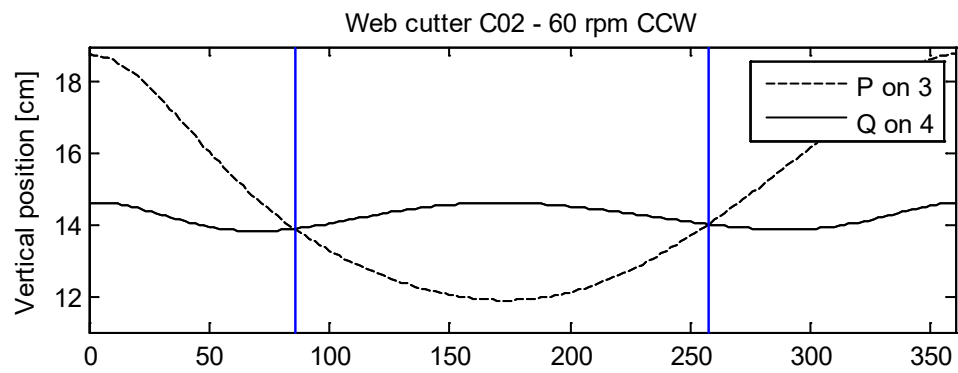
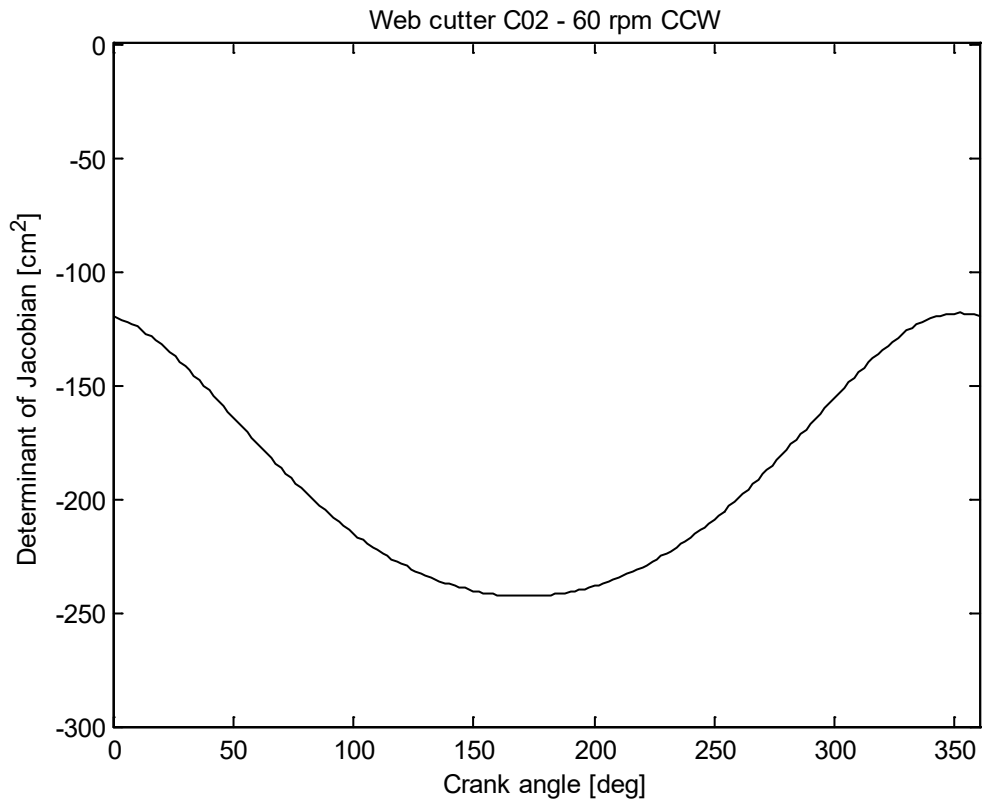
$$\{\gamma\}_{\text{REV}} = \dot{\phi}_j^2 [\mathbf{A}_j] \{\mathbf{s}_j\}^{\text{P}} - \dot{\phi}_i^2 [\mathbf{A}_i] \{\mathbf{s}_i\}^{\text{P}} \quad \{\gamma\}_{\text{DRIVER}} = -\{\Phi_{tt}\}$$

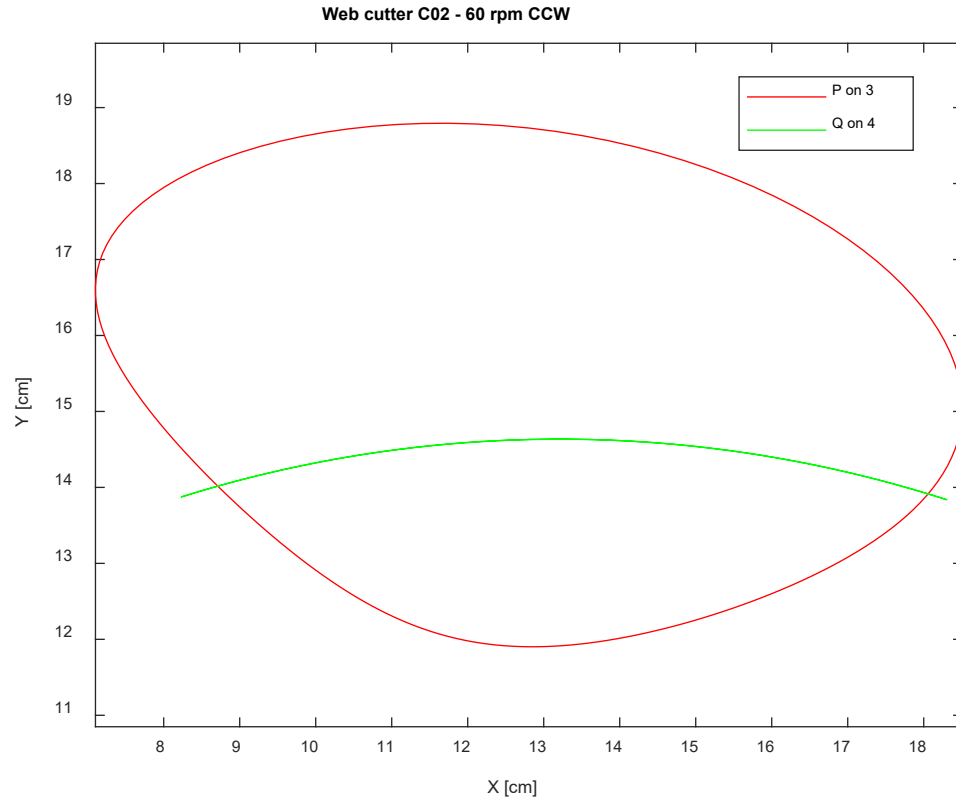
$$[\Phi_q]\{\ddot{\mathbf{q}}\} = \begin{Bmatrix} \{\gamma\}_{\text{KINEMATIC}} \\ \{\gamma\}_{\text{DRIVER}} \end{Bmatrix} = \begin{Bmatrix} \{\gamma\}_{\text{REV_A}} \\ \{\gamma\}_{\text{REV_B}} \\ \{\gamma\}_{\text{REV_C}} \\ \{\gamma\}_{\text{REV_D}} \\ \gamma_{\text{DRIVER}} \end{Bmatrix} = \begin{Bmatrix} \dot{\phi}_2^2 [\mathbf{A}_2] \{\mathbf{s}_2\}^{\text{A}} \\ \dot{\phi}_3^2 [\mathbf{A}_3] \{\mathbf{s}_3\}^{\text{B}} - \dot{\phi}_2^2 [\mathbf{A}_2] \{\mathbf{s}_2\}^{\text{B}} \\ \dot{\phi}_4^2 [\mathbf{A}_4] \{\mathbf{s}_4\}^{\text{C}} - \dot{\phi}_3^2 [\mathbf{A}_3] \{\mathbf{s}_3\}^{\text{C}} \\ \dot{\phi}_4^2 [\mathbf{A}_4] \{\mathbf{s}_4\}^{\text{D}} \\ 0 \end{Bmatrix}$$

$$\{\ddot{\mathbf{q}}\} = [\Phi_q]^{-1} \{\gamma\}$$

$$\{\dot{\mathbf{r}}_3\}^{\text{P}} = \{\dot{\mathbf{r}}_3\} + \dot{\phi}_3 [\mathbf{B}_3] \{\mathbf{s}_3\}^{\text{P}} \quad \{\dot{\mathbf{r}}_4\}^{\text{Q}} = \{\dot{\mathbf{r}}_3\} + \dot{\phi}_4 [\mathbf{B}_4] \{\mathbf{s}_4\}^{\text{Q}}$$







```

% wc_main_c02.m - web cutter four-bar for ME 581
% main for Computer 2
% HJSIII, 22.02.16

clear

% general constants
d2r = pi / 180;
R = [ 0 -1; 1 0 ];

% initialize
wc_ini_c01

% starting position
phi2_start = 0 * d2r; % start at zero
%phi2_start = 30 * d2r; % position in line drawing
%phi2_start = 90 * d2r; % check at 90 degrees
%phi2_start = 85.5 * d2r; % cutter closing
%q = [ 0 0 4.4925 -0.8726 -3.9037 1.7233 -3.0341 10.1612 -0.6438]'; % q at opening
%phi2_start = 257.4 * d2r; % cutter opening

% time loop
%tpr = 0; % single poisition
tpr = 2 * pi / w2; % one revolution at constant speed
t_start = 0; % start
t_end = tpr; % end
nt = 180; % number of time steps
dt = (t_end - t_start) / nt;

keep_q = [];
keep = [];
for t = t_start : dt : t_end;

% kinematics
wc_kin

% save kinematics
detJAC = det(JAC);
x3P = r3P(1);
y3P = r3P(2);
x4Q = r4Q(1);
y4Q = r4Q(2);
x3Pd = r3Pd(1);
x4Qd = r4Qd(1);

keep_q = [ keep_q ; q' qd' qdd' ];
keep = [ keep ; detJAC x3P y3P x4Q y4Q x3Pd x4Qd ];

% bottom - for t
end

% plot
ang2 = keep_q(:,3) /d2r;
ang3 = keep_q(:,6) /d2r;
ang4 = keep_q(:,9) /d2r;
phi3dd = keep_q(:,24);
phi4dd = keep_q(:,27);
detJAC = keep(:,1);
x3P = keep(:,2);
y3P = keep(:,3);
x4Q = keep(:,4);
y4Q = keep(:,5);
x3Pd = keep(:,6);
x4Qd = keep(:,7);

figure( 1 )
clf
plot( ang2,ang3,'k--', ang2,ang4,'k-' )
axis( [ 0 360 -80 120 ] )
title( 'Web cutter C02 - 60 rpm CCW' )
xlabel( 'Crank angle [deg]' )

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```

ylabel( 'Angle [deg]' )
legend( 'Link 3', 'Link 4' )

figure( 2 )
clf
plot( ang2,phi3dd,'k--', ang2,phi4dd,'k-' )
axis( [ 0 360 -40 40 ] )
title( 'Web cutter C02 - 60 rpm CCW' )
xlabel( 'Crank angle [deg]' )
ylabel( 'Angular acceleration [rad/s/s]' )
legend( 'Link 3', 'Link 4' )

figure( 3 )
clf
plot( ang2,detJAC,'k' )
axis( [ 0 360 -300 0 ] )
title( 'Web cutter C02 - 60 rpm CCW' )
xlabel( 'Crank angle [deg]' )
ylabel( 'Determinant of Jacobian [cm^2]' )

figure( 4 )
clf
subplot( 2, 1, 1 )
plot( ang2,y3P,'k--', ang2,y4Q,'k-' )
hold on
plot( [ 85.5 85.5 NaN 257.4 257.4 ], [ 11 19 NaN 11 19 ], 'b' )
axis( [ 0 360 11 19 ] )
title( 'Web cutter C02 - 60 rpm CCW' )
% xlabel( 'Crank angle [deg]' )
ylabel( 'Vertical position [cm]' )
legend( 'P on 3', 'Q on 4' )

subplot( 2, 1, 2 )
plot( ang2,x3Pd,'k--', ang2,x4Qd,'k-' )
hold on
plot( [ 85.5 85.5 NaN 257.4 257.4 ], [ -30 70 NaN -30 70 ], 'b' )
axis( [ 0 360 -30 70 ] )
% title( 'Web cutter C02 - 60 rpm CCW' )
xlabel( 'Crank angle [deg]' )
ylabel( 'Horizontal velocity [cps]' )
legend( 'P on 3', 'Q on 4' )

figure( 5 )
clf
plot( x3P,y3P,'r', x4Q,y4Q,'g' )
axis equal
title( 'Web cutter C02 - 60 rpm CCW' )
xlabel( 'X [cm]' )
ylabel( 'Y [cm]' )
legend( 'P on 3', 'Q on 4' )

% save position data for animation
save wc_q.txt keep_q -ascii

% bottom - wc_main_c02

```

Same code for

wc_ini_c01.m

wc_phi.m


```

% wc_kin.m - web cutter four-bar for ME 581
% position, velocity, and acceleration
% HJSIII, 22.02.16

% Newton-Raphson position solution
assy_tol = 1e-5;
wc_phi
while max(abs(PHI)) > assy_tol,
    q = q - inv(JAC) * PHI;
    wc_phi
end

% velocity
velrhs = zeros(9,1);
velrhs(9) = w2;
qd = inv(JAC) * velrhs;

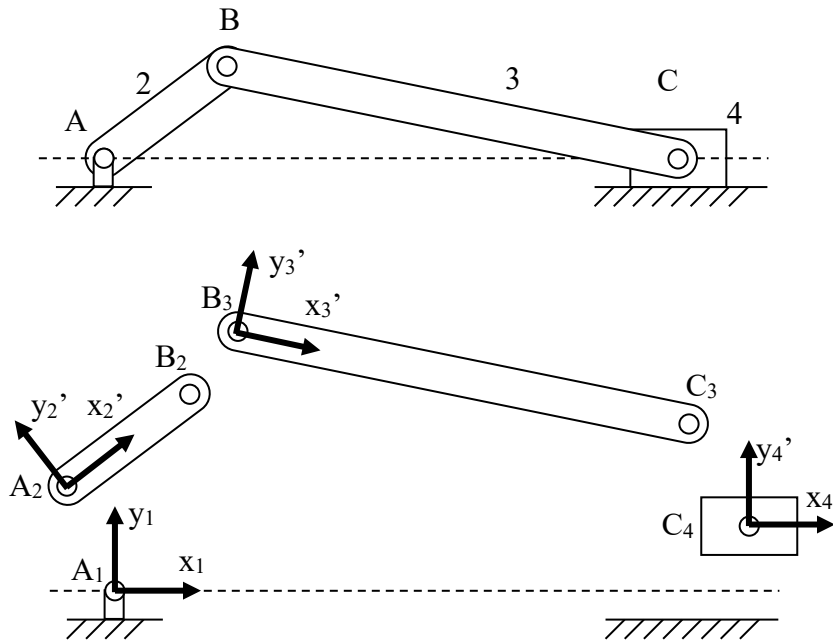
% global velocities of points
r2d = qd(1:2);
r3d = qd(4:5);
r4d = qd(7:8);
phi2d = qd(3);
phi3d = qd(6);
phi4d = qd(9);
r3Pd = r3d + phi3d*B3*s3pP;
r4Qd = r4d + phi4d*B4*s4pQ;

% acceleration
accrhs = zeros(9,1);
accrhs(1:2) = A2*s2pA*phi2d*phi2d;
accrhs(3:4) = A3*s3pB*phi3d*phi3d - A2*s2pB*phi2d*phi2d;
accrhs(5:6) = A4*s4pC*phi4d*phi4d - A3*s3pC*phi3d*phi3d;
accrhs(7:8) = A4*s4pD*phi4d*phi4d;
accrhs(9)=0;
qdd = inv(JAC) * accrhs;

% global accelerations
r2dd = qdd(1:2);
r3dd = qdd(4:5);
r4dd = qdd(7:8);
phi2dd = qdd(3);
phi3dd = qdd(6);
phi4dd = qdd(9);

% bottom - wc_kin

```



$$AB = R = 4 \text{ cm}$$

$$BC = L = 14.23 \text{ cm}$$

x_2 axis along centerline of link 2

x_3 axis along centerline of link 3

$\omega_2 = 60 \text{ rpm CCW constant}$

blueprint information

$$\{s_2\}^A = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix} \quad \{s_2\}^B = \begin{Bmatrix} R \\ 0 \end{Bmatrix} \quad \{s_3\}^B = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix} \quad \{s_3\}^C = \begin{Bmatrix} L \\ 0 \end{Bmatrix} \quad \{s_4\}^C = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix} \quad \{r_1\}^A = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}$$

adjust $\{r_2\}$ ϕ_2 $\{r_3\}$ ϕ_3 $\{r_4\}$ ϕ_4

check $\{r_2\}^A = \{r_1\}^A$ $\{r_3\}^B = \{r_2\}^B$ $\{r_4\}^C = \{r_3\}^C$ $y_4 = 0$ $\phi_4 = 0$

driver $\phi_2 = \omega_2 t$

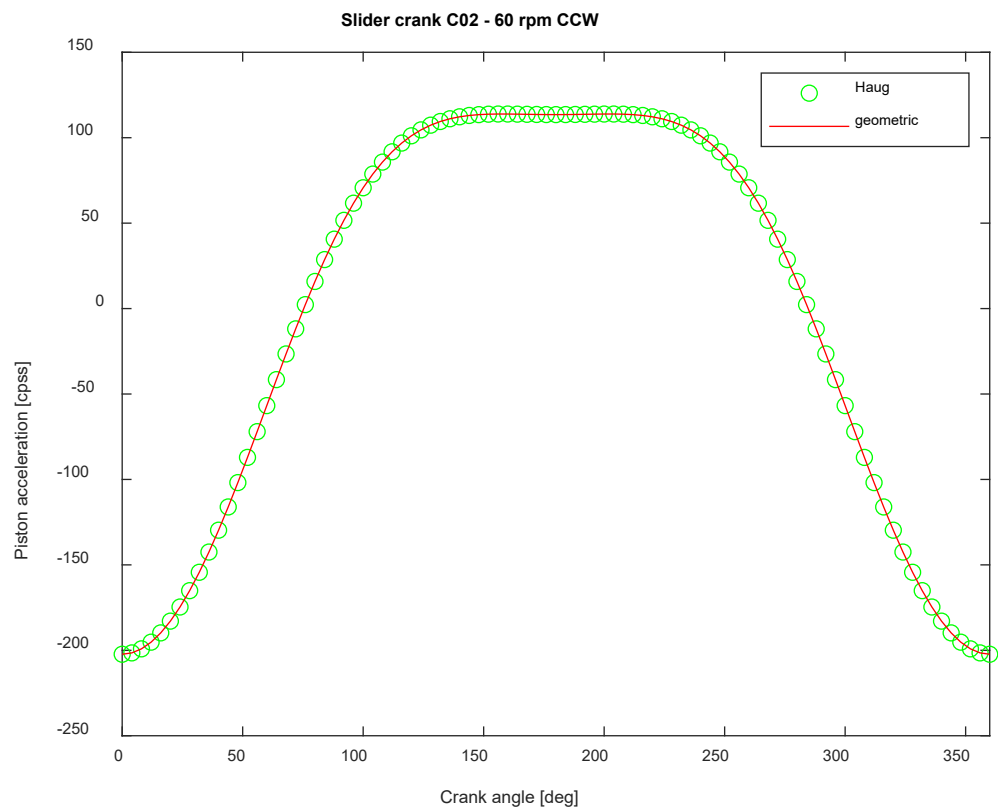
$$\{\Phi\} = \begin{Bmatrix} \{\Phi\}_{\text{KINEMATIC}} \\ \{\Phi\}_{\text{DRIVER}} \end{Bmatrix} = \begin{Bmatrix} \{\Phi\}_{\text{REV_A}} \\ \{\Phi\}_{\text{REV_B}} \\ \{\Phi\}_{\text{REV_C}} \\ \{\Phi\}_{\text{SLIDER}} \\ \Phi_{\text{DRIVER}} \end{Bmatrix} = \begin{Bmatrix} \{r_2\}^A - \{r_1\}^A \\ \{r_3\}^B - \{r_2\}^B \\ \{r_4\}^C - \{r_3\}^C \\ y_4 \\ \phi_4 \\ \phi_2 - \omega_2 t \end{Bmatrix} = \{0\}$$

$$[\Phi_q] = \begin{bmatrix} [I_2] & [B_2]\{s_2\}'^A & [0_{2 \times 2}] & [0_{2 \times 1}] & [0_{2 \times 2}] & [0_{2 \times 1}] \\ -[I_2] & -[B_2]\{s_2\}'^B & [I_2] & [B_3]\{s_3\}'^B & [0_{2 \times 2}] & [0_{2 \times 1}] \\ [0_{2 \times 2}] & [0_{2 \times 1}] & -[I_2] & -[B_3]\{s_3\}'^C & [I_2] & [B_4]\{s_4\}'^C \\ [0_{2 \times 2}] & [0_{2 \times 1}] & [0_{2 \times 2}] & [0_{2 \times 1}] & \begin{bmatrix} 0 & 1 \\ 0 & 0 \end{bmatrix} & \begin{Bmatrix} 0 \\ 1 \end{Bmatrix} \\ [0_{1 \times 2}] & 1 & [0_{1 \times 2}] & 0 & [0_{1 \times 2}] & 0 \end{bmatrix}$$

$$[\Phi_q]\{\dot{q}\} = \begin{Bmatrix} \{v\}_{\text{KINEMATIC}} \\ \{v\}_{\text{DRIVER}} \end{Bmatrix} = \begin{Bmatrix} \{v\}_{\text{REV_A}} \\ \{v\}_{\text{REV_B}} \\ \{v\}_{\text{REV_C}} \\ \{v\}_{\text{SLIDER}} \\ v_{\text{DRIVER}} \end{Bmatrix} = \begin{Bmatrix} \{0_{2 \times 1}\} \\ \{0_{2 \times 1}\} \\ \{0_{2 \times 1}\} \\ \{0_{2 \times 1}\} \\ \omega_2 \end{Bmatrix}$$

$$[\Phi_{q4}]^{\text{SLIDER}} = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad [\Phi_{q4}]\{\dot{q}_4\} = \begin{Bmatrix} \dot{y}_4 \\ \dot{\phi}_4 \end{Bmatrix} \quad ([\Phi_{q4}]\{\dot{q}_4\})_{q4} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix} \quad \{\gamma\}^{\text{SLIDER}} = \begin{Bmatrix} 0 \\ 0 \end{Bmatrix}$$

$$[\Phi_q]\{\ddot{q}\} = \begin{Bmatrix} \{\gamma\}_{\text{KINEMATIC}} \\ \{\gamma\}_{\text{DRIVER}} \end{Bmatrix} = \begin{Bmatrix} \{\gamma\}_{\text{REV_A}} \\ \{\gamma\}_{\text{REV_B}} \\ \{\gamma\}_{\text{REV_C}} \\ \{\gamma\}_{\text{SLIDER}} \\ \gamma_{\text{DRIVER}} \end{Bmatrix} = \begin{Bmatrix} \ddot{\phi}_2 {}^2[A_2]\{s_2\}'^A \\ \ddot{\phi}_3 {}^2[A_3]\{s_3\}'^B - \ddot{\phi}_2 {}^2[A_2]\{s_2\}'^B \\ \ddot{\phi}_4 {}^2[A_4]\{s_4\}'^C - \ddot{\phi}_3 {}^2[A_3]\{s_3\}'^C \\ \{0_{2 \times 1}\} \\ 0 \end{Bmatrix}$$



```

% sc_main.m - slider crank for ME 581 extra credit C02
%   main for Computer 2
% HJSIII, 20.03.04

clear

% general constants
d2r = pi / 180;
R = [ 0 -1; 1 0 ];

% initialize
sc_ini

% time loop
tpr = 2 * pi / w2;           % one revolution at constant speed
t_start = 0;                 % start
t_end = tpr;                 % end
nt = 180;                    % number of time steps
dt = (t_end - t_start) / nt;

keep_q = [];
for t = t_start : dt : t_end;

% kinematics
    sc_kin

% save kinematics
    keep_q = [ keep_q ; q'  qd'  qdd' ];

% bottom - for t
end

% values for plotting
phi2 = keep_q(:,3);
phi2_deg = phi2 / d2r;
x4dd = keep_q(:,25);

% geometric equations
R = R_link2;
L = L_link3;
theta = phi2;
st = sin(theta);
ct = cos(theta);

theta = phi2;
phi = asin( R * sin(theta) / L );
sp = sin(phi);
cp = cos(phi);

thetad = w2 * ones( size( theta ) );
phid = R*thetad.*ct ./ (L*cp);
sd = -R*thetad.*st -L*phid.*sp;

thetadd = zeros( size( theta ) );
phidd = ( R*thetadd.*ct -R*thetad.*thetad.*st +L*phid.*phid.*sp ) ./ (L*cp);
sdd = -R*thetadd.*st -R*thetad.*thetad.*ct -L*phidd.*sp -L*phid.*phid.*cp;

figure( 1 )
plot( phi2_deg,x4dd,'go', phi2_deg,sdd,'r' )
axis( [ 0 360 -250 150 ] )
title( 'Slider crank C02 - 60 rpm CCW' )
xlabel( 'Crank angle [deg]' )
ylabel( 'Piston acceleration [cpss]' )
legend( 'Haug', 'geometric' )

% bottom - sc_main

```

```
% sc_ini.m - slider crank for ME 581 extra credit C02
% initialize constants and assembly guesses
% HJSIII, 20.03.04

% mechanism constants
R_link2 = 4;           % units [cm]
L_link3 = 14.23;

s1pA = [ 0  0 ]';

s2pA = [ 0  0 ]';
s2pB = [ R_link2  0 ]';

s3pB = [ 0  0 ]';
s3pC = [ L_link3  0 ]';

s4pC = [ 0  0 ]';

% initial guesses
phi2 = 0 * d2r;
phi3 = 0 * d2r;
phi4 = 0 * d2r;

q = zeros(9,1);
q(1) = 0;
q(2) = 0;
q(3) = phi2;

q(4) = R_link2;
q(5) = 0;
q(6) = phi3;

q(7) = R_link2 + L_link3;
q(8) = 0;
q(9) = phi4;

% driver for crank - phi2 = w2*t
w2 = +60 * 2 * pi / 60;    % 60 rpm CCW, convert to rad/sec

% bottom - sc_ini
```

```

% sc_phi.m - slider crank for ME 581 extra credit C02
%   evaluate constraints and Jacobian for crank driving constraint
% HJSIII - 20.03.04

% global location of local frames and rotation matrices
r1 = [ 0  0  0 ]';
r2 = q(1:2);
r3 = q(4:5);
r4 = q(7:8);
phi1 = 0;
phi2 = q(3);
phi3 = q(6);
phi4 = q(9);
A1 = [ cos(phi1) -sin(phi1); sin(phi1) cos(phi1) ];
A2 = [ cos(phi2) -sin(phi2); sin(phi2) cos(phi2) ];
A3 = [ cos(phi3) -sin(phi3); sin(phi3) cos(phi3) ];
A4 = [ cos(phi4) -sin(phi4); sin(phi4) cos(phi4) ];
B2 = A2 * R;
B3 = A3 * R;
B4 = A4 * R;

% global locations of points
r1A = r1 + A1*s1pA;
r2A = r2 + A2*s2pA;
r2B = r2 + A2*s2pB;
r3B = r3 + A3*s3pB;
r3C = r3 + A3*s3pC;
r4C = r4 + A4*s4pC;
y4 = r4(2);

% three revolute constraints and slider constraint
PHI(1:2,1) = r2A - r1A;
PHI(3:4,1) = r3B - r2B;
PHI(5:6,1) = r4C - r3C;
PHI(7:8,1) = [ y4  phi4 ]';

% crank driver constraint
PHI(9,1) = phi2 - w2*t;

% Jacobian by rows
JAC = zeros(9,9);
JAC(1:2,1:3) = [ eye(2)  B2*s2pA ];

JAC(3:4,1:3) = [ -eye(2)  -B2*s2pB ];
JAC(3:4,4:6) = [ eye(2)  B3*s3pB ];

JAC(5:6,4:6) = [ -eye(2)  -B3*s3pC ];
JAC(5:6,7:9) = [ eye(2)  B4*s4pC ];

JAC(7,8) = 1;
JAC(8,9) = 1;

% driver constraint in Jacobian
JAC(9,3) = 1;

% current results
current_crank = phi2 / d2r;

% bottom - sc_phi

```

```

% sc_kin.m - slider crank for ME 581 extra credit C02
%   position, velocity, and acceleration
% HJSIII, 20.03.04

% Newton-Raphson position solution
assy_tol = 1e-5;
sc_phi
while max(abs(PHI)) > assy_tol,
    q = q - inv(JAC) * PHI;
    sc_phi
end

% velocity
velrhs = zeros(9,1);
velrhs(9) = w2;
qd = inv(JAC) * velrhs;

% global velocities of points
r2d = qd(1:2);
r3d = qd(4:5);
r4d = qd(7:8);
phi2d = qd(3);
phi3d = qd(6);
phi4d = qd(9);

% acceleration
accrhs = zeros(9,1);
accrhs(1:2) = A2*s2pA*phi2d*phi2d;
accrhs(3:4) = A3*s3pB*phi3d*phi3d - A2*s2pB*phi2d*phi2d;
accrhs(5:6) = A4*s4pC*phi4d*phi4d - A3*s3pC*phi3d*phi3d;
accrhs(7:8) = [ 0  0 ]';
accrhs(9) = 0;
qdd = inv(JAC) * accrhs;

% global accelerations
r2dd = qdd(1:2);
r3dd = qdd(4:5);
r4dd = qdd(7:8);
phi2dd = qdd(3);
phi3dd = qdd(6);
phi4dd = qdd(9);

% bottom - sc_kin

```